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NATIONAL DAM SAFETY PROGRAM. CONEWAGO CREEK WATERSHED DAM NUMB--ETC(U)

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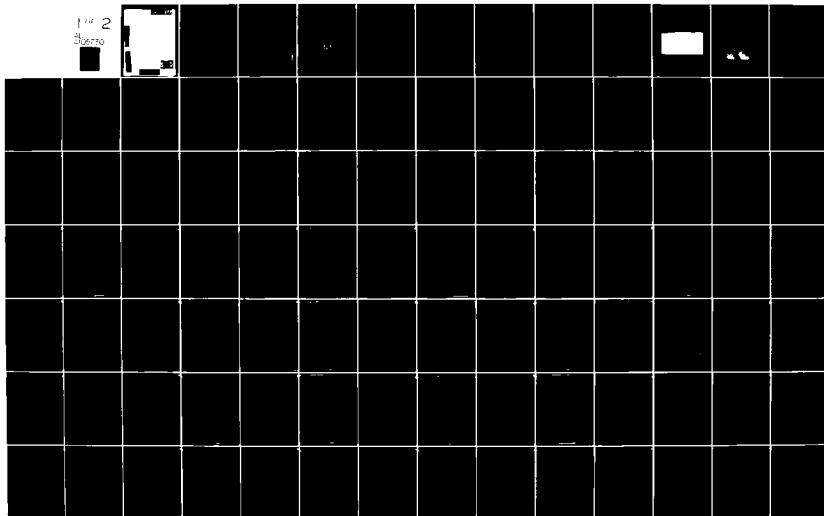
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report provides information and analysis on the physical condition of the dam as of the report date. Information and analysis are based on visual inspection of the dam by the performing organization. Examination of available documents and a visual inspection of the dam did not reveal conditions which constitute an immediate hazard to human life and property. However, the dam has some deficiencies which require further investigation and remedial action.		

The hydrologic/hydraulic analysis performed indicates that the spillway does not have sufficient capacity to discharge the peak outflow from the Probable Maximum Flood (PMF). However, spillway discharges occurring during large storm events will cause water surface elevations in the downstream hazard area to rise to flood levels. A dam failure resulting from overtopping would not significantly increase the hazard to loss of life from that which would exist just prior to an overtopping failure. The spillway has sufficient capacity to discharge 79% of the PMF. Therefore, the spillway is assessed as inadequate.

The dam is located in Seismic Zone 3 and there is no record of a seismic stability analysis being performed. Therefore, additional investigations by a qualified registered professional engineer to evaluate the seismic stability of the dam are recommended.

The investigations should be completed within 12 months of notification to owner, and to remedial actions resulting from these investigations completed in the subsequent 12 months.

The following remedial measures should be performed within one year from notification:

- Regrade and fill in the tire ruts on the downstream slope. Reseed the disturbed areas.
- Regrade and fill in the area of wave erosion on the upstream slope. Monitor for signs of future erosion.
- Implement a program of diligent and periodic maintenance including but not limited to: operation and lubrication of the reservoir drain; mowing of slopes and spillway channels; backfilling ruts, drainage gullies and animal burrows with suitable compacted material; clearing debris from trash racks and from upstream slopes.
- Install ladder rungs on the riser to provide access to the drain gate housing.
- Develop a formal written downstream warning system to alert the appropriate officials and residents in the event of an emergency.
- Develop and maintain a program of biannual technical inspections.

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ALLEGHENY RIVER BASIN

**CONEWANGO CREEK WATERSHED
DAM No. 9A**

**CHAUTAUQUA COUNTY, NEW YORK
INVENTORY No. N.Y. 596**

**PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM**

Conewango Creek Watershed Dam Number 9A
(Inventory Number NY.596), Allegheny River
Basin, Chautauqua County, New York. Phase
I Inspection Report.



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Robert J. Farrell

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NEW YORK DISTRICT, CORPS OF ENGINEERS

AUGUST 1981

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PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the Investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. In cases where the reservoir was lowered or drained prior to inspection, such action, while improving the stability and safety of the dam, removes the normal load on the structure and may obscure certain conditions which might otherwise be detectable if inspected under the normal operating environment of the structure.

It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through frequent inspections can unsafe conditions be detected and only through continued care and maintenance can these conditions be prevented or corrected.

Phase I Inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test Flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. Because of the magnitude and rarity of such a storm event a finding that a spillway will not pass the Test Flood should not be interpreted as necessarily posing a highly inadequate condition. The Test Flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Name of Dam:	Conewango Creek Watershed Dam No. 9A
State Located:	New York
County Located:	Chautauqua
Stream:	Conewango Creek
Basin:	Allegheny River
Date of Inspection:	May 22, 1981

ASSESSMENT

Examination of available documents and a visual inspection of the dam did not reveal conditions which constitute an immediate hazard to human life and property. However, the dam has some deficiencies which require further investigation and remedial action.

The hydrologic/hydraulic analysis performed indicates that the spillway does not have sufficient capacity to discharge the peak outflow from the Probable Maximum Flood (PMF). However, spillway discharges occurring during large storm events will cause water surface elevations in the downstream hazard area to rise to flood levels. A dam failure resulting from overtopping would not significantly increase the hazard to loss of life from that which would exist just prior to an overtopping failure. The spillway has sufficient capacity to discharge 79% of the PMF. Therefore, the spillway is assessed as inadequate.


The dam is located in Seismic Zone 3 and there is no record of a seismic stability analysis being performed. Therefore, additional investigations by a qualified registered professional engineer to evaluate the seismic stability of the dam are recommended.

The investigations should be completed within 12 months of notification to owner, and to remedial actions resulting from these investigations completed in the subsequent 12 months.


The following remedial measures should be performed within one year from notification:

- Regrade and fill in the tire ruts on the downstream slope. Reseed the disturbed areas.
- Regrade and fill in the area of wave erosion on the upstream slope. Monitor for signs of future erosion.

- Implement a program of diligent and periodic maintenance including but not limited to: operation and lubrication of the reservoir drain; mowing of slopes and spillway channels; backfilling ruts, drainage gullies and animal burrows with suitable compacted material; clearing debris from trash racks and from upstream slopes.
- Install ladder rungs on the riser to provide access to the drain gate housing.
- Develop a formal written downstream warning system to alert the appropriate officials and residents in the event of an emergency.
- Develop and maintain a program of biannual technical inspections.


Robert J. Farrell, P.E.
New York No. 55983

Approved by:


Col. W.M. Smith, Jr.
New York District Engineer

Date:

27 Aug 81

Conewango Creek Watershed (Site 9A)



OVERVIEW

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM
CONEWANGO CREEK WATERSHED DAM NO. 9A

SECTION I - PROJECT INFORMATION

1.1 GENERAL

a. Authority

The Phase I inspection reported herein was authorized by the New York District Corps of Engineers in a letter dated 24 February 1981, in fulfillment of the requirements of the National Dam Inspection Act, Public Law 92-367, dated 8 August 1972.

b. Purpose of Inspection

This inspection was conducted to evaluate the existing conditions of the dam, to identify deficiencies and hazardous conditions, to determine if these deficiencies constitute hazards to life and property, and to recommend remedial measures where required.

1.2 DESCRIPTION OF THE PROJECT

a. Description of Dam and Appurtenances

The Conewango Creek Watershed Dam No. 9A is an earth embankment approximately 1590 ft. long, with a maximum height of about 43 ft. and a crest width of 16 ft. The grassed downstream slope is 1V:2½H. The upstream slope is 1V:3H and grassed from the bottom to the top.

According to available contract drawings, the embankment consists of semi-pervious silty sand and gravel core with coarse gravel shells. There is a berm on the upstream slope approximately 10 ft. wide. The berm extends the full length of the dam at elevation 1365.5 MSL. Beneath the embankment is an earthfill cutoff trench which is 12 ft. wide at the bottom. According to available plans, it is constructed of the same silty sand and dense gravel material as the embankment.

The principal spillway consists of a reinforced concrete drop inlet structure with a sluice gate controlled inlet pipe, two uncontrolled orifice inlets and a 48 in. outlet pipe supported on a concrete cradle.

The inside dimensions of the riser structure are 30 ft. high and 12 ft. wide normal to the axis of the dam. It is 4 ft. long parallel to the embankment and flares to 21.67 ft. long at the top. The walls of the structure are 18 in. thick for the bottom 4.5 ft., 15 in. thick for the next 10 ft., 12 in. thick for the next 5 ft., and 10 in. thick for the top section. The top slab is 8 in. thick. The structure is founded on a 9 ft. by 15 ft. spread footing.

The "low stage inlet" is an uncontrolled opening approximately 15.6 ft. above the sluice gate invert. It is 3 ft wide and 2.2 ft. high and is located in the upstream face of the riser structure. The water flows through this orifice and drops into the riser structure. It is protected by a trash rack assembly approximately 11 ft. high and 5.5 ft. wide. This assembly is fabricated from galvanized steel angle sections.

The "high stage inlet" consists of two openings approximately 30 ft. above the sluice gate invert. They are 12 ft. wide and 2 ft. high and are located in the left and right sides of the flared portion of the riser structure. They are protected by a galvanized steel grating 33.4 in. high placed in front of each high stage opening and 5 galvanized steel angles placed in the sloping section below each opening. A 3 ft. diameter manhole permits access into the riser structure.

The riser structure is drained by a 48 in. diameter reinforced concrete pressure pipe. It is approximately 178 ft. long and drops approximately 2 ft. over that length. The pipe penetrates the downstream side of the riser structure and is supported by a 6 in. thick concrete cradle within the embankment. Plans indicate 7 concrete anti-seep collars cast around the pipe within the embankment.

The downstream end of the pipe penetrates the reinforced concrete impact basin. The inside dimensions of the impact basin are 23.3 ft. wide normal to the axis of the dam and 17.5 ft. long parallel to the embankment. It is 12.3 ft. high at the upstream face and tapers to 7.3 ft. at the downstream end. At the downstream side there is a cutoff wall extending 3.0 ft. beneath the floor of the impact basin and there are two wingwalls extending 10.5 ft. beyond the sidewalls of the basin parallel to the embankment. There is a 1 ft. thick by 7.5 ft. high baffle spanning between the walls of the impact basin. A 24 in. thick rip-rap apron extends 16 ft. downstream from the end of the impact basin.

An excavated emergency spillway channel is located at the north abutment. The channel is approximately 200 ft. wide at the base, 5.2 ft. high, and has 1V:3H side slopes. The control section is 200 ft. wide and 50 ft. long and the downstream channel is roughly 400 ft. long. A 50 ft. wide excavated bench is located north of the emergency spillway at elevation 1396 MSL. The bench intersects existing ground at 1V:3H side slope.

A 48 ft. long reinforced concrete pressure pipe located on the upstream side of the principal spillway sewer acts as the reservoir drain. The pipe rests on a 6 in. thick unreinforced concrete cradle. The upstream invert is at elevation 1354.5 MSL, and the pipe enters the principal spillway at elevation 1353.8 MSL, 2.8 ft. above the riser floor. The drain is regulated inside the structure by an 18 in. diameter slide gate, and a stem, and stem guides which rise to the top of the top slab where the handle housing is located.

A vertical seepage drain is located beneath the downstream slope to provide a safe outlet for seepage. It is 4 ft. wide and of variable depth. From approximately 160 ft. right of the principal spillway outlet to approximately 800 ft. left of the outlet, the drain contains a system of two, 8 in. diameter, perforated asbestos cement pipes which outlet on either side of the impact basin outlet structure.

b. Location

The dam is located approximately 4 miles northwest of South Dayton, New York in the Town of Villanova.

c. Size Classification

The dam is 43 ft. high and the reservoir has a storage capacity of 964 acre-ft. at elevation 1391.8 (top of dam). The dam is classified as "INTERMEDIATE" in size (40 to 100 ft. in height).

d. Hazard Classification

The dam is classified as HIGH hazard due to the significant economic and high potential for loss of life downstream in the event of dam failure. Table 5-1 shows the locations of downstream dwellings.

e. Ownership

The dam is owned and operated by:

Conewango Creek Watershed Commission
Donald Crowell, Chairman
RD #2
S. Dayton, New York 14138
Tele: (716) 988-3300

f. Purpose of Dam

The purpose of this dam is to reduce downstream flooding by providing temporary storage for the runoff from 3,840 acres. The temporary storage is released gradually through the two-stage principal spillway system.

g. Design and Construction History

The dam was designed by the U.S. Department of Agriculture Soil Conservation Service. For this inspection, a set of "as-built" contract drawings was provided by the Soil Conservation Service in Syracuse, New York. "As-built" dam cross sections, geotechnical design and analysis data, and supervision of construction reports can be found at the U.S. Department of Agriculture - Soil Conservation Service, Design Section, Syracuse, New York. The dam was constructed in 1972. The contractor's name is unknown.

h. Normal Operating Procedure

Water release from the lake is through the 48 in. reinforced concrete outlet pipe.

1.3 PERTINENT DATA

a. Drainage Area - 6.0 square miles

b. Discharge at Damsite

Maximum known flood at damsite - Unknown

Discharge from observed recent high water mark 114 cfs

Emergency Spillway

Maximum Pool (top of dam) 7708 cfs

Principal Spillway

Maximum Pool (top of dam) 492 cfs

Total Spillway Capacity at Maximum Pool Elevation 8200 cfs

c. Elevation (U.S.G.S. Datum)

Top of dam - 1391.8 ft.

Normal Pool 1366.6 ft.

Principal Spillway

Upstream invert 1351 ft.

Downstream invert 1349 ft.

Riser Crest 1381 ft.

Emergency Spillway Crest 1386.6 ft.

d. Reservoir

Length of Normal Pool 1200 ft.

Length of Maximum Pool 3400 ft.

e. Storage

Normal Pool 41 acre-ft.

Maximum Pool 964 acre-ft.

f. Reservoir Surface

Normal Pool 8.8 acres

Maximum Pool 74.6 acres

- | | | |
|----|---------------------------|---|
| g. | <u>Dam</u> | |
| | Type | Earth |
| | Length | 1590 ± ft. |
| | Maximum Height | 43 ± ft. |
| | Top Width | 16 ft. |
| | Side Slopes (V:H) | |
| | Upstream | 1:3 |
| | Downstream | 1:2.5 |
| h. | <u>Reservoir Drain</u> | |
| | Type | Reinforced concrete pipe |
| | Diameter | 18 in. |
| | Closure | Vertical slide gate |
| i. | <u>Principal Spillway</u> | |
| | Type | Reinforced concrete pipe |
| | Diameter | 48 in. |
| | Location | Near center of reservoir |
| | Support | Concrete cradle |
| | Upstream | Rectangular concrete drop inlet structure |
| | Downstream | Reinforced concrete impact basin |
| j. | <u>Emergency Spillway</u> | |
| | Type | Excavated channel |
| | Base Width | 200 ft. |
| | Height | 5.2 ft. |
| | Side Slopes | 1V:3H |
| | Location | North abutment |

SECTION 2 - ENGINEERING DATA

2.1 GEOLOGY

Local bedrock consists of interbedded shales, siltstones, and sandstones of late Devonian Age (345-375 million years ago). These relatively underformed flat-lying sedimentary rocks are medium hard. Regionally, the bedrock forms a homocline dipping southward to southwestward at approximately 40 feet per mile. Small terraces and low folds locally modify this dip to essentially horizontal over short distances. Only minor folding and faulting are found in the region with no major or active faults known to exist in the area.

The Conewango Creek Dam 9A is situated in a region classified as Zone 3 seismicity as shown on Figure No. 1 of the Recommended Guidelines for Safety Inspection of Dams.

Pleistocene glaciation (beginning approximately 2 million years ago) has modified the topography by means of erosion and deposition. The thick continental ice sheet advanced and receded repeatedly in the area smoothing terrain by glacial scour and mantling uplands with till deposits.

The Pleistocene geology of the immediate dam site consists of glacial ground moraine deposits. Generally, the overburden consists of sandy gravel alluvial deposits overlying lacustrine clays and silts. Alluvial gravels and sands underlie the lacustrine materials and dense glacial tills underlay the alluvial materials. In recent times alluvium, eroded from nearby uplands, has been deposited upon the glacial deposits.

2.2 SUBSURFACE INVESTIGATION

Test hole logs are contained in the "as-built" drawings. A total of 28 test pits and 34 drill holes were dug to determine subsurface conditions. The logs show that the dam is founded on glacial till at the north abutment and on silty sand and gravels in the center and south abutments.

2.3 DESIGN RECORDS

The records available for the project consists of 34 contract drawings which show the plans, sections and details of the dam, appurtenant structures, impact basin details and grating, fencing details, and logs of test holes; and a design report issued by the U.S. Soil Conservation Service dated May 10, 1972.

2.4 CONSTRUCTION RECORDS

Construction records and specifications are available at the U.S. Soil Conservation Service, Design Section, Syracuse, N.Y.

The sedimentation basin structure shown on Page 2 of the "As-built" drawings was not found during the visual inspection.

2.5 OPERATION RECORDS

No written maintenance or operation records exist for the dam

2.6 EVALUATION OF DATA

Information obtained from the "As built" drawings is consistent with observations made during this inspection with the exception of the sedimentation basin discussed in Section 2.4. The information obtained from available data was considered adequate for the Phase I inspection and evaluation.

SECTION 3 - VISUAL INSPECTION

3.1 FINDINGS

a. General

A visual inspection of Conewango Creek Watershed Dam No. 9A was made on 2 May 1981. The weather was clear and the temperature in the mid-seventies. At the time of the inspection, the reservoir level was about 2 in. above the intake structure crest elevation.

b. Dam

The earth embankment appears to be in good condition.

There is a light brush growth at the waterline on the upstream slope. The grass cover on this dam is generally in good condition. There has been some vehicular traffic on the downstream slope resulting in ruts approximately 2 to 4 in. deep, running vertically up the slope approximately 75 ft. to the right of the outlet structure. The crest of the dam is in good condition with no evidence of vertical or horizontal movement.

Animal burrows up to 6 in. in diameter were noted in the downstream slope approximately 150 ft. to the left of the right abutment, approximately 300 ft. to the left of the outlet structure, and at the contact with the emergency spillway diversion berm. An animal burrow approximately 8 in. in diameter was noted at the right upstream end of the diversion berm.

There is no slope protection on the upstream slope other than the vegetative cover and a 10 ft. berm just below waterline. Approximately 4 to 6 in. of erosion due to wave action was noted at and just above the waterline. Small (1-2 in diameter) eddy current type, erosion gullies were noted over most of the surface of the embankment. A few minor (3 in. deep) erosion channels were noted approximately 400 ft. north of the outlet structure on the downstream slope. A mat of dead grass caused by infrequent mowing is believed to be responsible for this concentration of runoff.

Some debris in the form of trash, vegetation, and driftwood, etc., has collected along the upstream slope at approximately the level of the high stage inlet.

Two toe drain outlets are located in the wingwalls of the impact basin. No discharge was noted from these outlets.

c. Principal Spillway

The principal spillway appears to be in good condition. No debris was noted on the low or high stage trash racks or on riser structure. There is a minimum amount of erosion around the inlet and outlet works. There is no access to the riser structure. No seepage was found around the spillway pipe. The channel for 16 ft. downstream of the impact basin is protected by rip-rap which appears durable and is generally in good condition.

d. Emergency Spillway

The emergency spillway appears to be in good condition. Grass, 6 in. high, covers the crest and downstream channel spillway. No debris was noted on the crest. An area of ponded runoff or natural groundwater was noted downstream of the control section of the channel. It encompasses the surface of the berm on the north slope. A small spring was noted on the north slope above the berm.

The water is drained from the berm through a 4 in. cast iron pipe located approximately at station 8+00, 100 ft. left on the emergency spillway.

There is a small tributary which joins the outlet channel approximately 250 ft. downstream of the principal spillway outlet. The tributary flows normal to the direction of outflow channel from dam.

e. Appurtenant Structures

The sedimentation basin structure shown on Page 2 of "As built" drawing was not found but there exists an embankment with no definite slope.

The stem of the slide gate does not have a handle attached to it. The operability of the gate could not, therefore, be determined. The reservoir drain inlet was located below the water surface at the time of inspection.

f. Downstream Channel

The downstream channel is a narrow channel passing over relatively flat flood plain. Minor erosion of the right bank has taken place at a point 200 ft. downstream of the outlet. The channel bottom is gravel.

g. Reservoir

The shore of the reservoir is generally shallow sloping pasture and farmland. It appears to be stable and in good condition. There is no visible sign of sedimentation problems in the reservoir area.

h. Abutments

No seepage was observed at either the south or north abutments. The south abutment is covered by farm lands and the north abutment is cut into a hill covered by woods. There exists an unpaved road at the south abutment that runs along the top of the dam.

3.2 EVALUATION OF OBSERVATIONS

Visual observations made during the course of the inspection did not indicate any serious problems which would adversely affect the adequacy of the dam and appurtenant facilities.

The potential problems noted during the visual inspection are listed below:

1. Animal burrows in embankment slopes.
2. Brush growth and wave erosion at the waterline on the upstream slope.
3. Rutting of downstream slope due to vehicular traffic.
4. Grass needs regular mowing.
5. The operation of the reservoir drain could not be checked because there is no access to the top of the riser and no gate handle on the stem.

SECTION 4 - OPERATION AND MAINTENANCE PROCEDURES

4.1 PROCEDURES

No written operation and maintenance procedures exist for the project. The normal operation of the project consists of allowing water to flow through the service spillway outlet pipe.

4.2 MAINTENANCE OF DAM

An annual inspection of the dam is made by the Soil Conservation Service. Recommendations resulting from this inspection are implemented by the Soil Conservation Service.

4.3 WARNING SYSTEM IN EFFECT

No warning system is in effect or in preparation.

4.4 EVALUATION

The overall condition of the dam and appurtenant structures appears to be good. Recommendations in connection with regular maintenance are discussed in Section 7.

SECTION 5 - HYDRAULIC/HYDROLOGIC

5.1 DRAINAGE AREA CHARACTERISTICS

Conewango Creek Watershed Dam No. 9A is located on a tributary of Conewango Creek in the Allegheny River basin, and has a drainage area of 6.0 square miles. The dam is situated approximately 4 miles northwest of South Dayton, New York in the Town of Villenova. The topography of the watershed is hilly woodland, pastures, and farmlands.

5.2 DESIGN DATA

The dam was designed as a Class B structure in accordance with criteria established in Washington Engineering Memorandum SCS-27. Under this classification, the emergency spillway is designed for a rainfall equal to $P(100) + 0.12 [PMP - P(100)]$, while the freeboard pool is designed for $P(100) + 0.40 [PMP - P(100)]$.

The Soil Conservation Service (SCS) design calculations have been reviewed. The dam was designed to contain the runoff for the 50 year flood without discharging through the emergency spillway. The peak outflow is 312 cfs and the peak elevation is 1386.6 ft. (MSL). The SCS design allowed for a 50 year sediment accumulation with a storage of 40.6 acre-ft. The principal spillway consists of 48 in. diameter reinforced concrete pressure pipe and a 4 ft. x 12 ft. reinforced concrete riser with two 12 ft. x 2 ft. openings with a crest elevation of 1381.0 ft. (MSL). The riser has a 3.0 ft. x 2.17 ft. orifice with a crest elevation of 1366.6 ft. (MSL). The emergency spillway control cross section is 200 ft. wide, with side slopes of 3 horizontal to 1 vertical and a crest elevation of 1386.6 (MSL). The dam crest elevation is 1391.8 (MSL).

5.3 ANALYSIS CRITERIA

The analysis of the spillway capacity of the dam and the storage of the reservoir was performed using the Corps of Engineers HEC-1 Dam Safety Version computer model. The unit hydrograph was defined by the Snyder Synthetic Unit Hydrograph method, and the Modified Puls routing procedure was incorporated. The Probable Maximum Precipitation (PMP) was 22.6 in. (24 hours 200 sq. miles) from Hydrometeorological Report #33 in accordance with the Recommended Guidelines of the Corps of Engineers. The dam is 43 ft. high and impounds approximately 964 acre-ft. at the top of the dam. The dam is classified as a HIGH hazard and INTERMEDIATE in size, according to the Recommended Guidelines of the Corps of Engineers. The spillway design flood is the Probable Maximum Flood (PMF). The floods selected for analysis were 20, 40, 50, 60 80 and 100% of the PMF flows. The PMF inflow of 10,448 cfs was routed through the reservoir and the peak outflow was determined to be 10,423 cfs. The peak PMF

5.5 EXPERIENCE DATA

There are no flood records for the dam site. However, during the field investigation evidence of recent high water was observed at elevation 1380.5 ft. (MSL). This reservoir elevation corresponds to a peak outflow of 114 cfs.

5.6 OVERTOPPING POTENTIAL

The maximum capacity of the spillways is 8259 cfs which is less than the PMF peak outflow of 10,423 cfs. The dam is overtopped by the PMF, the peak elevation being 0.4 ft. above the top of the dam. The dam is not overtopped by half the PMF, the peak elevation being 1.5 ft. below the top of the dam. The spillways can pass 79% of the PMF outflow before overtopping occurs.

5.7 ANALYSIS OF DOWNSTREAM IMPACTS

During the field investigation, dwellings and highways located downstream of the dam were identified and referenced to the channel invert. The cross section locations used in the downstream channel routing are shown on Page D-2, Appendix D. The impacts of the PMF on dwellings located downstream of the dam are shown in Table 5.1. For the purposes of this analysis, a danger of loss of life was assumed to exist if the computed PMF water surface was above the first floor elevation of a structure. This situation does not occur at any of the structures and no roads are overtopped during the PMF. In spite of these results, the potential danger of loss of life and economic damage is substantial enough to warrant classification as a HIGH hazard dam.

5.8 EVALUATION

The spillway of Conewango Creek Watershed Dam No. 9A will safely pass the 1/2 PMF without overtopping but it will not pass the PMF without overtopping. The spillway, therefore, is assessed as inadequate, but not seriously inadequate. Potential problems include:

- a) The danger of loss of life and economic damage downstream of the dam for the PMF condition.

TABLE 5-1

SUMMARY OF DOWNSTREAM IMPACTS FOR PMF

Location # (See Pg. D-2) Appendix D	Location	# of Dwellings	Structure Height Above Streambed* (ft)	Peak Flow (cfs)	Peak Stage (ft)	Comments
-	At Dam	-	-	10423	-	-
1	670 ft. d/s of Dam	1 1	13.5 12	10430	8.8	No danger of loss of life
2	7600 ft. d/s of Location 1	2	20.	20599	14.1	No danger of loss of life
3	1800 ft. d/s of Location 2	1	26	20605	16.6	No danger of loss of life
4	1500 ft. d/s of Location 3	2	20.	20577	14.6	No danger of loss of life

* The structure height above the streambed is the elevation of the first floor above the channel invert.

NOTE: A tributary stream joins the channel leading from the dam at a point between Locations 1 and 2

SECTION 6 - STRUCTURAL STABILITY

6.1 VISUAL OBSERVATIONS

There does not appear to be significant displacement or distress associated with the embankments at this site. The dam appears to be in good condition at the present time.

6.2 DESIGN AND CONSTRUCTION DATA

Analyses carried out during the design and construction phase by the Soil Conservation Service included a slope stability analysis by a modified Swedish circle method. The parameters assumed were:

Upstream slope: 3H:1V, full drawdown, 10 ft. berm at El. 1365.6 ft, $\phi = 31.5^\circ$, $c = 100$ psf.

Downstream slope: 2.5H:1V, trench drain at $c/b = 0.6$, no berm, $\phi = 31.5^\circ$, $c = 100$ psf.

The factors of safety calculated were 1.35 for the upstream slope and 1.74 for the downstream slope. The Phase I Recommended Guidelines suggests safety factors of 1.2 and 1.5, respectively, for the conditions analyzed. Based on the existing conditions as revealed by the visual inspection and the review of the original design information, the dam is considered to possess adequate structural stability.

6.3 POST CONSTRUCTION CHANGES

There have been no known changes to any of the embankments or structures at this dam.

6.4 SEISMIC STABILITY

The dam is located in Seismic Zone #3 and, in accordance with recommend Phase I guidelines, a seismic stability analysis is warranted. This should be accomplished by a qualified registered professional engineer and should be made part of the record for this dam.

SECTION 7 - ASSESSMENT/RECOMMENDATIONS

7.1 ASSESSMENT

a. Safety

Examination of the available documents and visual inspections of the Conewango Creek Watershed Dam No. 9A and appurtenant structures did not reveal any conditions which constitute a hazard to human life or property. The dam and its appurtenances are considered to be in good condition at the present time.

Using the Corps of Engineers screening criteria for review of spillway adequacy, it has been determined that the dam would be overtopped for the spillway design flood of the full PMF. The principal and auxiliary spillway capacity are, therefore, judged as inadequate. The dam would not be overtopped for one-half the PMF.

b. Adequacy of information

This report and its conclusions are based on visual inspection, interview data, contract drawings, and office hydrologic/hydraulic studies. This information and data are adequate for a Phase I inspection.

c. Need for additional investigations

It is recommended that the services of a qualified registered professional engineer be retained to evaluate:

- 1) the seismic stability of the dam.

The engineer should make recommendations for remedial measure if warranted and the owner should implement the findings of these studies.

d. Urgency

All remedial actions described below should be completed within one year of notification to the owner.

7.2 RECOMMENDED MEASURES

It is recommended that the owner institute the following remedial measures:

- 1) Develop a formal written downstream warning system to alert the appropriate officials and residents in the event of an emergency.
- 2) Develop and maintain a program of biannual technical inspections.

- 3) Regrade and fill in the tire ruts on the downstream slope. Reseed the disturbed areas.
- 4) Regrade and fill the area of wave erosion on the upstream slope. Monitor for signs of future erosion.
- 5) Install ladder rungs on the riser to provide access to the drain gate housing.
- 6) Implement a program of diligent and a periodic maintenance including but not limited to: mowing of slopes and spillway channels; back-filling ruts, drainage gullies, and animal burrows with suitable compacted material; clearing debris from trash racks and upstream slopes; and check the operability of and lubricating of the reservoir drain gate.

APPENDIX A
VISUAL INSPECTION CHECKLIST

VISUAL INSPECTION CHECKLIST

1) Basic Data

a. General

Name of Dam Conewango Creek Watershed Dam No. 9A
Fed. I.D. # N.Y. 00596 DEC Dam No. 7B-3979
River Basin Allegheny
Location: Town Villanova County Chautauqua
Stream Name Tributary of Conewango Creek
Tributary of _____
Latitude (N) 42° 23.0' Longitude (W) 79° 06.9'
Type of Dam Earth Embankment
Hazard Category HIGH
Date(s) of Inspection May 20, 1981
Weather Conditions Sunny, 75°
Reservoir Level at Time of Inspection Approximately elevation 1367

b. Inspection Personnel Jeff Hardin, Ray Kampff, Ken Avery, Bob Farrell

c. Persons Contacted (including Address & Phone No.) _____

U.S. Soil Conservation Service, RM771-Federal Bldg., So. Clinton St., Syracuse, N.Y.

State Construction Engineer: Philip "Skip" Nelson / 1-315-423-5502

Area 1 Project Engr (Batavia): Pete Wright / 1-716-343-3664

Contracting Office for Ischua Creek Watershed: Ed Smith - Contacted through Pete Wright

d. History:

Date Constructed 1972 Date(s) Reconstructed _____

Designer U.S.D.A. Soil Conservation Service

Constructed by _____

Owner Conewango Creek Watershed Commission

(2) Embankment

a. Characteristics

- (1) Embankment Material Semi-pervious, silty sand and gravel core, coarse gravel shells
- (2) Cutoff Type Earth fill, semi-pervious, 12 feet wide, variable depth
- (3) Impervious Core Semi-pervious silty sand and gravel (compacted glacial till)
- (4) Internal Drainage System 4 foot wide trench drain with 8 inch diameter perforated pipe
- (5) Miscellaneous _____

b. Crest

- (1) Vertical Alignment Good
- (2) Horizontal Alignment Good
- (3) Surface None noted
- (4) Miscellaneous _____

c. Upstream Slope

- (1) Slope (Estimate) (V:H) 1 vertical to 3 horizontal
- (2) Undesirable Growth or Debris, Animal Burrows light brush and grass growth, needs mowing
- (3) Sloughing, Subsidence or Depressions None noted

(4) Slope Protection Grass, no riprap, 10 foot berm just below waterline, approximately 6 inches of wave erosion at, and just above, waterline

(5) Surface Cracks or Movement at Toe None noted

d. Downstream Slope

(1) Slope (Estimate - V:H) 1 vertical and 2.5 horizontal

(2) Undesirable Growth or Debris, Animal Burrows Animal burrows noted 150 feet left of right abutment, 300 feet left of outlet and at left

(3) ^{abutment} Sloughing, Subsidence, or Depressions None noted

(4) Surface Cracks or Movement at Toe None noted

(5) Seepage None noted

(6) External Drainage System (Ditches, Trenches, Blanket) None

(7) Condition Around Outlet Structure Generally good, minor erosion along slopes

(8) Seepage Beyond Toe None noted

e. Abutments - Embankment Contact

Generally good condition, spring noted in left abutment above top of dam elevation

(1) Erosion at Contact None noted

(2) Seepage Along Contact None noted

3) Drainage System

(a) Description of System 4 ft. wide, trench drain with 8 in. perforated pipe

(b) Condition of System Could not be assessed, zero discharge probably not significant since no signs of seepage were noted.

(c) Discharge from Drainage System None

4) Instrumentation (Monumentation/Surveys, Observation Wells, Weirs, Piezometers, etc.) None installed

5) Reservoir

a. Slopes Appear stable and in good condition

b. Sedimentation Very minor accumulation

c. Unusual Conditions Which Affect Dam None noted

6) Area Downstream of Dam

a. Downstream Hazard (No. of homes, highways, etc) Refer to Table 5.1 for a summary of downstream dwellings and highways

b. Seepage, unusual growth None noted

c. Evidence of movement beyond toe of Dam None noted

d. Conditions of Downstream Channel Erosion of right stream bank, should be regraded and slope protection provided

7) Spillway(s) (Including Discharge Conveyance Channel)

Principal Spillway: Drop inlet structure with outlet conduit to impact basin

Emergency Spillway: Vegetated earth, 200 ft. wide

a. General Good

b. Condition of Service Spillway Excellent

c. Condition of Auxiliary Spillway Good

d. Condition of Discharge Conveyance Channel Good with minimum erosion

8) Reservoir Drain/Outlet

Type: Pipe x Conduit _____ Other _____

Material: Concrete x Metal _____ Other _____

Size: 18" Ø Length 40±

Invert Elevations: Entrance 1354.5 Exit 1353.78

Physical Condition (Describe): _____ Unobservable x

Material: _____

Joints: _____ Alignment _____

Structural Integrity: _____

Hydraulic Capability: _____

Means of Control: Gate _____ Valve x Uncontrolled _____

Operation: Operable _____ Inoperable x Other _____

Present Condition (Describe): No handle

9) Structural

- a. Concrete Surfaces N/a
- b. Structural Cracking N/A
- c. Movement - Horizontal & Vertical Alignment (Settlement) N/A
- d. Junctions with Abutments or Embankments N/A
- e. Drains - Foundation, Joint, Face N/A
- f. Water Passages, Conduits, Sluices N/A
- g. Seepage or Leakage N/A
- h. Joints - Construction, etc. N/A
- i. Foundation N/A
- j. Abutments N/A
- k. Control Gates N/A
- l. Approach & Outlet Channels N/A

m. Energy Dissipators (Plunge Pool, etc) N/A

n. Intake Structures N/A

o. Stability N/A

p. Miscellaneous N/A

10) Appurtenant Structures (Power House, Lock, Gatchouse, Other)

a. Description and Condition None

APPENDIX B
ENGINEERING DATA

APPENDIX B

<u>TITLE</u>	<u>PAGE</u>
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Plan of Structural Works	B-5
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Cutoff Trench Excavation	B-7
Emergency Spillway	B-8
Fill Placement & Principal Spillway Excavation	B-9
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Plan Profile of Principal Spillway	B-12
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Tile Drainage Emergency Spillway	B-30

CONEWANGO CREEK WATERSHED PROJECT

FLOODWATER RETARDING DAM

SITE 9A

DRAINAGE AREA	3840 Acres
FLOOD STORAGE	612 Ac Ft
(TO EMERGENCY SPILLWAY CREST)	
WATER SURFACE AREA	9 Acres
(SEDIMENT POOL)	
HEIGHT OF DAM	⁴² 42 Feet
VOLUME OF FILL	174,319 Cu Yds

BUILT UNDER THE WATERSHED PROTECTION AND
FLOOD PREVENTION ACT

BY

CONEWANGO CREEK WATERSHED COMMISSION

WITH THE ASSISTANCE OF THE
SOIL CONSERVATION SERVICE

OF THE

U S DEPARTMENT OF AGRICULTURE

[SITE 9A]

INDEX

SHEET 1	COVER SHEET
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SHEET 3	PLAN OF STRUCTURAL WORKS
SHEET 4	LAYOUT DATA
SHEET 5	CUTOFF TRENCH EXCAVATION
SHEET 6	EMERGENCY SPILLWAY
SHEET 7	FILL PLACEMENT & PRINCIPAL SPILLWAY EXCAVATION
SHEET 8	DRAINAGE SYSTEM
SHEET 9	DRAINAGE SYSTEM
SHEET 10	PLAN PROFILE OF PRINCIPAL SPILLWAY
SHEET 11	OUTLET CHANNEL & RIPRAP DETAILS
SHEET 12	RISER STRUCTURAL DETAILS
SHEET 13	RISER STRUCTURAL DETAILS
SHEET 14	RISER STRUCTURAL DETAILS
SHEET 15	RISER STRUCTURAL DETAILS
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SHEET 17	48" DIA CONDUIT DETAILS
SHEET 18	RESERVOIR DRAIN CONDUIT DETAILS
SHEET 19	IMPACT BASIN DETAILS
SHEET 20	IMPACT BASIN DETAILS
SHEET 21	IMPACT BASIN DETAILS
SHEET 22	IMPACT BASIN DETAILS
SHEET 23	IMPACT BASIN DETAILS
SHEET 24	IMPACT BASIN GRATING
SHEET 25	RESERVOIR DRAIN INLET DETAILS
SHEETS 26	FENCING DETAILS — 27-28-29-30 LOGS OF TEST HOLES

HED PROJECT M

3840 Acres
612 Ac Ft
9 Acres
43
42 Feet
174,319 Cu Yds

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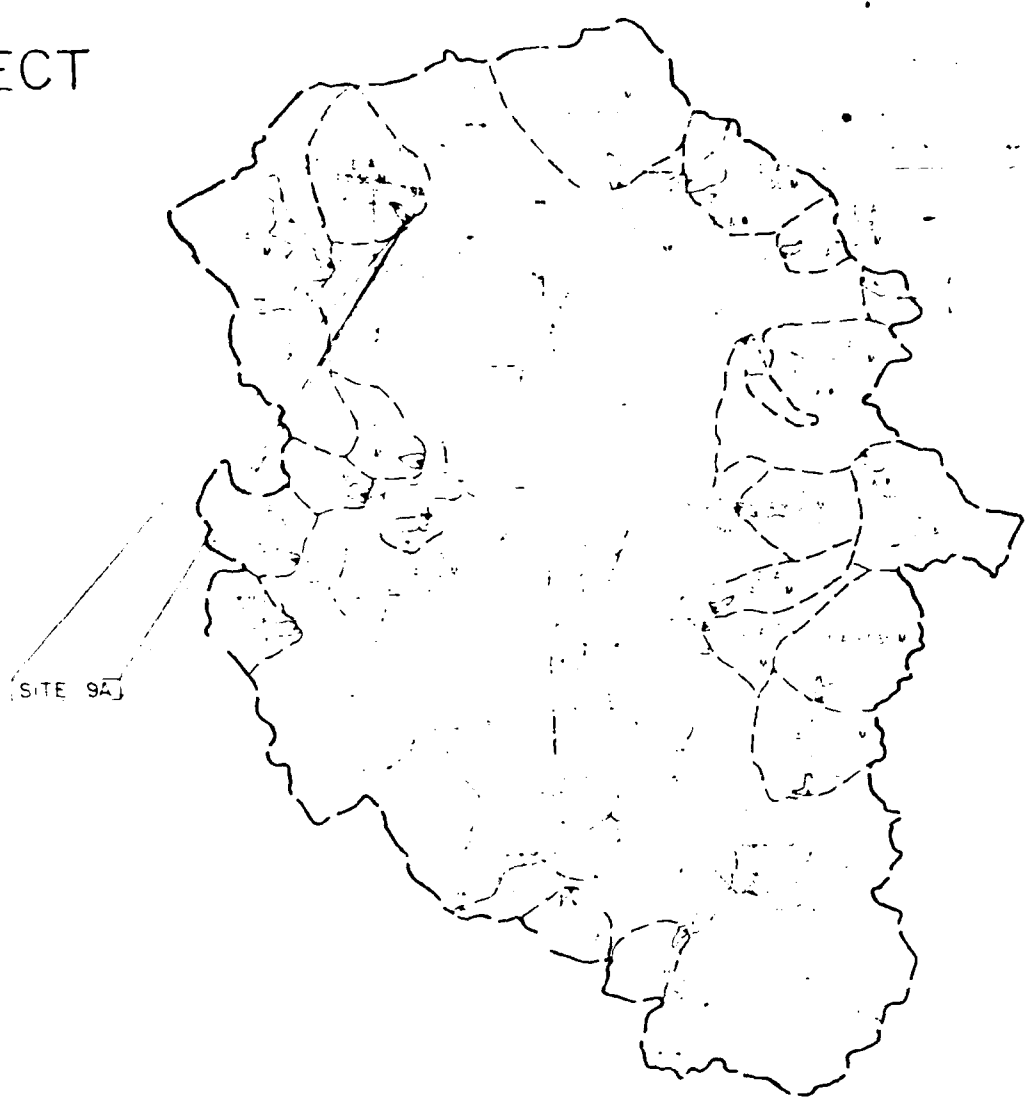
OMMISSION

RE

WAY EXCAVATION

AY
S

LOGS OF TEST HOLES



SITE 9A

AS BUILT
8/22/74

APRIL 72	SHEETS 2, 3, 5, 6, 6	11/15/72
DATE	NEW	APP'D
REVISION		
CONEWAGO CREEK WATERSHED PROJECT		
SITE 9A		
FLOODWATER RETARDING DAM		
CHAUTAUQUA COUNTY, NEW YORK		
COVER SHEET		
U. S. DEPARTMENT OF AGRICULTURE		
SOIL CONSERVATION SERVICE		
11/71	JOHN HESSEN	11/71
11/71	WILLIAM TURNER	11/71
		NY-216-P

2

B-2

CONSTRUCTION DETAILS

- 1 Areas under the dam and levee emergency spillway including 15 feet outside the cut slopes shall be cleared and grubbed. Limits of area to be cleared and grubbed to be staked in the field by the engineer.
- 2 The waste area and the area upstream from the dam and below elevation 126' E. or less, depending on the flood plain shall be cleared. Limits of area to be cleared shall be staked in the field by the engineer.
- 3 Depths and limits of borrow excavation shall be determined in the field by the engineer at the time of construction. At the completion of earth fill operations, the borrow area will be left gently sloping, generally smooth and free draining. Side slopes shall be no steeper than 3:1.
- 4 Bottom section of emergency spillway to be covered with 6" of topsoil from sta. 3+50 to approx. sta. 4+40.
- 5 Waste areas to be graded so as to prevent ponding.
- 6 The contractor will sprinkle or apply dust suppressors on Haul Roads and at the site as necessary to reduce pollution of the air.
- 7 All chemicals, fuels and lubricants will be located, stored, and disposed of in such a manner as to prevent their entry into streams, wells, or springs.
- 8 Sanitary facilities will be located in such a manner as to prevent pollution of springs, wells, and streams.
- 9 The abandoned road in the right abutment shall not be broken up except within the base area of the dam.
- 10 Diversions and rock-lined channel above the emergency spillway and borrow area shall be completed before borrow is taken from the emergency spillway or borrow area unless otherwise approved by the engineer.

SEDIMENT BASIN CONSTRUCTION DETAILS

- 1 Use earth fill requirements for zone 2 as described on sheet 7 except that class C compaction shall consist of a minimum of one pass of the equipment used to place the fill.
- 2 Use of other earth fill materials will be as approved by the engineer.
- 3 Sediment basin location and length as shown is approximate and will be staked in the field by the engineer.

NOTE
FOR PLAN VIEW OF
SEDIMENT BASIN
SEE SHEET 3

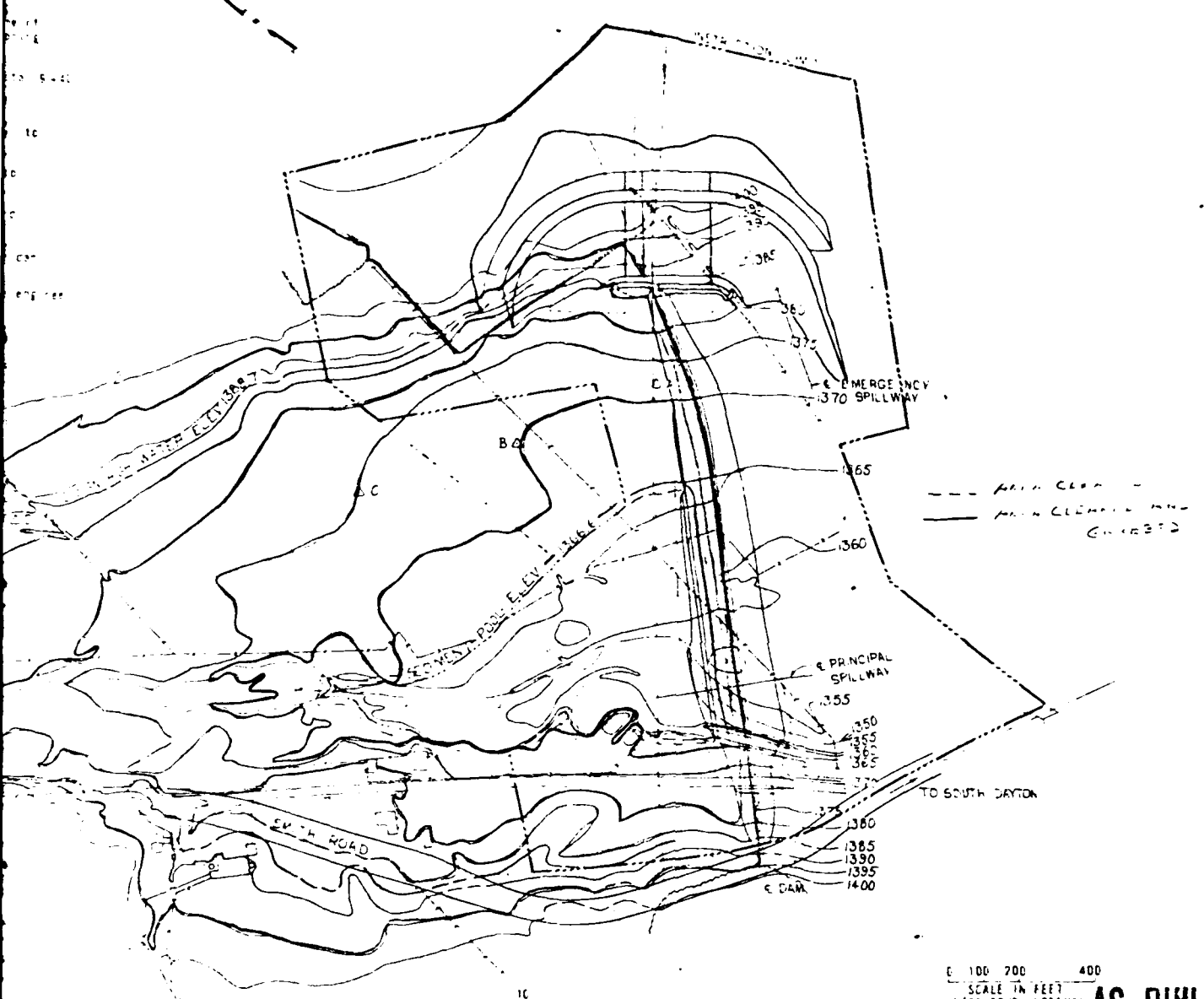
CONCRETE STEEL PLATE WELDED
TO END OF 6" DIA. PERFORATED PIPE

ELEV. 126'
6" DIA. PERFORATED PIPE

6" DIA.

15'-1"

FIELD
SEE SHEET 2



0 100 200 400
SCALE IN FEET
5' CONTOUR INTERVAL

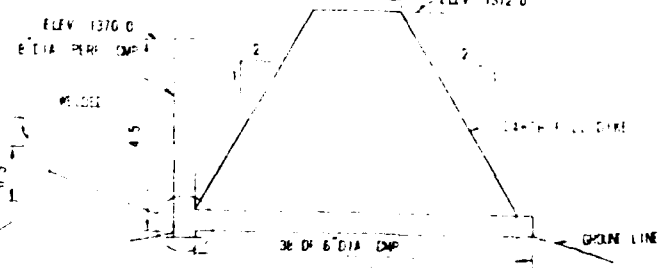
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APRIL 72 'SECMENT' BASIN EMERG. CRRY. BENCH
DATE ITEM REVISION

CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
PLAN OF STORAGE AREA

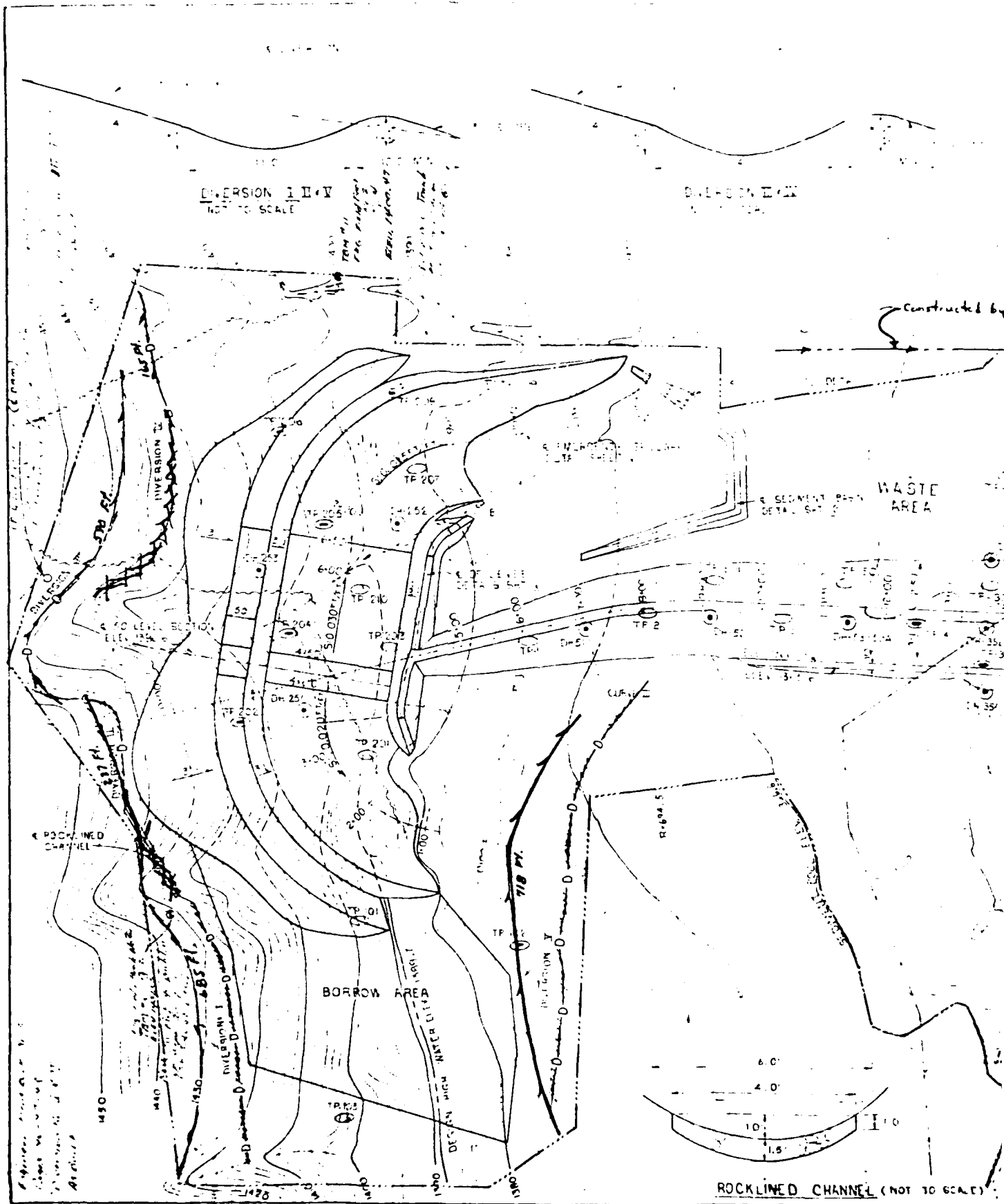
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

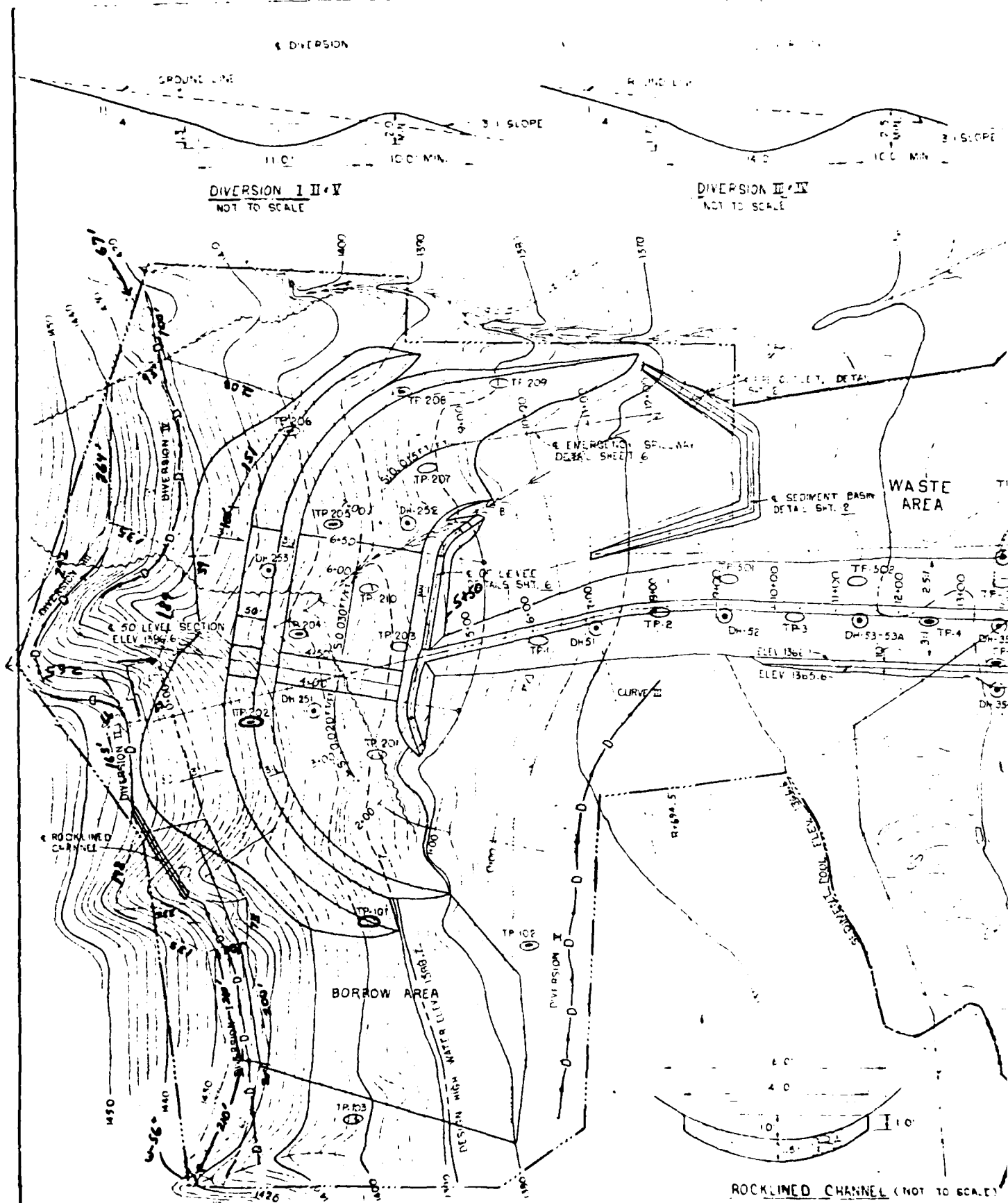
J. TOENNISSSEN	6/71
D. BURDICK	6/71
D. BURDICK	6/71
2 NY-2161-P	



SEDIMENT BASIN DETAILS
(NOT TO SCALE)

2





VERSION II-X
TO SCALE

LEGEND

- CONTOUR LINE
- - - 6" ELEVATION
- - - ELEVATION (FEET)
- BUILDING
- BENCH MARK
- DESIGN HIGH WATER
- SEDIMENT POOL
- TEST PIT (HIGHEST POINT)
- TEST PIT (LOWEST POINT)
- DRILL HOLE (LOGGED & SAMPLED)
- CONSTRUCTION LIMITS
- FENCE LINE (PLANNED)
- PAVED ROAD
- DIVERSION (PLANNED)
- POWER LINE

FOUNDATION EXCAVATION DETAILS

SHAPE RIGHT ABUTMENT TO SLOPES AS SHOWN ON SHEETS A AND B FOR DISTANCES 130 FT UPSTREAM AND 130 FT DOWNSTREAM FROM & OF DAM TO PROVIDE A SMOOTH, CLEAN SURFACE FOR PLACEMENT OF COMPACTED FILL

DIVERSION AND ROCKLINED CHANNEL CONSTRUCTION DETAILS

1. Final locations and slopes of diversions and rocklined channel to be staked in the field by the engineer at the time of construction
2. The 4:1 side slopes of the diversion may be steepened to reduce excavation in certain areas as directed by the engineer
3. The rock in the rocklined channel will be well graded between a minimum of 3 and a maximum of 18"

OF DAM, TOP WIDTH
60' ELEV. 1391.8
GATE

Survey Date 1973

BENCH MARK DESCRIPTION

BM#25 ELEV. 1357.18
TOP OF IRON RAILING NORTH SIDE
OF BRIDGE EAST CORNER

2' CONTOUR INTERVAL
0 50 100 200
SCALE IN FEET

AS BUILT

8/22/74

APRIL 72	SEDIMENT BASIN-EMERG	SPWY	BENCH	1/11/72
DATE	ITEM	REVISION	APP'D	

CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUE COUNTY, NEW YORK
PLAN OF STRUCTURAL WORKS
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

J. TOENNIESSEN 7/71
D. ANGELO 11/71

3A
NY-2161-P

B-5

LAYOUT DATA CURVE I

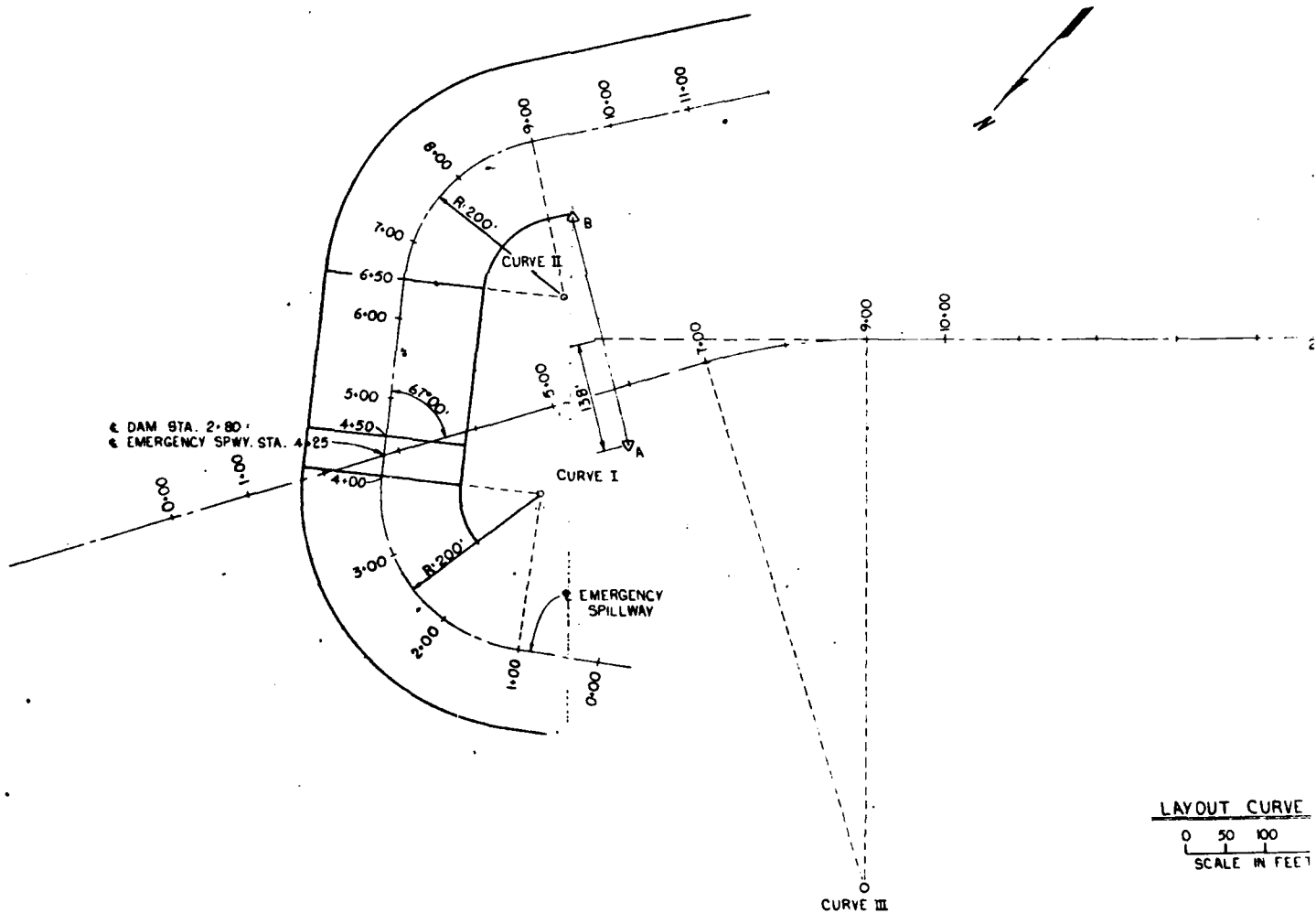
$\Delta = 85^\circ 37'$ $T = 186.34'$
 $R = 200'$ $E = 73.55'$
 $D = 88^\circ 39'$ $M = 53.67'$
 $L = 300'$

STATION	DEFLECTION	CHORD DIST.
1+00	0° 00'	—
1+50	7° 10'	49.87
2+00	14° 20'	
2+50	21° 29'	
3+00	28° 39'	
3+50	35° 49'	
4+00	42° 58.5'	

LAYOUT DATA CURVE II

$\Delta = 71^\circ 37'$ $T = 144.31'$
 $R = 200'$ $E = 46.63'$
 $D = 28^\circ 39'$ $M = 37.81'$
 $L = 250'$

STATION	DEFLECTION	CHORD DIST.
1+50	0° 00'	—
1+00	7° 10'	49.87
1+50	14° 20'	
2+00	21° 29'	
2+50	28° 39'	
3+00	35° 48.75'	



LAYOUT DATA CURVE II

$\Delta = 1^\circ 37'$ $T = 144.31'$
 $R = 200'$ $E = 46.63'$
 $D = 28^\circ 39'$ $M = 37.81'$
 $L = 250'$

LAYOUT DATA CURVE III

$\Delta = 16^\circ 30'$ $T = 100.6'$
 $R = 694.5'$ $E = 7.22'$
 $D = 8^\circ 15'$ $M = 7.15'$
 $L = 200.0'$

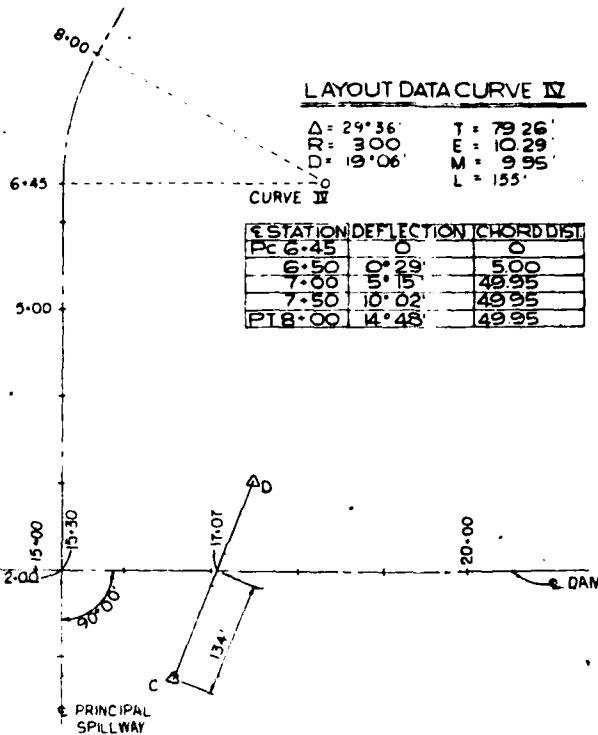
STATION	DEFLECTION	CHORD DIST.
1+50	0° 00'	
2+00	7° 10'	49.87
2+50	14° 20'	
3+00	21° 29'	
3+50	28° 39'	
4+00	35° 48.75'	

STATION	DEFLECTION	CHORD DIST.
9+00	0° 00'	
8+50	2° 04'	50.00
8+00	4° 08'	
7+50	6° 11'	
7+00	8° 15'	

LAYOUT DATA CURVE IV

$\Delta = 29^\circ 36'$ $T = 79.26'$
 $R = 300'$ $E = 10.29'$
 $D = 19^\circ 06'$ $M = 9.95'$
 $L = 155'$

STATION	DEFLECTION	CHORD DIST.
PC 6+45	0° 00'	0
6+50	0° 29'	5.00
7+00	5° 15'	49.95
7+50	10° 02'	49.95
PT 8+00	14° 48'	49.95



LAYOUT CURVE DATA

0 50 100 200
 SCALE IN FEET

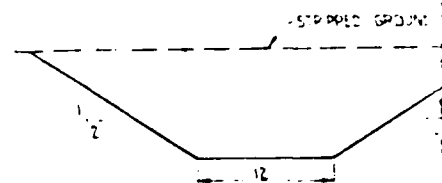
8/22/74
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CONEWANGO CREEK WATERSHED PROJECT
 SITE 9A
 FLOODWATER RETARDING DAM
 CHAUTAUQUA COUNTY, NEW YORK
 LAYOUT DATA

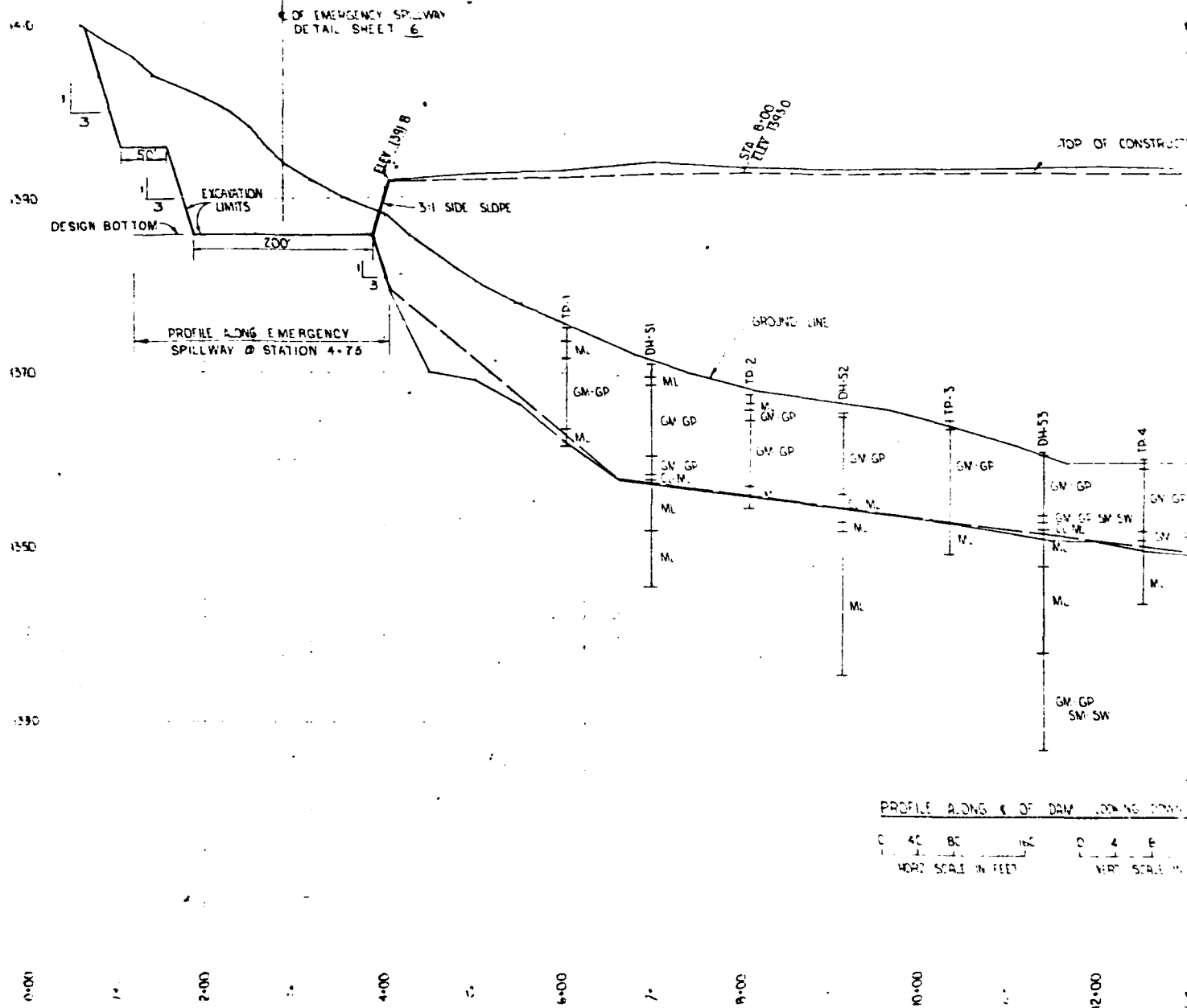
U. S. DEPARTMENT OF AGRICULTURE
 SOIL CONSERVATION SERVICE

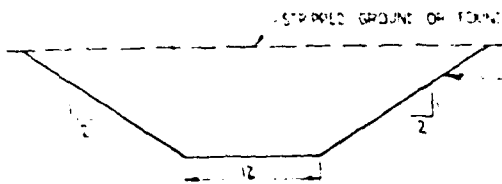
Designed	J. TOENNIESSEN	Date	9/71	Approved by	
Drawn	D. ANGELO	Date	9/71	Title	
Traced		Date		Sheet	4 of 4
Checked		Date		Drawing No.	NY-2161-P

B-6



CROSS SECTION OF CUTOFF TRENCH



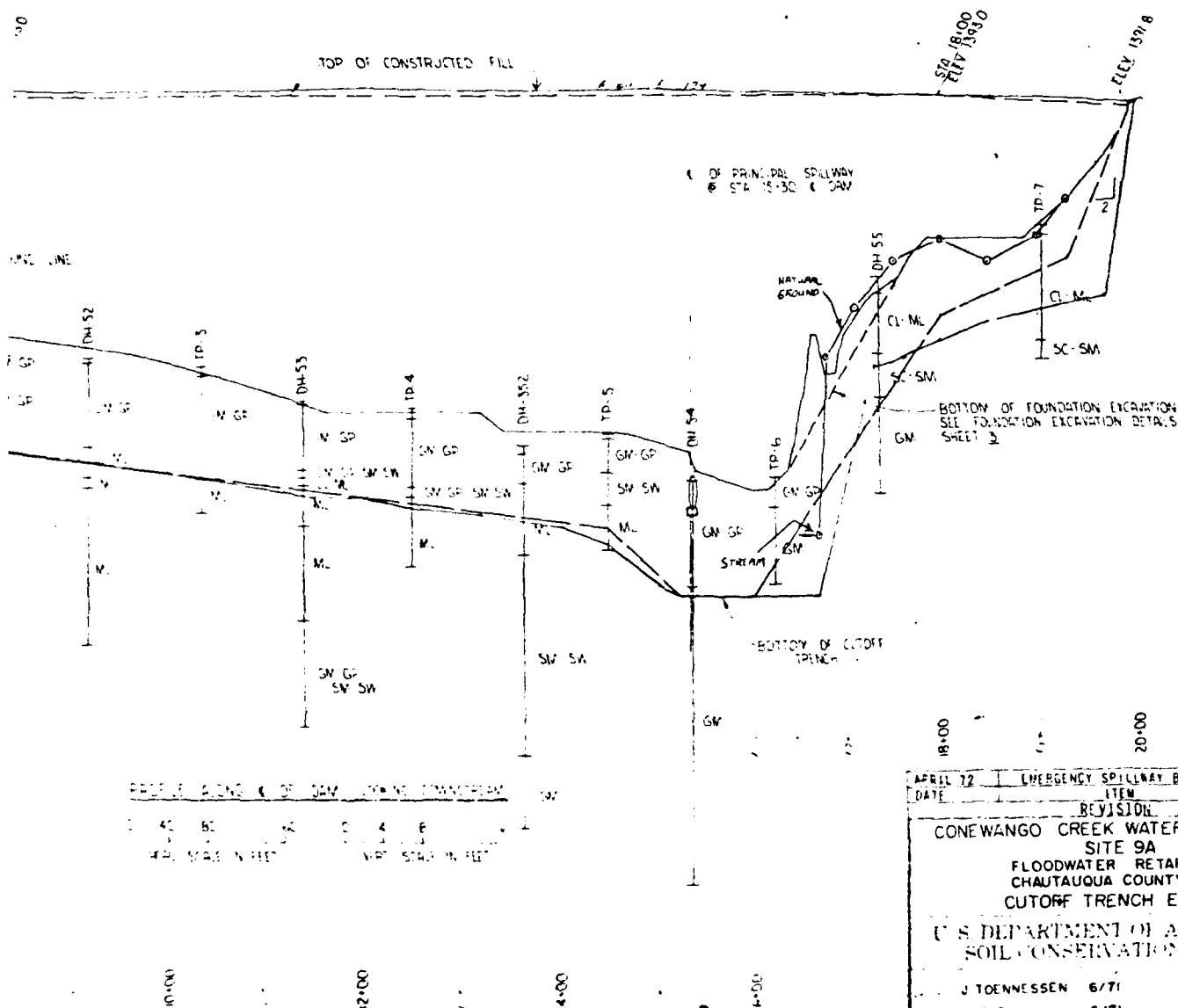


CROSS SECTION OF CUTOFF TRENCH

CONSTRUCTION DATA

FINAL DEPTH OF TRENCH TO BE DETERMINED BY THE ENGINEER AT THE TIME OF CONSTRUCTION

CUTOFF TRENCH SHALL BE THREE FEET WIDE AT THE TOP AND SHALL BE THREE FEET WIDE AT THE BOTTOM TO ONE (1) FOOT FROM STATION 15+20 TO STATION 15+40



AS BUILT
6/22/74

APRIL 72	EMERGENCY SPILLWAY BENCH
DATE	ITEM
REVISION	
CONEWANGO CREEK WATERSHED PROJECT	
SITE 9A	
FLOODWATER RETARDING DAM	
CHAUTAUQUA COUNTY NEW YORK	
CUTOFF TRENCH EXCAVATION	
U.S. DEPARTMENT OF AGRICULTURE	
SOIL CONSERVATION SERVICE	
J. TOENNESSEN	6/71
W. E. G.	6/71
NY-2161-P	

EMERGENCY SPILLWAY.
DESIGN BOTTOM

GROUNDLINE

3:1 SLOPE

EXCAVATION LIMITS

SECTION OF INSIDE LEVEE AT STA 4+50

TYPICAL FROM 50' UPSTREAM OF E OF LEVEE SECTION
TO 250' DOWNSTREAM OF E OF LEVEE SECTION

0 2 4 8 FT

VERTICAL SCALE

0 4 8 16 FT

HORIZONTAL SCALE

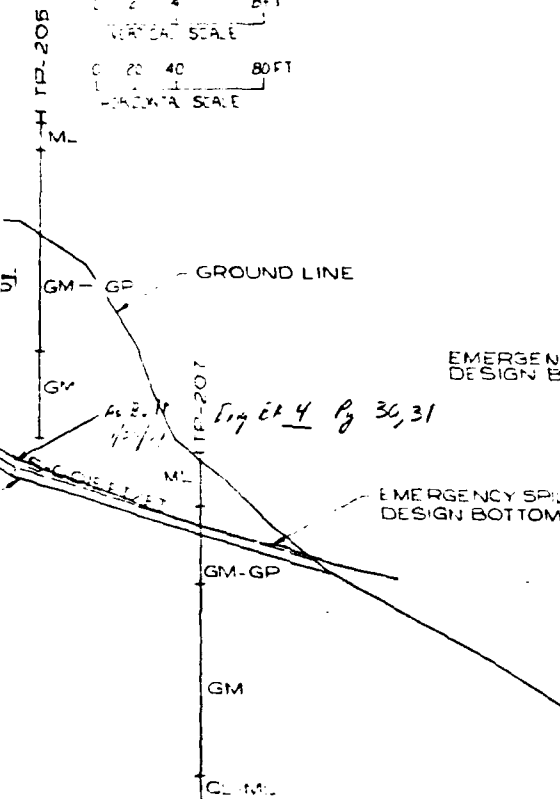
SECTION OF EMERGENCY SPILLWAY AT STA 4+25
FROM STATION 3+50 TO APPROX. STATION 12+00
N LIMITS TO DESIGN BOTTOM FROM APPROX
1+50 TO STATION 3+50

0 2 4 8 FT

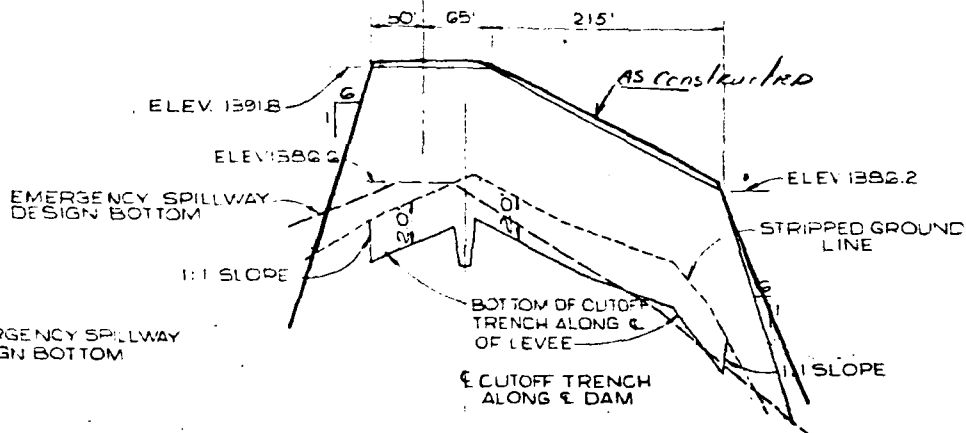
VERTICAL SCALE

0 20 40 80 FT

HORIZONTAL SCALE



EMERGENCY SPILLWAY LEVEL SECTION



0 2 4 8 FT

VERTICAL SCALE

0 40 80 160 FT

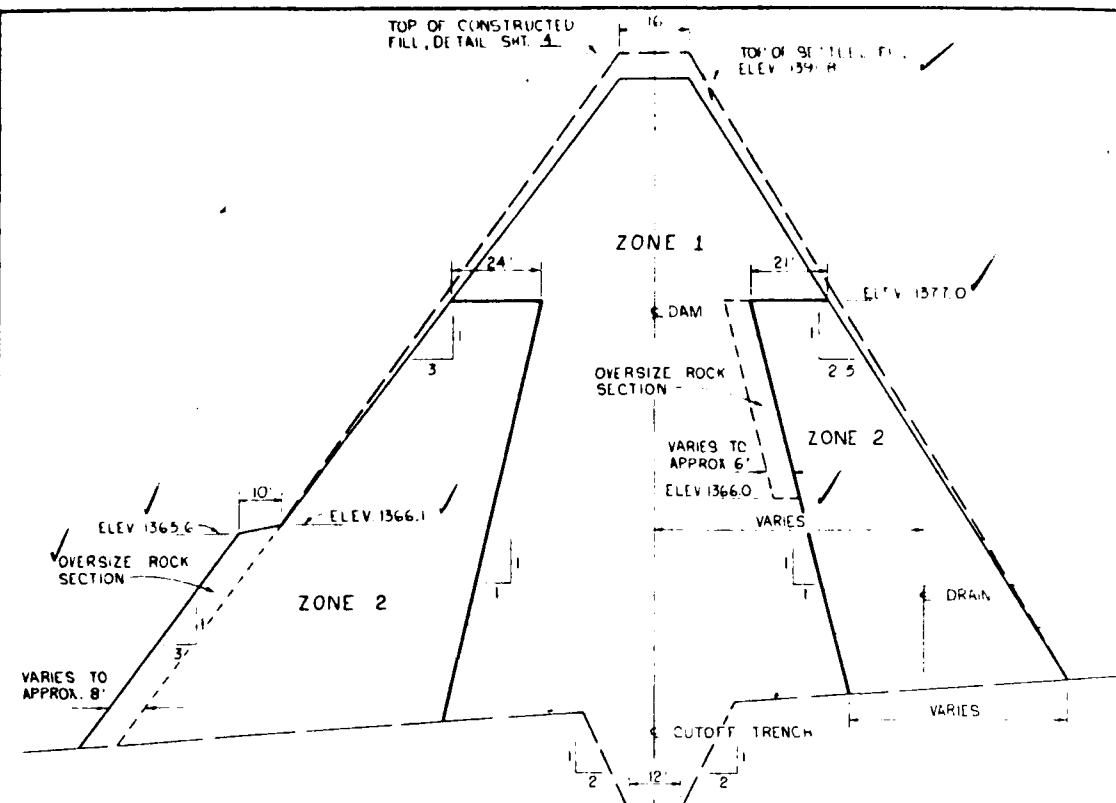
HORIZONTAL SCALE

PROFILE ALONG E OF LEVEE

1370
AS BUILT
8/22/77

DATE	REVISION	APPROVED
APRIL 72	EMERGENCY SPILLWAY BENCH	
	ITEM	
	REVISION	
CONEWANGO CREEK WATERSHED PROJECT		
SITE 9A		
FLOODWATER RETARDING DAM		
CHAUTAUQUA COUNTY NEW YORK		
EMERGENCY SPILLWAY		
U. S. DEPARTMENT OF AGRICULTURE		
SOIL CONSERVATION SERVICE		
J. TOENNIESSEN	11/71	
WILLIAM TURNER	11/71	
		NY-2161-P

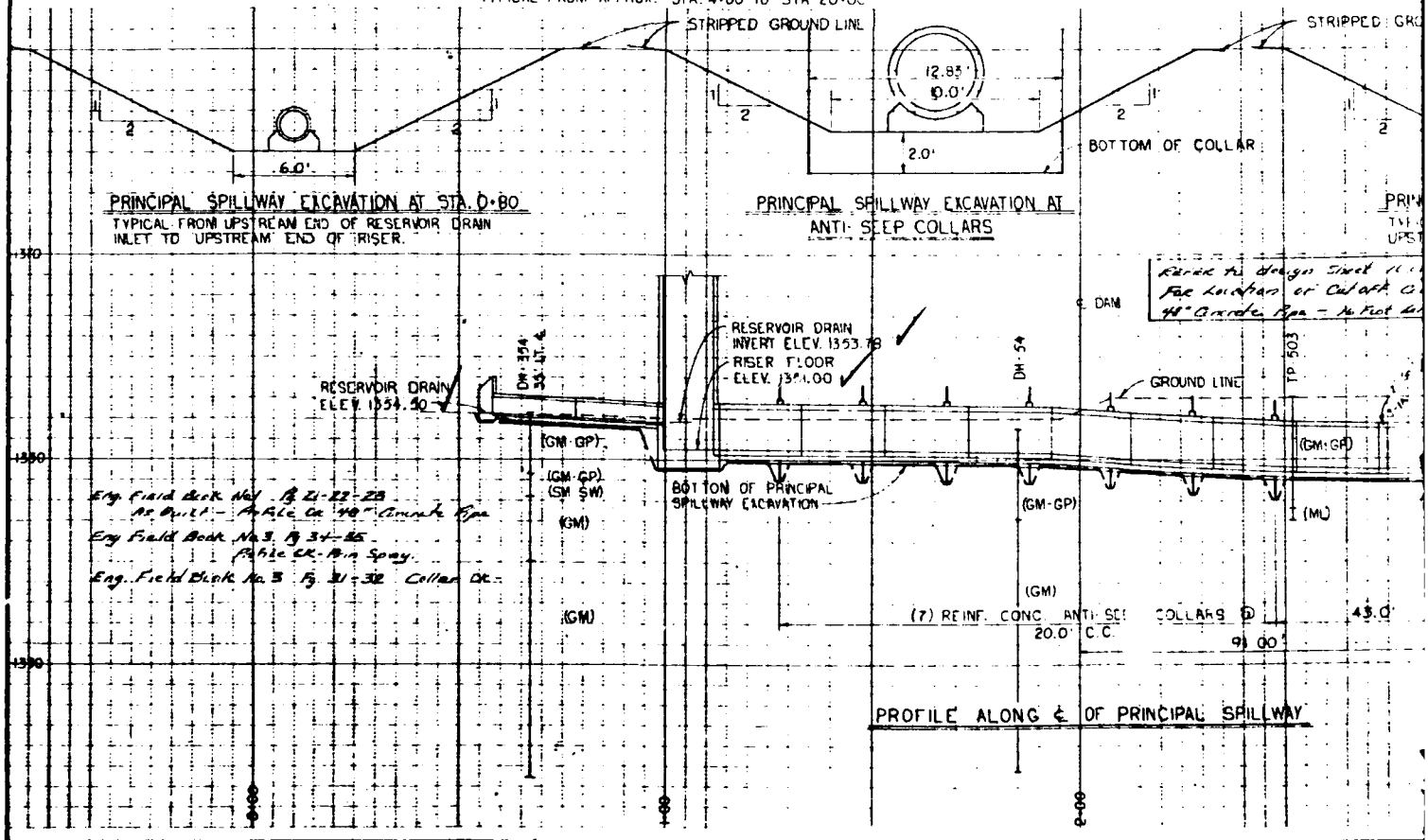
2



ZONE	MATERIAL
1	GLACIAL TILL RE TP 204 From 10 TP 206 From 9
2	ALLUVIAL & COLL REPRESENTED BY TP 7 From 1 TP 202 From 5 TP 205 From 1 TP 205 From 0

- 1/ The placement of
- 2/ a) Maximum rock
Plate Vibrators
b) Maximum rock
as shown on the
Maximum lift to
than 18' prior to
water content at
Thoroughly wet
a) Not more than
at the time of
b) Not so wet as
of equipment
5/ a) For typical
Use CLASS C
minimum of six
approved by the
- 1 Zone boundaries are
- 2 Material placed
be essentially fine
at the upstream side
Topsoil that is su
slopes of the earth

SECTION OF DAM @ STATION 15+00
TYPICAL FROM APPROX. STA. 4+00 TO STA. 20+00



PRINCIPAL SPILLWAY EXCAVATION AT STA. 0+80
TYPICAL FROM UPSTREAM END OF RESERVOIR DRAIN
INLET TO UPSTREAM END OF RISER.

PRINCIPAL SPILLWAY EXCAVATION AT
ANTI-SEEP COLLARS

Eng. Field Book No. 1, p. 21-22-23
As built - 1/4" scale 1/8" contour
Eng. Field Book No. 3, p. 34-35
Public Co. 1/4" scale
Eng. Field Book No. 3, p. 31-32 Collar Dr.

Check the design sheet for
the location of Collar Dr.
1/4" Contour Map - 1/4" scale

PROFILE ALONG C OF PRINCIPAL SPILLWAY

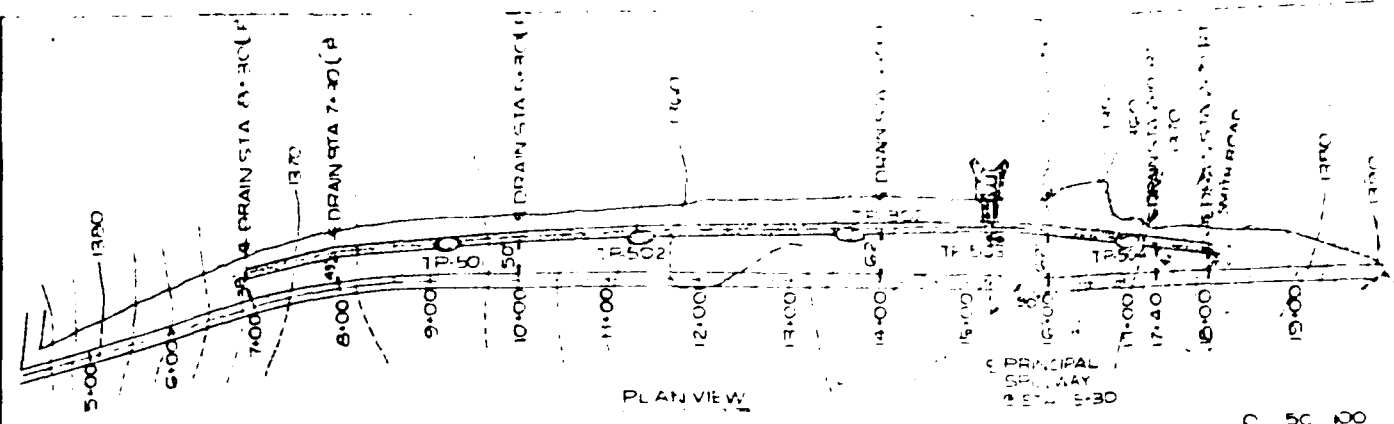
- | EARTH FILL REQUIREMENTS | | | | | | |
|-------------------------|--|------------------|-----------------------|-----------------------------------|---------------|--|
| ZONE | MATERIAL 1/ | MAX ROCK SIZE 2/ | MAX LIFT 3/ THICKNESS | MIN REQUIRED WATER CONTENT 4/ | COMPACTION 6/ | |
| | | | | | CLASS | DEFINITION |
| 1 | GLACIAL TILL REPRESENTED BY
TP 204 From 10'-0" to 14'-4" (SM)
TP 206 From 9'-0" to 16'-0" (ML) | 6" | 9" | 2 percentage points below optimum | A | 98 standard density by ASTM D 698 method A |
| 2 | ALLUVIAL & COLLUVIAL MATERIALS REPRESENTED BY
TP 7 From 1'-0" to 12'-0" (CL ML)
TP 202 From 5'-5" to 0'-0" (GM GP)
TP 205 From 1'-0" to 11'-0" (GM-GP)
TP 205 From 0'-5" to 1'-0" (CL) | 6" | 9" | wet 5/ | C | Four passes per layer of fill by a smooth wheel vibrating roller at least 72" wide weighing at least one ton (Static Service Weight) per foot of width and capable of exerting a dynamic impact of at least 20,000 pounds at the rate of at least 1,200 times per minute |

The drawing consists of several parts:

- Plan View (Top):** Shows the layout of the dam and spillways. Key features include:
 - STRIPPED GROUND LINE:** Indicated by dashed lines.
 - BOTTOM OF COLLAR:** Labeled on the left side.
 - PRINCIPAL SPILLWAY EXCAVATION AT STA. 2+00:** A circular structure with a diameter of 10.0'.
 - PRINCIPAL SPILLWAY EXCAVATION AT STA. 1+05:** A rectangular structure with a width of 1.0'.
 - SYMMETRICAL ABOUT C.C.:** A vertical line indicating the center of gravity.
- Profile View (Bottom):** Shows the cross-section of the dam and spillways. Key features include:
 - GROUND LINE:** Indicated by a dashed line.
 - DAM:** The main structure with a height of 43.0'.
 - SPILLWAY:** The structure on the right with a height of 43.0'.
 - INVERT ELEV. 1349.00:** Labeled on the spillway structure.
 - VERT. SCALE IN FEET:** A scale from 0 to 16.
 - HORIZ. SCALE IN FEET:** A scale from 0 to 40.
- Excavation Details (Right):** A section titled "PRINCIPAL SPILLWAY EXCAVATION DETAILS" stating: "Final depth of excavation to be determined by the engineer at the time of construction."
- AS BUILT (Bottom Right):** A stamp indicating the drawing is "AS BUILT" with the date "8/25/77".
- Project Information (Bottom Right):**
 - CONEWANGO CREEK WATERSHED PROJECT**
 - SITE 9A**
 - FLOODWATER RETARDING DAM**
 - CHAUTAUQUA COUNTY, NEW YORK**
 - FILL PLACEMENT & PRINCIPAL SPWY EXCAV.**
 - U. S. DEPARTMENT OF AGRICULTURE**
 - SOIL CONSERVATION SERVICE**
- Design and Drawing Information (Bottom Right):**
 - Designed by:** TOENNIESSEN
 - Date:** 9/71
 - Drawn by:** D. Angelo
 - Title:** 11-71
 - Traced by:**
 - Sheet:** 7 of 30
 - Drawing No.:** NY-2161-P

**CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
FILL PLACEMENT & PRINCIPAL SPWY EXCAVA
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE**

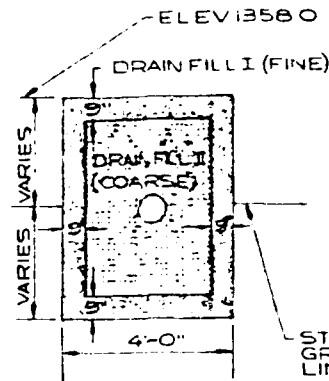
Date		Approved by	
Designed	J TOENNIESSEN	9-71	Title
Drawn	D. Angelo	11-71	Title
Traced			
Checked		Sheet	Drawing No
		No. 7	
		of 30	NY-2161-P



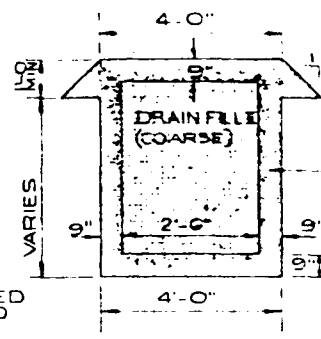
PLAN VIEW

PRINCIPAL SPILLWAY
P-504
P-505

C 50 100
SCALE IN FEET



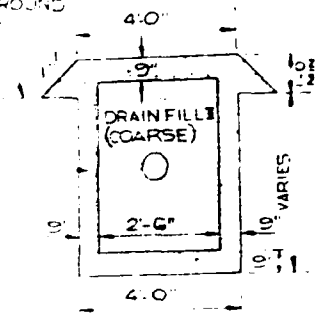
SECTION B-B



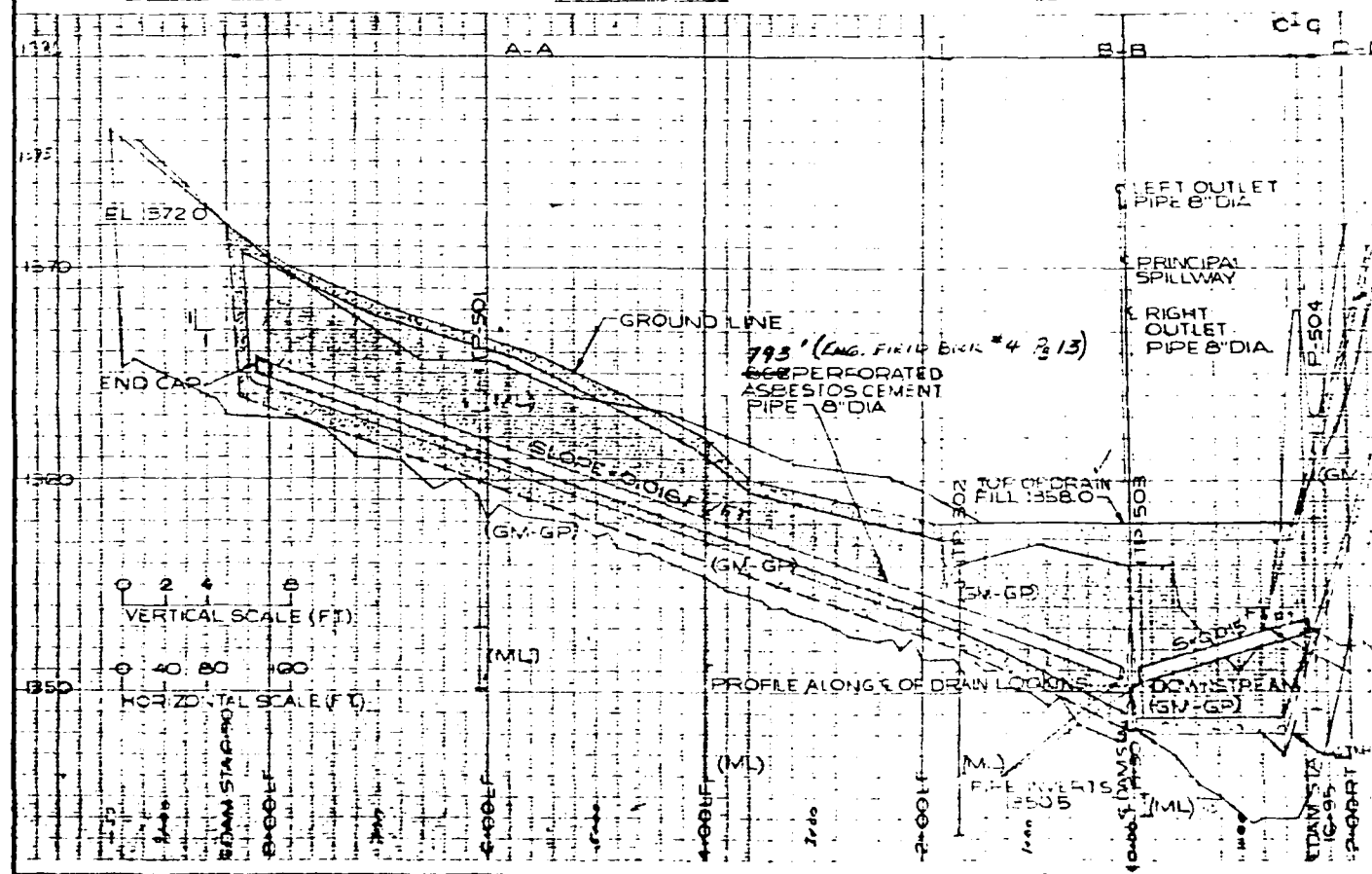
SECTION D-D

STRIPPED GROUND LINE OR FOUNDATION EXCAVATION LINE

DRAIN FILL I (FINE)



SECTION A-A
C-C



DRAINAGE SYSTEM DETAILS

PERFORATED DRAIN PIPE SHALL CONFORM TO A.S.T.M. A 131 AND SHALL BE 8" DIA PRESSURE PIPE LINED WITH 1/2" THICK PROFILE AT THE BOTTOM OF ALL EXCAVATION. ALL DIMENSIONS ARE ONLY APPROXIMATE. THE REQUIRED FINISH SHALL BE ESTABLISHED IN THE FIELD AT THE TIME OF CONSTRUCTION BY THE ENGINEER.

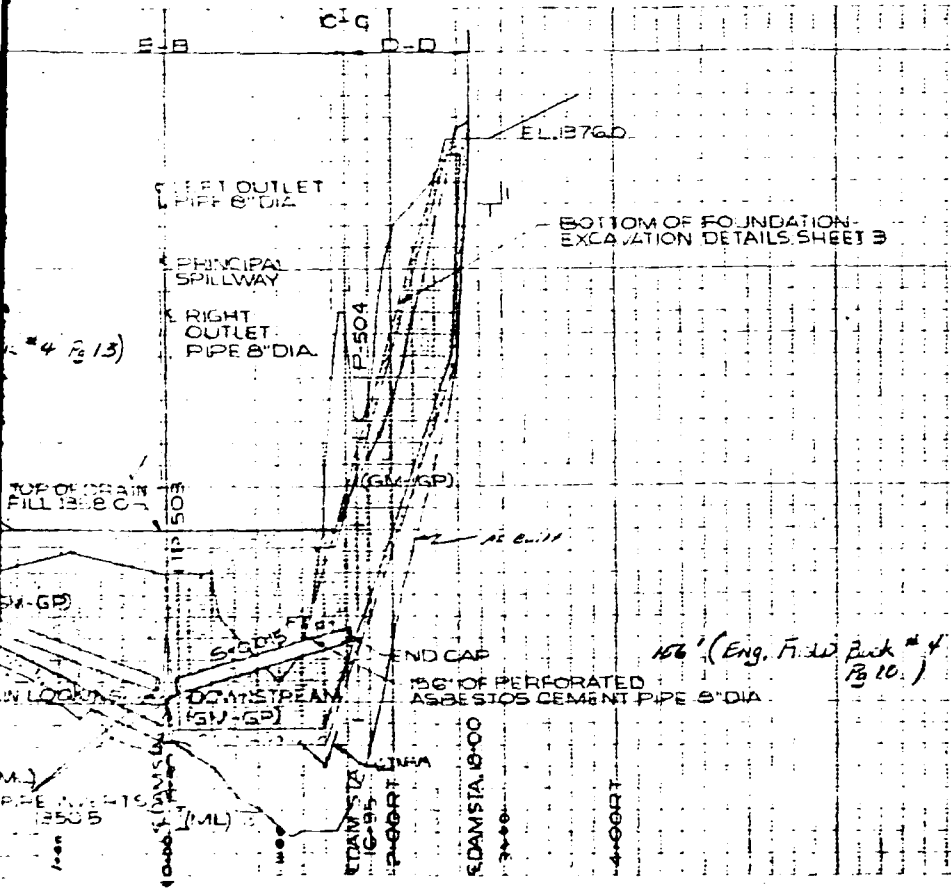
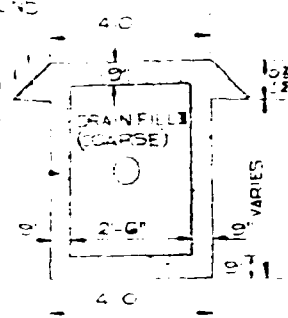
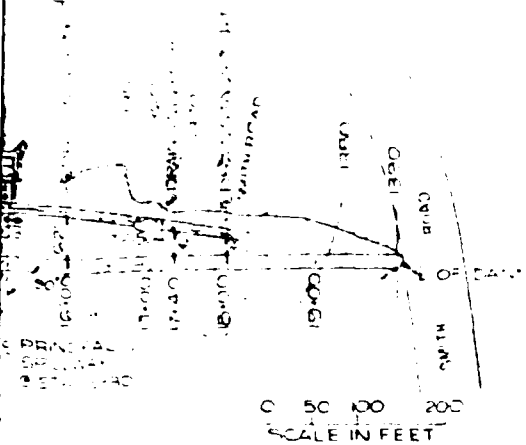
QUANTITY SUMMARY

- 925 = 20 YDS DRAIN FILL I (FINE)
- 847 = 20 YDS DRAIN FILL II (COARSE)
- 1063 = 100 FT STRAIGHT SECTION OF PERFORATED ASBESTOS CEMENT PIPE (8" DIA)
- 2 END CAPS
- 1 90° ELBOWS (8" DIA CAST IRON)
- 2 45° ELBOWS (8" DIA CAST IRON)

GRAIN SIZE DESCRIPTION FOR DRAIN FILL

DRAIN FILL I (FINE) SHALL MEET THE GRADATION OF A.S.T.M. C 33-67 FOR FINE AGGREGATE. IN ADDITION, THE PERCENTAGE OF MATERIAL IN DRAIN FILL I FINER THAN A # 200 SIEVE SHALL NOT BE MORE THAN THREE (3) PERCENT.

DRAIN FILL II (COARSE) SHALL MEET THE GRADATION OF N.Y.S. DOT COARSE AGGREGATE #1. IN ADDITION, THE PERCENTAGE OF MATERIAL IN DRAIN FILL II FINER THAN A # 200 SIEVE SHALL NOT BE MORE THAN THREE (3) PERCENT.

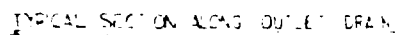


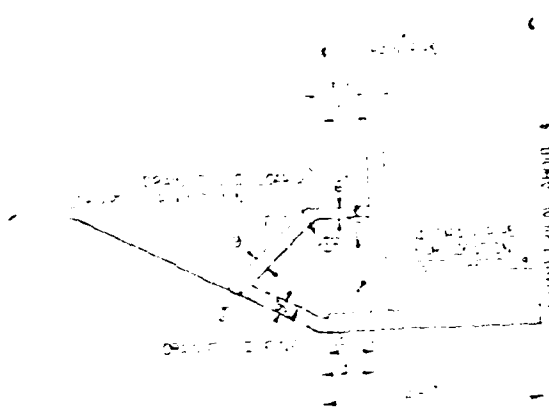
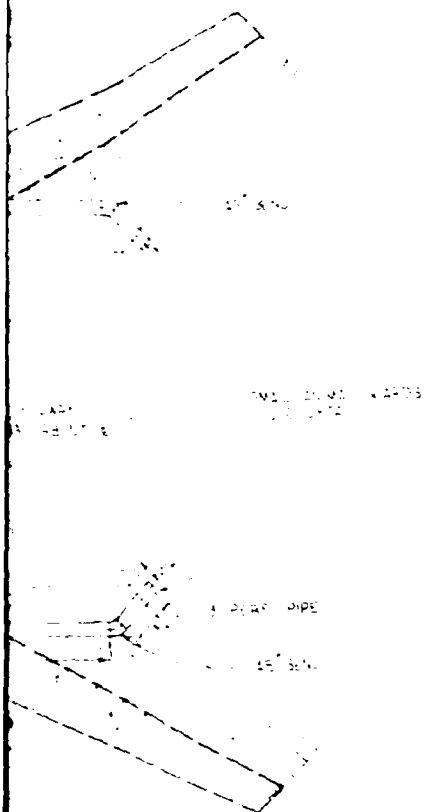
9/22/74
AS BUILT

CONE WANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
DRAINAGE SYSTEM

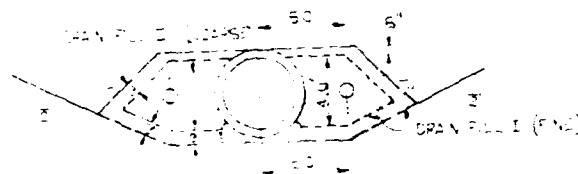
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

Designed by J. TOENNIESSEN	Date 9/71	Approved by WILLIAM TURNER	Date 9/71
Title NY-216-P		Scale 1" = 10'	





SECTION AA



SECTION BB

8" PRECASTED
ASBESTOS CEMENT
PIPE



8" ASBESTOS CEMENT PIPE

15' DRAIN

WATER GATE BOLT WELT
WASHER 1/2"



15" WOVEN WIRE MESH
GALVANIZED NO. 2 GAGE

DETAIL OF WALL AND WALL SCREEN & OUTLET OF DRAIN PIPE
NOT TO SCALE

AS BUILT
8/22/77

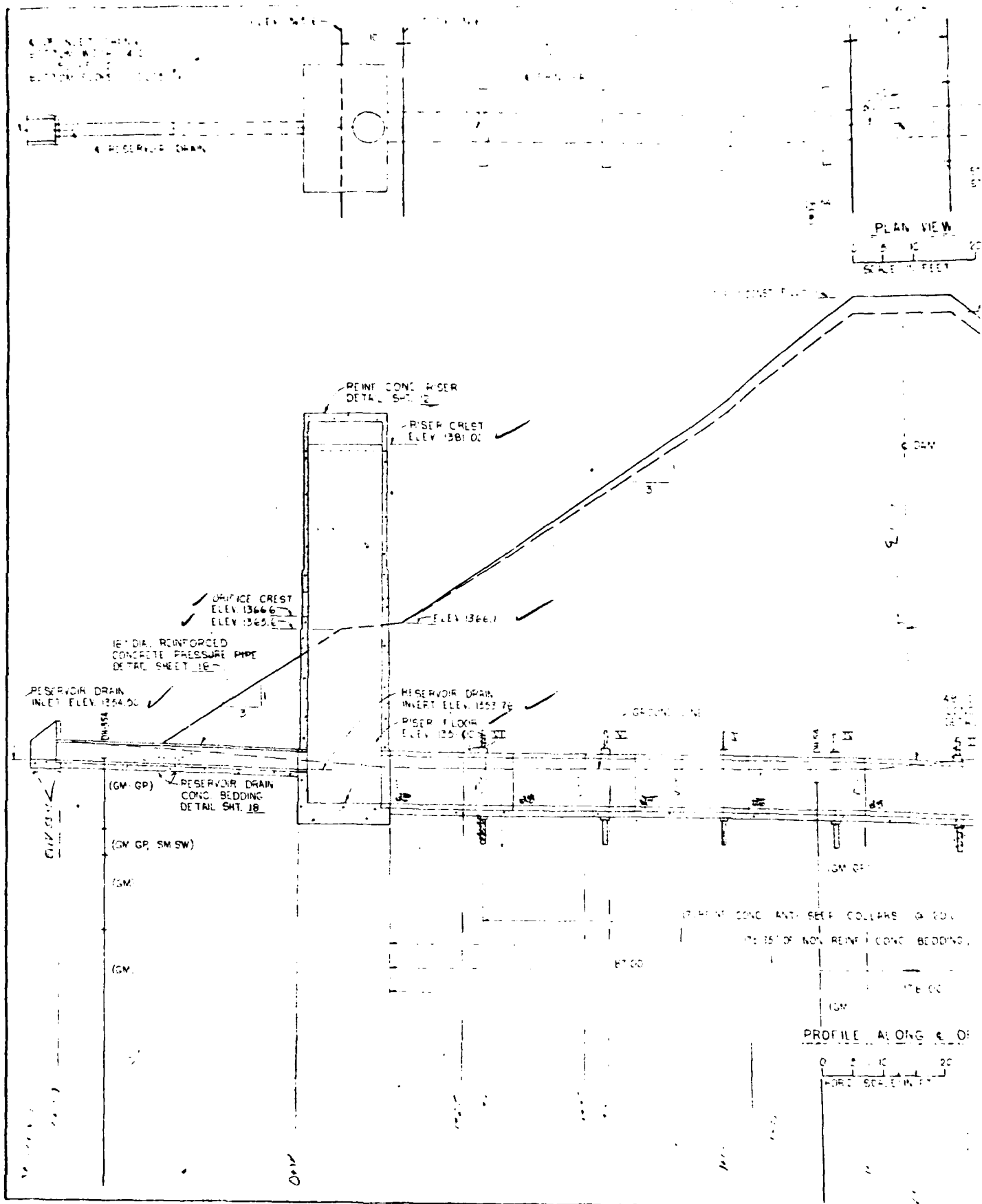
CHENANGO CREEK WATERSHED PROJECT
SITE 3A
FLOODWATER RETARDING DAM
CHAUTAUQUE COUNTY, NEW YORK
DRAINAGE SYSTEM
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

DATE: 9/7/77
BY: [signature]

IN-10-10

B-II

2



PLAN VIEW

SCALE 1" = 20'

WHEN PIPE IS SUPPLIED IN LENGTHS OTHER THAN SHOWN, THE ENGINEER WILL PROVIDE THE CONTRACTOR WITH A REVISION OF THIS SHEET SHOWING ORDER OF INSTALLATION AND PIPE INVERT ELEVATIONS.

COLLAR	DIST. FROM OUTLET	INVERT OF PIPE
I	43	1349.32
II	61	1349.72
III	78	1350.17
IV	103	1350.72
V	123	1350.91
VI	143	1350.96
VII	166	1350.98

ABOVE DIMENSIONS FOR LENGTHS OF PIPE ARE BASED ON NOMINAL LENGTHS AND DO NOT INCLUDE CREEP.

COLLAR	DIST. FROM OUTLET	INVERT OF PIPE
I	43	1349.32
II	61	1349.72
III	78	1350.17
IV	103	1350.72
V	123	1350.91
VI	143	1350.96
VII	166	1350.98

PROFILE ALONG & OF PRINCIPAL SPILLWAY

SCALE 1" = 20' HORIZ. SCALE 1" = 10' VERT.

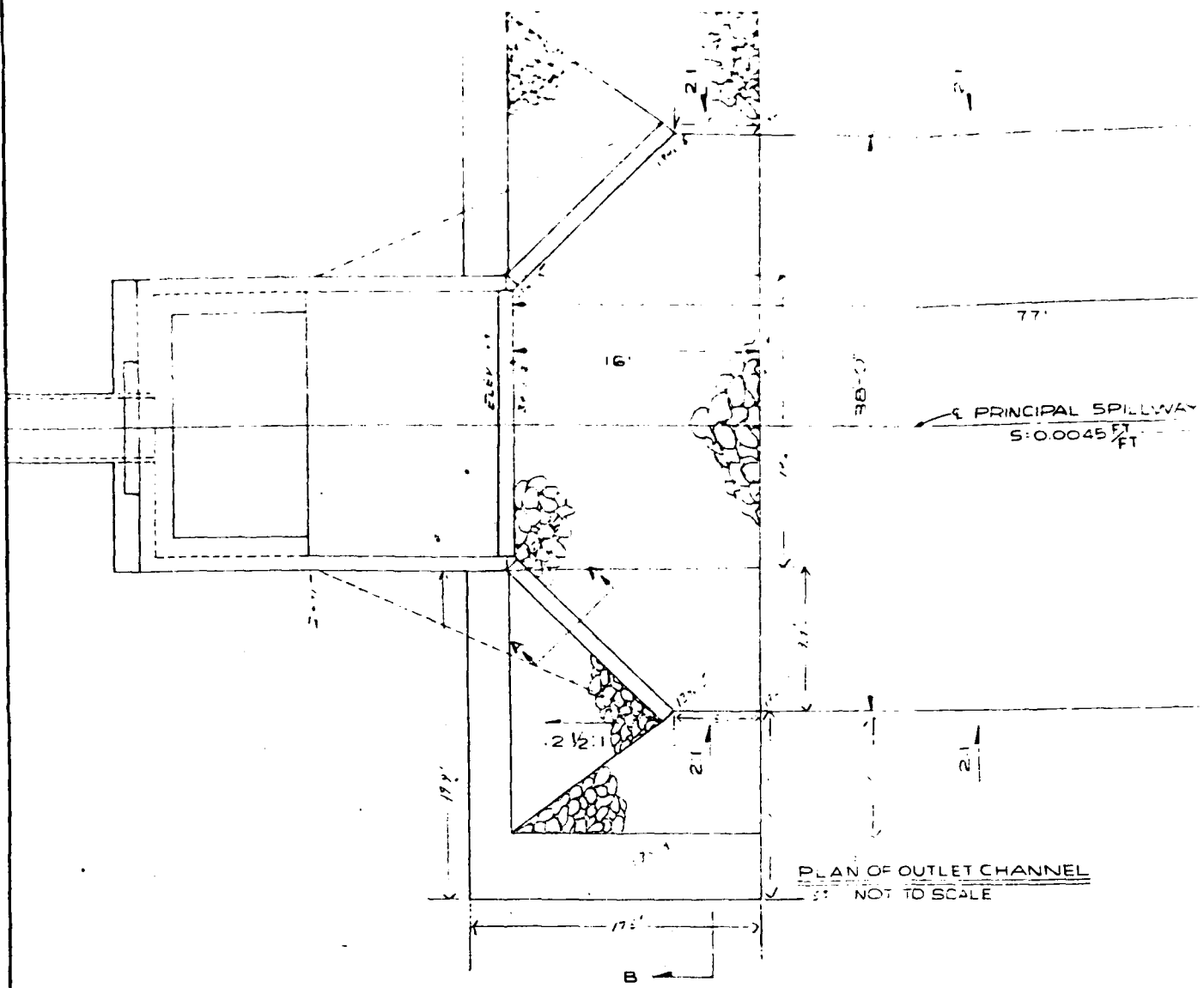
AS BUILT
8/22/79

CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY NEW YORK
PLAN PROFILE OF PRINCIPAL SPILLWAY
U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

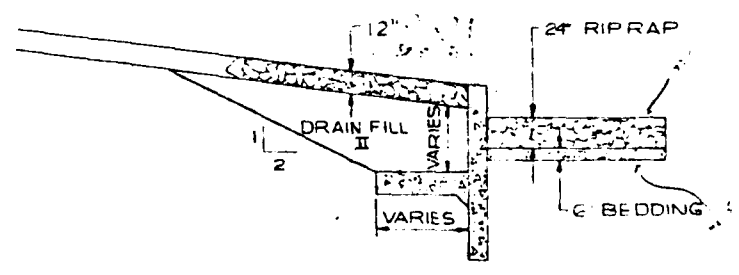
J. TOENNISSSEN 9/7/79
D. J. ANGELO 9/7/79

NY-2161-P

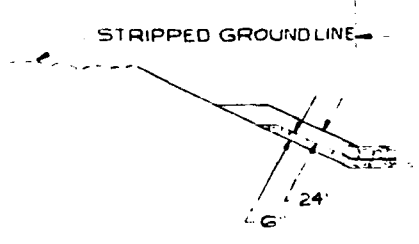
B-12



PLAN OF OUTLET CHANNEL
 NOT TO SCALE



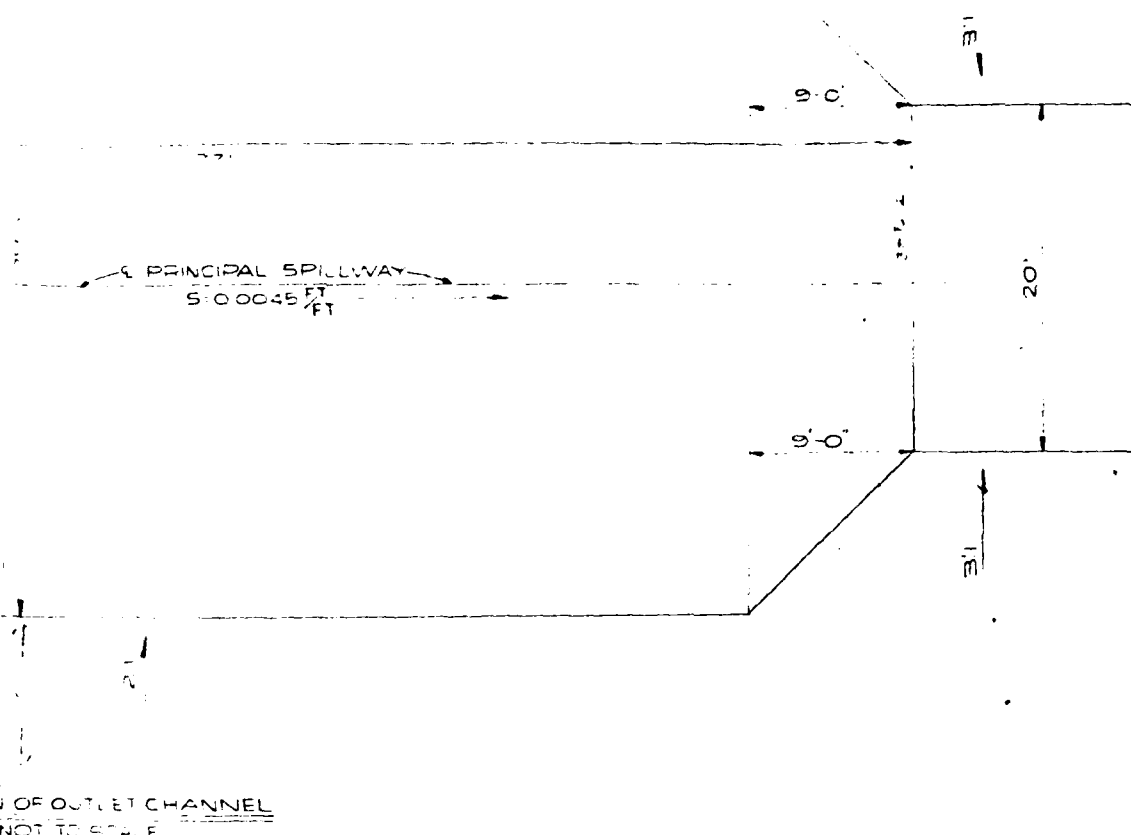
SECTION AA
 NOT TO SCALE



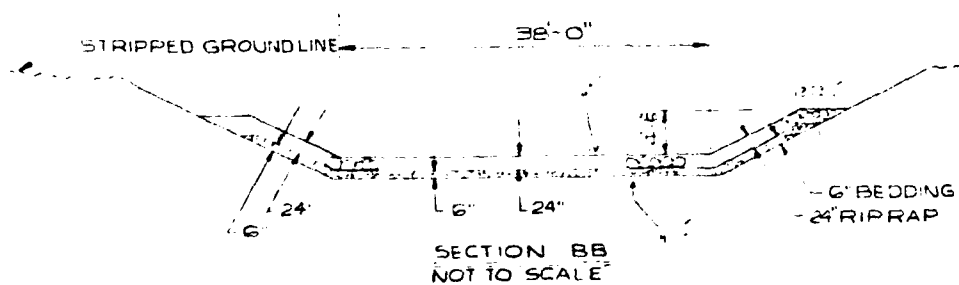
LOOSE ROCK RIP RAP SHALL BE GRADED FROM A MAXIMUM SIZE OF 10" TO A MINIMUM SIZE OF 2 1/2". 75% OF 20'S SHALL BE LESS THAN 6" (10 LB) A MAXIMUM OF 60'S SHALL BE LESS THAN 12" (60 LB)

BEDDING DETAILS

BEDDING SHALL MEET THE SPECIFICATION OF NYS DEPT OF TRANSPORTATION COARSE AGGREGATE # 1



OF OUTLET CHANNEL
NOT TO SCALE

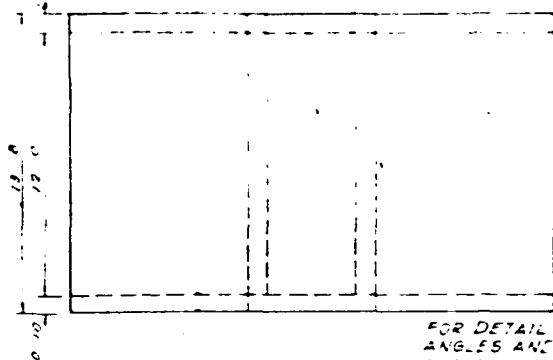


SECTION BB
NOT TO SCALE

2

8/22/74
AS BUILT

CONEWANGO CREEK WATERSHED SITE 9A FLOODWATER RETARDING DAM CHAUTAUQUA COUNTY, NEW YORK OUTLET CHANNEL AND RIPRAP DETAILS	
U. S. DEPARTMENT OF AGRICULTURE SOIL CONSERVATION SERVICE	
Designed: J. D. TOENNISSSEN	Date: 8-71
Drawn: W. TURNER	Date: 8-71
Checked:	Date:
Project:	NY-2161-P

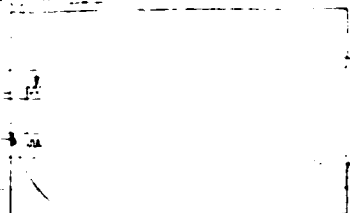


TOP PLAN

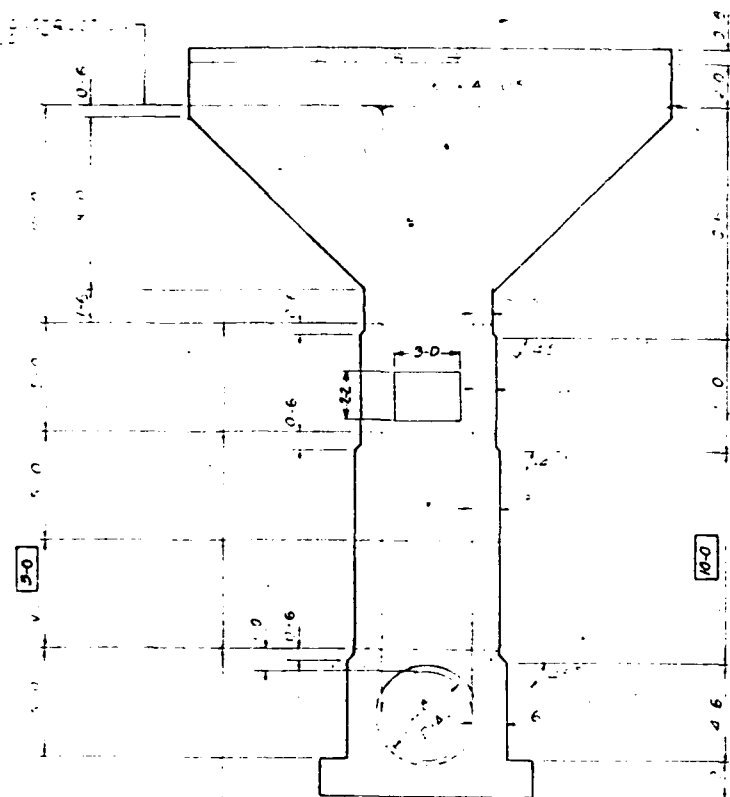
FOR DETAIL OF TRASH-RACK
ANGLES AND GRATINGS
SEE SHEET 16

MANHOLE ASSEMBLY DETAILS
CONCRETE MANHOLE RINGS
MINIMUM SIZE 30" DIA.
NATIONAL FOUNDRY COMPANY
MODEL R-64E1-MH 1/2" 11"
STAINLESS STEEL SCREENS OR
APPROVED EQUIVALENT

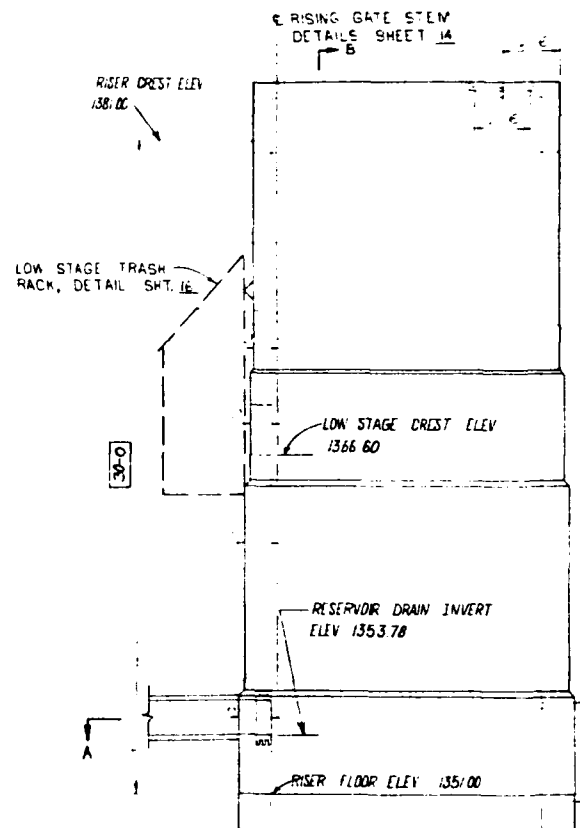
WALL FITTING SEE DETAIL SHEET 16



BELL WALL FITTING
DETAIL SHEET 16



SECTION B-B



ERISING GATE STEM
DETAILS SHEET 14

RISER DREST ELEV
1381.00

LOW STAGE TRASH
RACK, DETAIL SHT. 16

LOW STAGE DREST ELEV
1366.60

RESERVOIR DRAIN INVERT
ELEV 1353.78

RISER FLOOR ELEV 1351.00

DATE 2-28-68
SHEET 1 OF 4

STANDARD COVERED RISER			
MANHOLE RINGS	1/2" - 4000 PS	1/2" - 1600 PS	
MANHOLE RINGS	1/2" - 8	1/2" - 2000 PS	
STANDARD DREST NO	ES 3040 3050		
DATE	2-28-68	SHEET	1 OF 4

DRAFTED BY
LOEWER AND ASSOCIATES
ARCHITECTS & ENGINEERS
372C FARRAGUT AVE KENSINGTON, MD

0 2 4 6
SCALE IN FEET

BELL WALL FITTING
DETAIL SHEET E

SECTION A-A

CRABING GATE STEM
DETAIL SHEET 1A

LOW STAGE DREST ELEV
1366.60

RESERVOIR DRAIN INVERT
ELEV 1353.78

PSR FLOOR ELEV 1351.00

SIDEWALL ELEVATION

STEEL SCHEDULE

MARK	SIZE	QUANTITY	LENGTH	TYPE	TOTAL LENGTH
71	5	24	5.6	1	134.4
72	5	8	12.3	1	98.4
73	5	4	8.6	1	34.4
74	5	4	3	1	12.0
75	5	4	6.0	1	24.0
76	5	4	4.9	1	19.6
77	5	4	3.6	1	14.4
78	5	4	14.0	19	56.0
79	5	16	12.9	1	206.4
710	5	4	12.9	1	51.6
711	5	2	4.9	1	9.8
712	5	2	5.9	1	11.8
713	5	2	8.3	1	16.6
714	5	2	10.9	1	21.8
715	5	2	13.3	1	26.6
716	5	2	15.9	1	31.8
717	5	2	18.3	1	36.6
718	5	2	20.9	1	41.8
719	5	20	5.9	1	118.0
720	5	10	12.3	1	123.0
721	5	4	9.3	1	37.2
722	5	4	6.0	1	24.0
723	5	4	5.9	1	23.6
724	5	4	5.9	1	23.6
725	5	4	2.3	1	9.2
726	5	4	3.6	1	14.4
727	5	4	4.0	19	76.0
728	5	32	11.3	21	361.6
729	5	16	11.0	24	176.0
730	5	2	8.3	1	16.6
731	5	2	6.3	1	12.6
732	5	2	11.3	1	22.6
733	5	2	13.9	1	27.8
734	5	2	16.3	1	32.6
735	5	2	18.9	1	37.8
736	5	2	21.3	1	42.6
737	5	4	21.3	1	85.2
738	5	4	21.3	1	85.2
739	5	30	12.9	1	387.0
740	5	5	9.3	1	46.5
741	5	11	21.3	1	234.3
742	5	4	9.3	1	37.2
743	5	11	21.3	1	234.3
744	5	4	9.3	1	37.2
745	5	36	9.3	21	334.8
746	5	2	11.6	21	23.2
747	5	2	2.9	21	5.8

71	5	24	5.6	1	134.4
72	5	8	12.3	1	98.4
73	5	4	8.6	1	34.4
74	5	4	3	1	12.0
75	5	4	6.0	1	24.0
76	5	4	4.9	1	19.6
77	5	4	3.6	1	14.4
78	5	4	14.0	19	56.0
79	5	16	12.9	1	206.4
710	5	4	12.9	1	51.6
711	5	2	4.9	1	9.8
712	5	2	5.9	1	11.8
713	5	2	8.3	1	16.6
714	5	2	10.9	1	21.8
715	5	2	13.3	1	26.6
716	5	2	15.9	1	31.8
717	5	2	18.3	1	36.6
718	5	2	20.9	1	41.8
719	5	20	5.9	1	118.0
720	5	10	12.3	1	123.0
721	5	4	9.3	1	37.2
722	5	4	6.0	1	24.0
723	5	4	5.9	1	23.6
724	5	4	5.9	1	23.6
725	5	4	2.3	1	9.2
726	5	4	3.6	1	14.4
727	5	4	4.0	19	76.0
728	5	32	11.3	21	361.6
729	5	16	11.0	24	176.0
730	5	2	8.3	1	16.6
731	5	2	6.3	1	12.6
732	5	2	11.3	1	22.6
733	5	2	13.9	1	27.8
734	5	2	16.3	1	32.6
735	5	2	18.9	1	37.8
736	5	2	21.3	1	42.6
737	5	4	21.3	1	85.2
738	5	4	21.3	1	85.2
739	5	30	12.9	1	387.0
740	5	5	9.3	1	46.5
741	5	11	21.3	1	234.3
742	5	4	9.3	1	37.2
743	5	11	21.3	1	234.3
744	5	4	9.3	1	37.2
745	5	36	9.3	21	334.8
746	5	2	11.6	21	23.2
747	5	2	2.9	21	5.8

8/22/74 AS BUILT

QUANTITIES

STEEL 3186.0 LBS
3323 LBS
15482.0 LBS

CONCRETE 69.0 CUBIC YDS.

LENGTH OF 6 BAR (354) + LENGTH OF BARS 4 THROUGH 21

CONEWANGO CREEK WATERSHED PROJECT

SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
RISER STRUCTURAL DETAILS

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

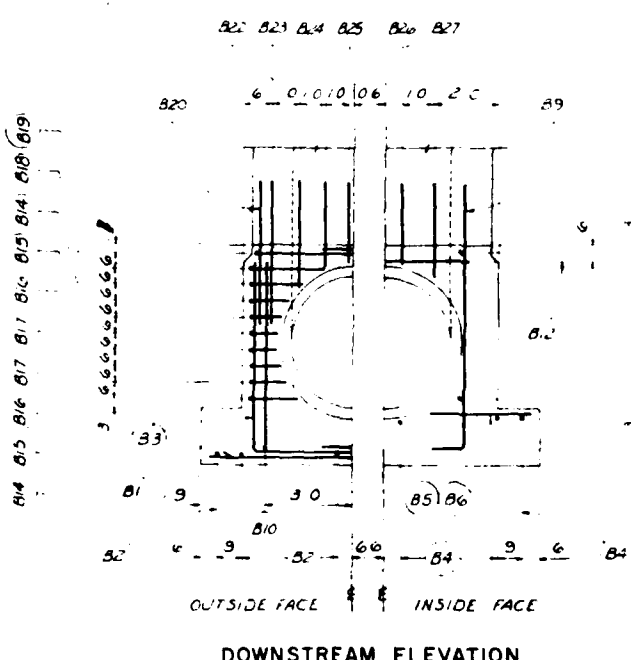
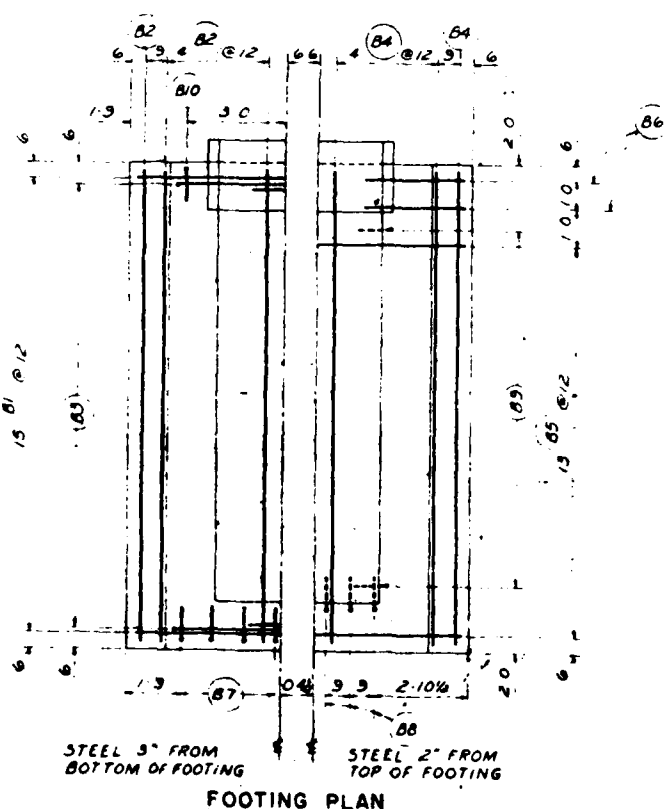
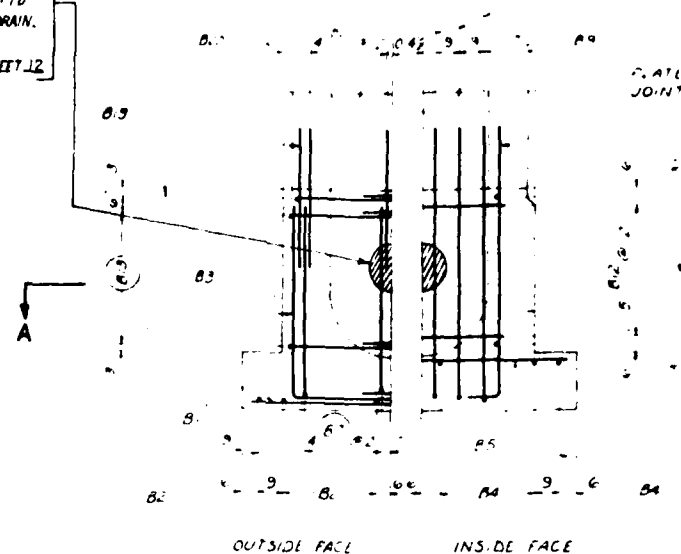
DESIGNED BY J. DENNISSEN

CHECKED BY R. G. YOLTON

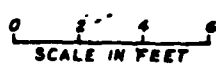
DATE 7/71

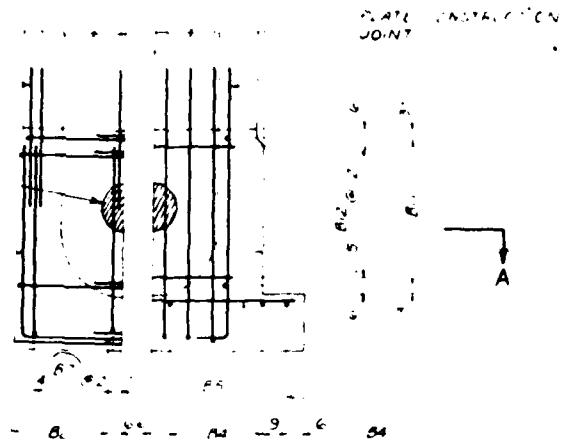
DATE 7/71

NY-26-P

[illegible]

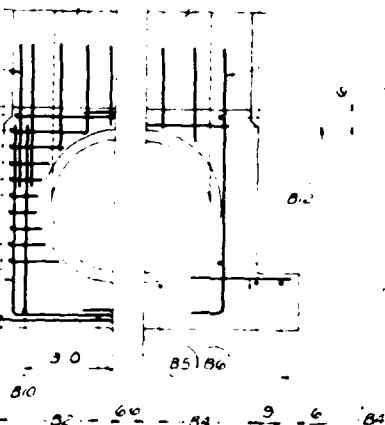
STANDARD COVERED RISER	
DESIGN CONSTANTS	$f'_c = 4000 \text{ psi}$ $n = 8$
	$f_t = 1600 \text{ psi}$ $f_s = 20,000 \text{ psi}$
STANDARD SPEC. NO. ES-3048-30:5E	
DATE 8-06	SHEET 2 OF 4



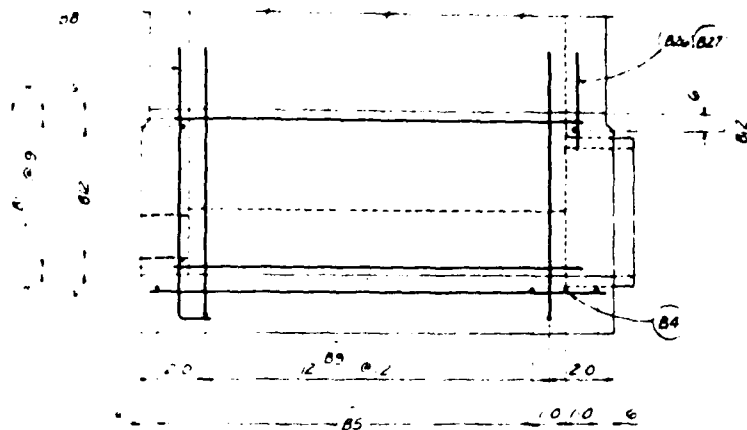


UPSTREAM ELEVATION

B21 B24 B25 B26 B27
B10 B11 B12 B13 B14 B15 B16 B17 B18 B19 B20

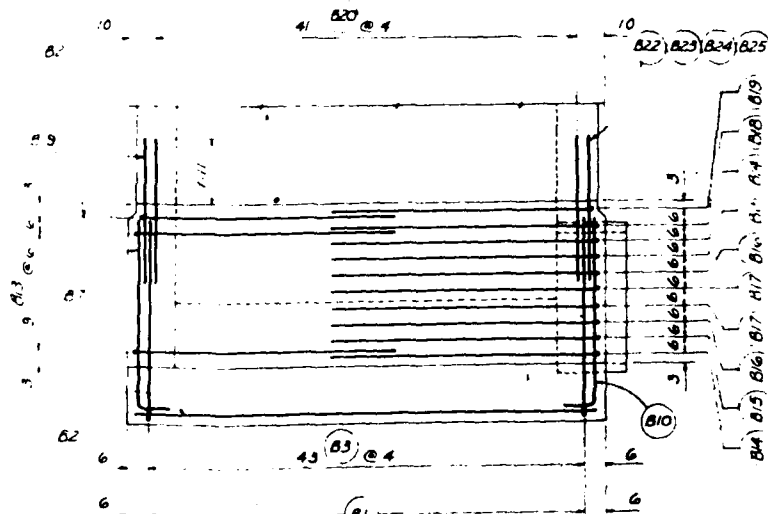


DOWNSTREAM ELEVATION



STEEL 2" FROM INSIDE FACE OF RISER
AND 2" FROM TOP OF FOOTING

SIDEWALL ELEVATION



STEEL 2" FROM OUTSIDE FACE OF RISER
AND 3" FROM BOTTOM OF FOOTING

SIDEWALL ELEVATION

AS BUILT
8/22/77

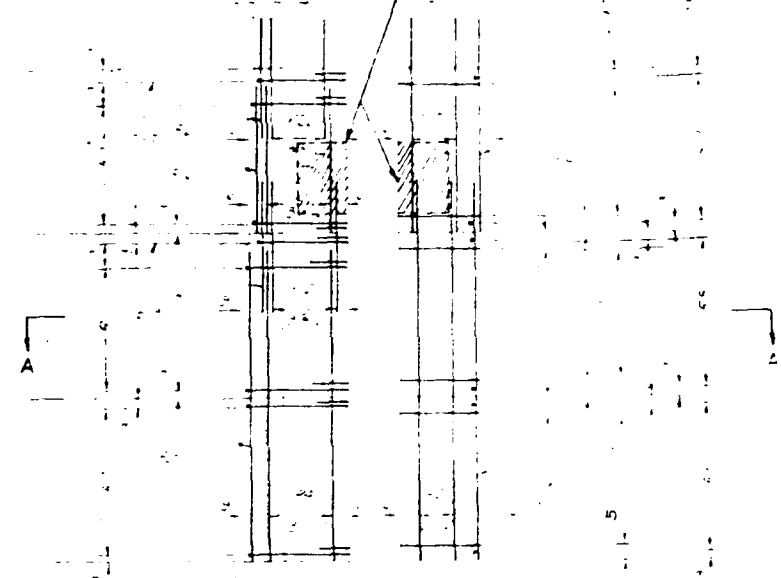
CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
RISER STRUCTURAL DETAILS

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

Adapted: J. Thomasson	Date: 11/21	Approved by:	
Drawn:		Reviewed by:	
Traced:		Checked by:	
Checked:		NY-2161-P	

B-15

The drawing shows a rectangular frame with a dotted border. The frame is labeled 'Fig. 1' and 'Fig. 2'.



ENDWALL ELEVATION

CONSTR. JOINT

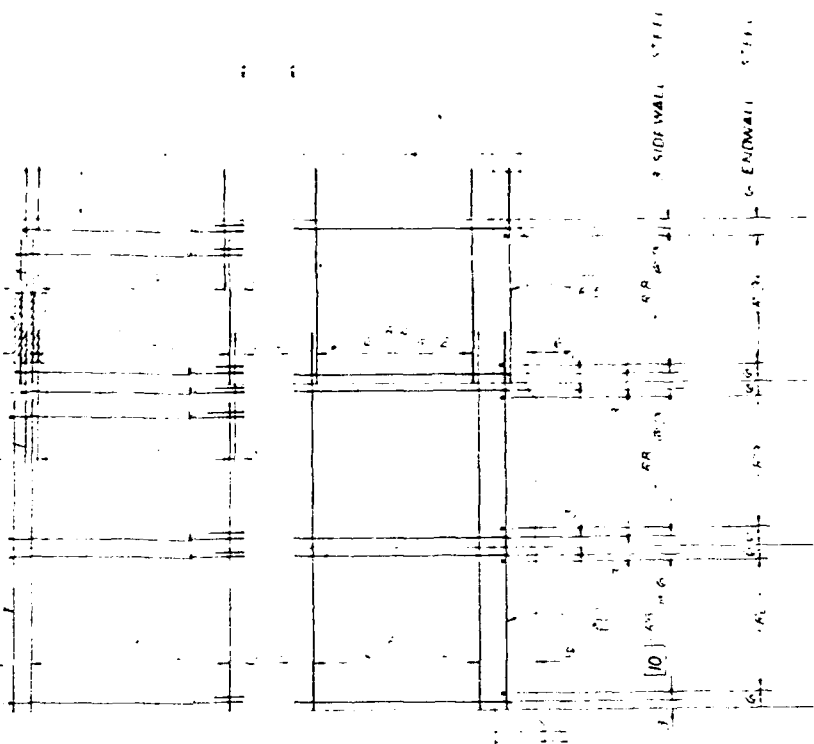
- ### SLIDE GATE DETAILS

1. 18" DIA. FLAT FRAME SLIDE GATE
2. CLASS 0-30
3. SLIDE GATE SHALL CONFORM TO SPEC 533 AND SHALL BE TYPE MHS-1.
4. 7" TYPE WALL TWIMBLE 10" DEEP.
5. RISING STEM, STEM GUIDES, AND LIFTING DEVICE SHALL BE SIZED, AND SPACED ACCORDING TO MANUFACTURER'S RECOMMENDATIONS.

0 2 4 6
SCALE IN FEET

[illegible]

PLA
CONST



SIDEWALL ELEVATION



CONSTR JOINT

Continuous thru constr joint
 Splices shall be either:
 1. Butt welded
 2. Lapped 3' and lap sp
 3. Lapped 3' and lap sp



PLATE
 CONSTR JOINT

2

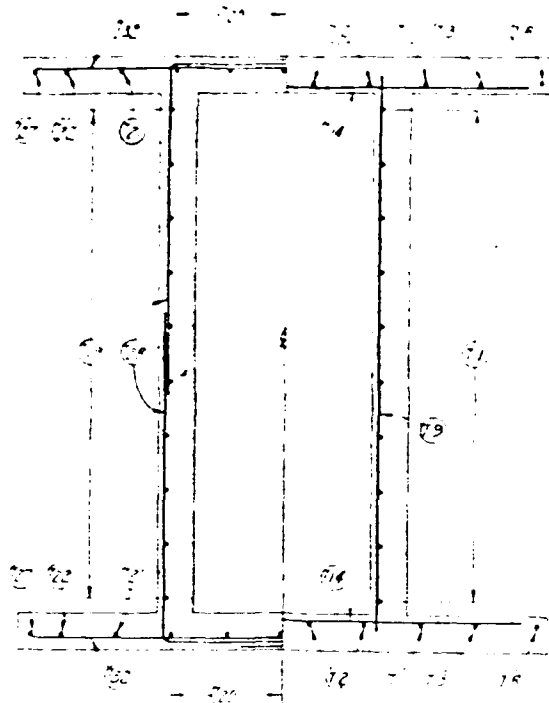
AS BUILT
 8/22/77

CONEWANGO CREEK WATERSHED PROJECT
 SITE 9A
 FLOODWATER RETARDING DAM
 CHAUTAUGUA COUNTY, NEW YORK
 RISER STRUCTURAL DETAILS

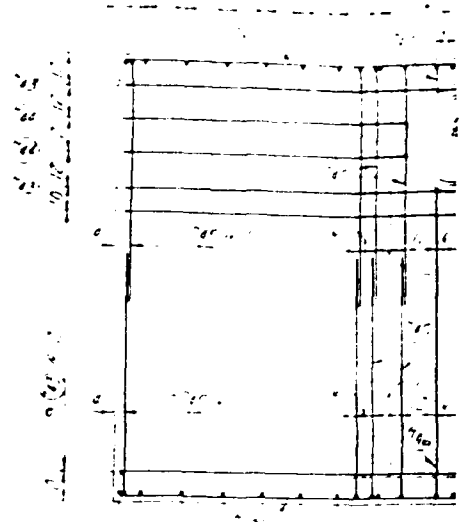
U. S. DEPARTMENT OF AGRICULTURE
 SOIL CONSERVATION SERVICE

DESIGNED J. TOENNIESSEN 7/77
 DRAWN R. G. YOJON 7/77

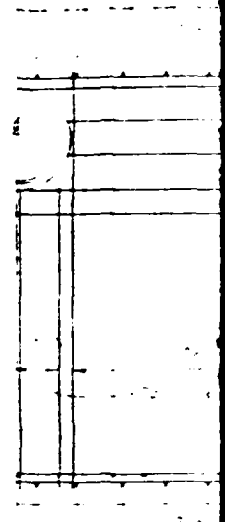
NY-2161-P



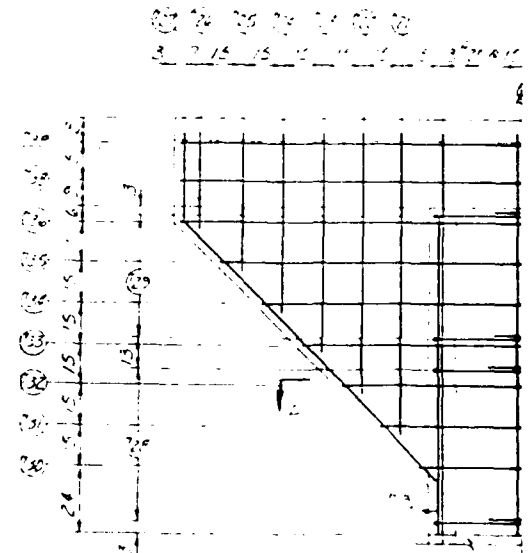
Outside Steel Inside Steel
 24" 72" 24" 72" 18"
 1000 Feet



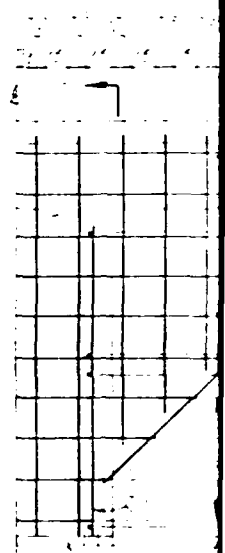
24" 72" 24" 72" 18"
 1000 Feet



24" 72" 24" 72" 18"
 1000 Feet



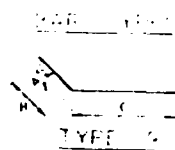
24" 72" 24" 72" 18"
 1000 Feet



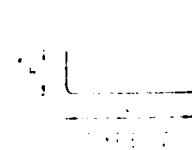
24" 72" 24" 72" 18"
 1000 Feet

STANDARD COVERED RISER			
DISCREPANCIES	1/4" - 400 ps.	1/4" - 100 ps.	
	n = 8	1/4" - 200 ps.	
STANDARD DRG NO.	ES 4046 3015E		
DATE	1/1	SHEET	4 OF 4

TYPE

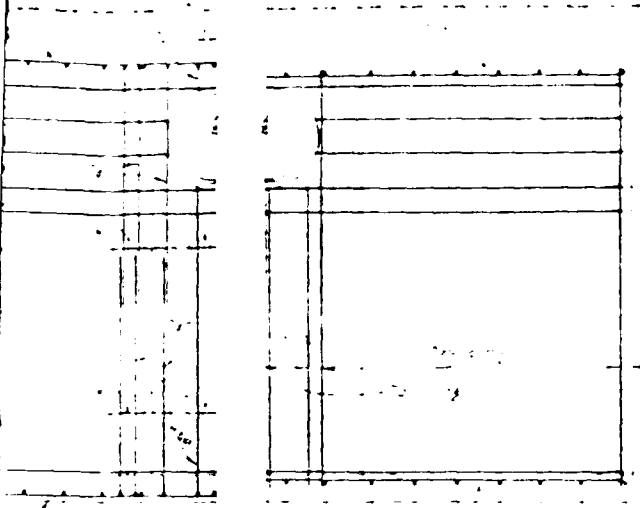


TYPE 1

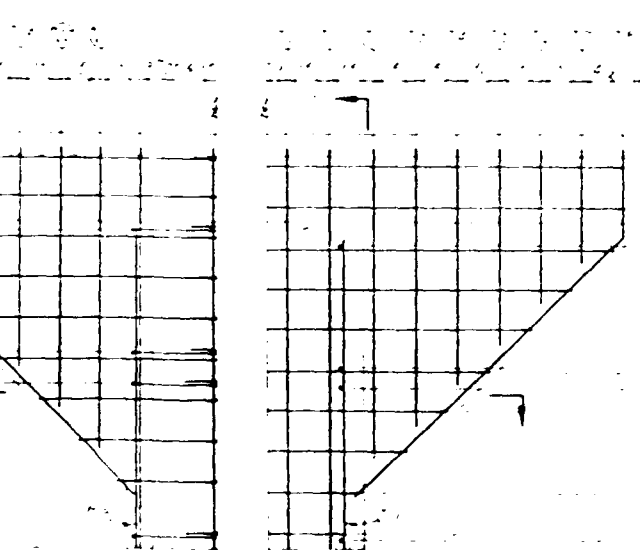


TYPE 2

NOTE:
 1. OUT OF THE...
 2. THE...
 3. CLEAR DISTANCE...
 4. RADIUS OF BEND...
 5. OF 1000 FEET



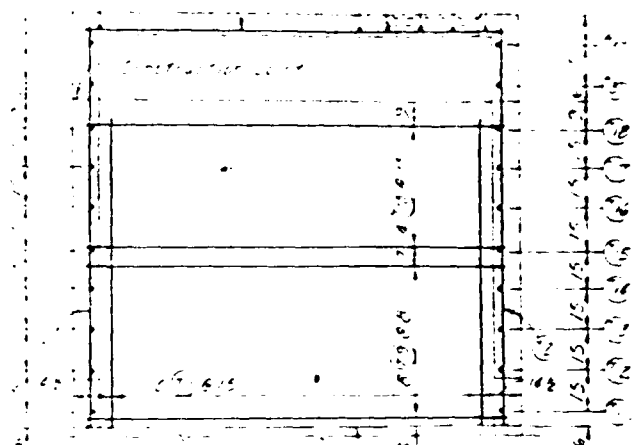
Steel 2" From Inside Face
Steel 2" From Bottom
Steel 2" From Top



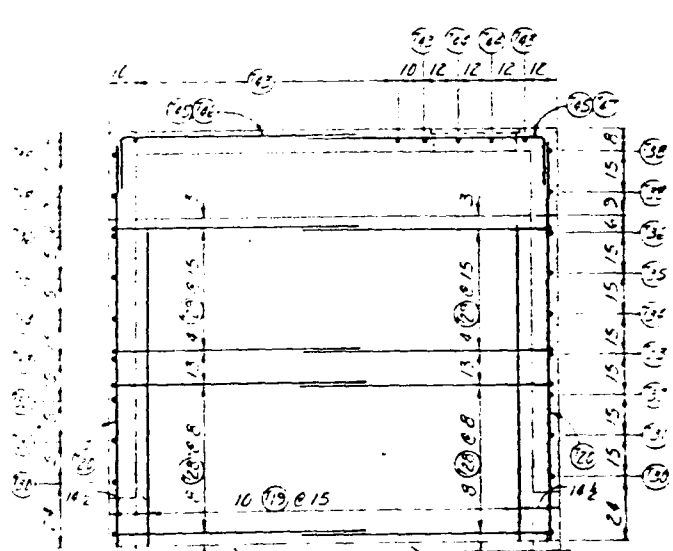
Steel 2" From Inside Face
Steel 2" From Bottom
Steel 2" From Top

1. All dimensions are in feet and inches.
2. The 2" and 4" dimensions are from the face of the concrete.
3. Radius of bend equals 12" for all reinforcement bars.
4. All reinforcement bars are to be placed in the concrete.

2



Steel 2" From Inside Face
Steel 2" From Bottom
Steel 2" From Top



Steel 2" From Outside Face
Steel 2" From Bottom
Steel 2" From Top

AS BUILT

Scale in Feet
Unless Otherwise Shown 8/24/79

CONEWAGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUE COUNTY, NEW YORK
RISER STRUCTURAL DETAILS

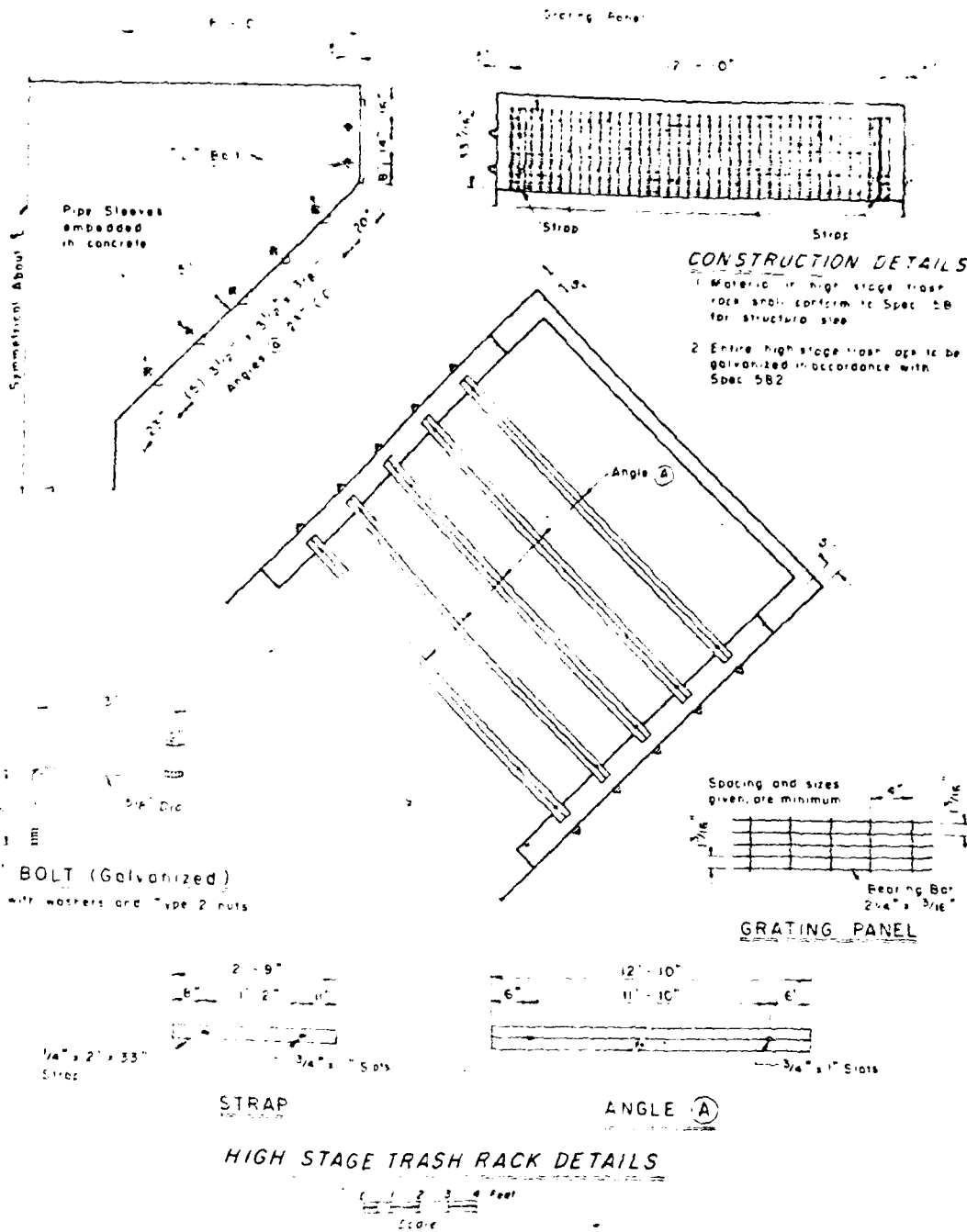
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

DATE: 11/71
DRAWN BY: J. T. GIBSON
CHECKED BY: J. T. GIBSON
APPROVED BY: J. T. GIBSON

NY-218-P

LOW STAGE TRASH RACK DETAILS

SECTION 4.4



"L" BOLT (Galvanized)
Supply with washers and Type 2 nuts

HIGH STAGE TRASH RACK BILL OF MATERIALS		MATERIALS	
ITEM	SIZE	LENGTH	QUANTITY
Angle A	3 1/2" x 2 1/2" x 3/4"	2 - 10'	10
Strap	1/4" x 2' x 33"	2 - 10'	4
"L" Bolt	1/2" Dia	2 - 10'	26
Grating Panel	22" x 12' x 10'	2 - 10'	2
Support Brackets	1/4" x 10"	2 - 10'	26

2

CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
RISER TRASH RACKS
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

Adopted by TOENNISSSEN 11/73
Drawn by L. H. Burtis

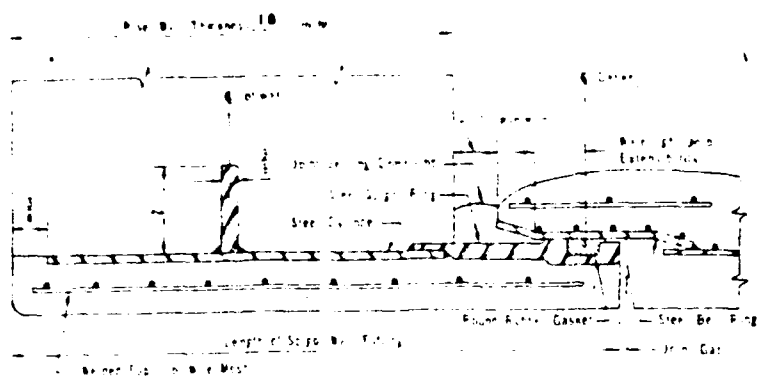
AS BUILT
8/22/77

NY-2.6.-P

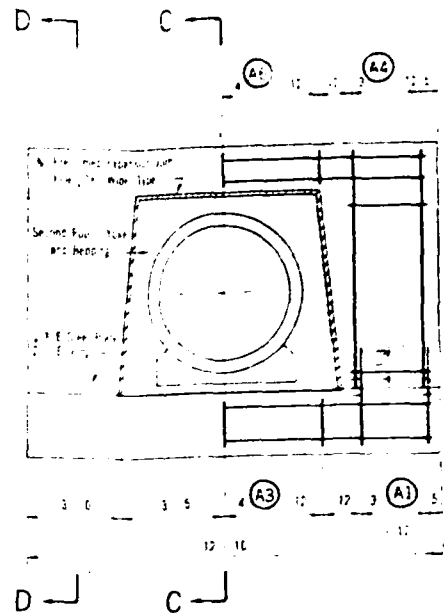
B-18

SECTION 4.8

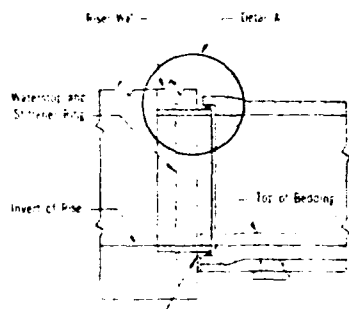
LS



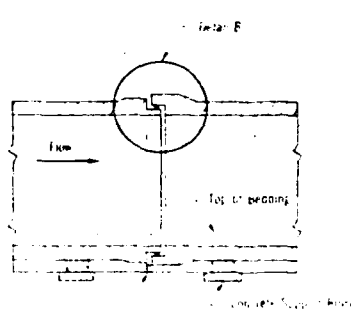
DETAIL A



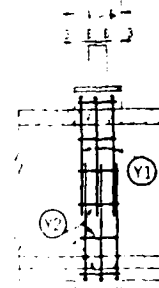
DETAIL OF ANTI-SEEP COLLAR 7



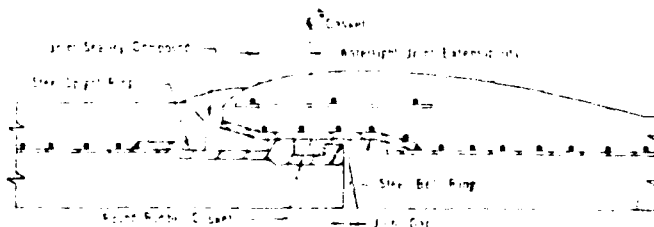
DETAIL OF SPIGOT WALL FITTING



DETAIL OF PIPE JOINT



SECTION C-C



DETAIL B

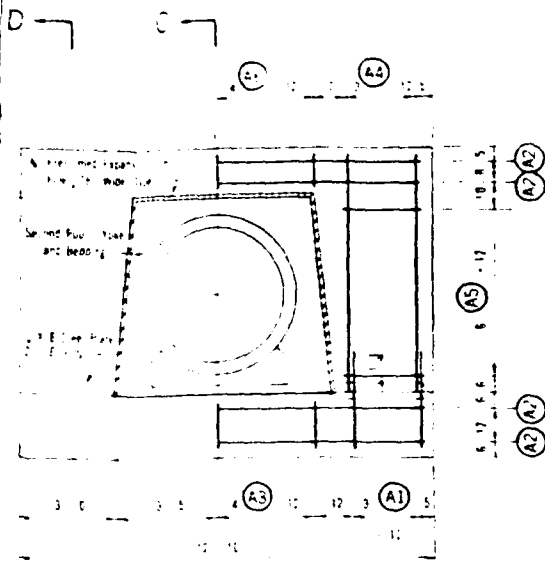
JOINT REQUIREMENTS			
NO. OF PIPE SECTIONS	PIPE SIZE	JOINT TYPE	REQUIREMENTS
EACH			
B	200	2" x 4"	0.050" 2" x 53"
I	18 0	2" x 4"	0.050" 2" x 53"

SUPPLY ONE SPIGOT RING WALL FITTING FOR 18" WALL CAST OUTSIDE OF SPIGOT RING WITH CONCRETE ON 18" SECTION

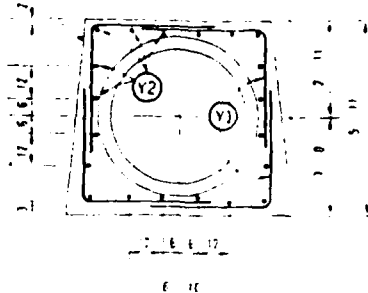
STANDARD CONDUIT DETAILS	
FOR REINFORCED CONCRETE PRESSURE PIPE PRINCIPAL SPILLWAY	
STANDARD LRG NO.	ES-5048-BE
DATE	2-70
SHEET	1 OF 1

THE PIPE SHALL BE JOINED TOGETHER SO THAT THE MAXIMUM JOINT GAP DOES NOT EXCEED 1/8" FOR PIPE Laid ON A STRAIGHT LINE. FOR CURVED PIPE OR PIPE Laid ON A CURVED LINE, THE JOINT GAP AT THE LOWEST POINT SHALL NOT EXCEED 1/4" INCH.

FOR PIPE JOINTS OF OTHER TYPES, THE JOINT REQUIREMENTS WILL BE DETERMINED BY THE ENGINEER.



DETAIL OF ANTI-SEEP COLLAR 7 REQUIRED



DETAIL OF ANTI-SEEP COLLAR YOKE

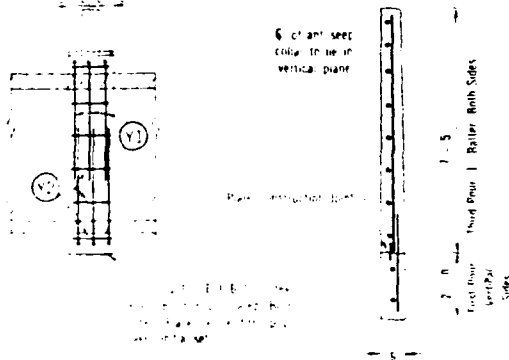
STEEL SCHEDULE

Item	Size	Quantity	Unit	Weight	Notes
1	4	1	lb	120-0	
2	4	1	lb	144-4	
3	4	1	lb	144-4	
4	4	1	lb	144-4	
5	4	1	lb	144-4	
6	4	1	lb	144-4	
7	4	1	lb	144-4	
8	4	1	lb	144-4	
9	4	1	lb	144-4	
10	4	1	lb	144-4	
11	4	1	lb	144-4	
12	4	1	lb	144-4	
13	4	1	lb	144-4	
14	4	1	lb	144-4	
15	4	1	lb	144-4	
16	4	1	lb	144-4	
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18	4	1	lb	144-4	
19	4	1	lb	144-4	
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21	4	1	lb	144-4	
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96	4	1	lb	144-4	
97	4	1	lb	144-4	
98	4	1	lb	144-4	
99	4	1	lb	144-4	
100	4	1	lb	144-4	

QUANTITIES

Item	Quantity	Unit
Concrete		
Anti-seep Collar including Yoke	22.0	cu yds
Total	21.2	cu yds
Steel	1231	lb
Anti-seep Collar including Yoke	1842-2	lb
Total	57.48	lb

Complete quantities are given in an outside diameter of 48 inches.



SECTION C-C

SECTION D-D

DETAIL OF BEDDING



BAR TYPES



SUGGESTED SUPPORT BLOCKS

Sufficient blocks shall be provided to support the pipe to the required line and grade. The contractor shall determine the number and size of blocks required. Weight of blocks shall be noted.

AS BUILT

JOINT REQUIREMENTS

Joint	Material	Quantity
200	2" x 4" x 8" x 16"	0.050 2" x 53"
18 0	2" x 4" x 8" x 16"	0.050 2" x 53"

STRENGTH REQUIREMENTS

Item	Material	Quantity
1	Concrete	15,114
2	Steel	15,114

The contractor shall provide a minimum of 15,114 pounds of concrete and 15,114 pounds of steel for the joint. The contractor shall determine the number and size of blocks required. Weight of blocks shall be noted.

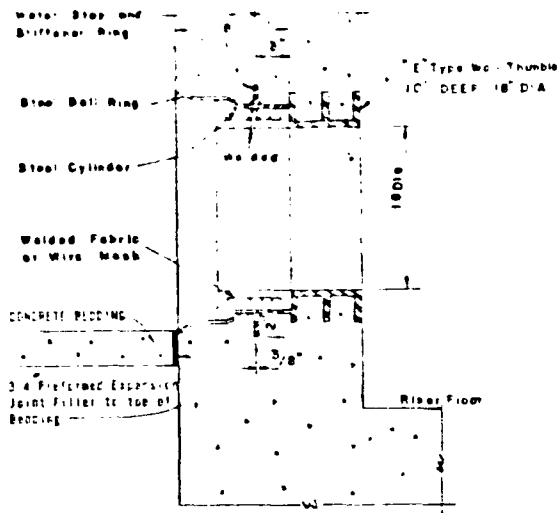
CONEWAGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAMPAIGN COUNTY, NEW YORK
48" DIA. CONDUIT DETAILS

U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

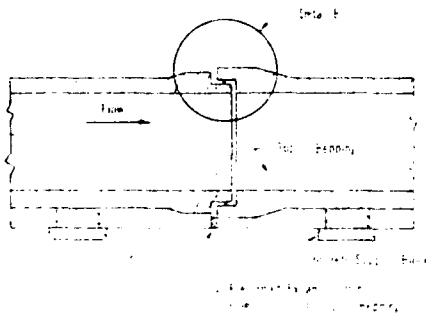
Item	Material	Quantity
1	Concrete	15,114
2	Steel	15,114

NY-216-P

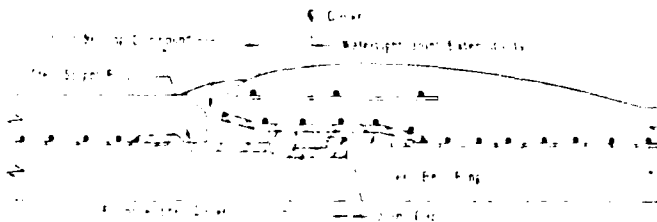
B-19



BELL WALL FITTING
W/ "E" TYPE WALL THIMBLE



DETAIL OF PIPE JOINT



DETAIL B

JOINT REQUIREMENTS

No of PIPE SECTIONS EACH	20.0	23.4"	00960 5*30"
2			

STANDARD CONDUIT DETAILS		
FOR REINFORCED CONCRETE PRESSURE PIPE PRINCIPAL SPILLWAY		
STANDARD ERL NO	ES 5018-BE	
DATE	2-70	SHEET 1 OF 1

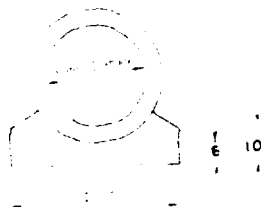
The drawing is to be used for the design of the spillway structure. It is to be used for the design of the spillway structure. It is to be used for the design of the spillway structure.

1. The drawing is to be used for the design of the spillway structure. It is to be used for the design of the spillway structure. It is to be used for the design of the spillway structure.

STR

18.C

QUANTITIES, (THIS SHEET ONLY)
 CONCRETE 2.4 CU Yds
 (NON-REINF)



DETAIL OF BEDDING



SUGGESTED SUPPORT BLOCKS

See note on sheet 10 for details of support
 blocks and required line and grade. The
 drainage pipe should be placed in the center of the
 support block. Water may be used to
 fill the support block.

Blue/ry
AS BUILT

STRENGTH REQUIREMENTS

IT REQUIREMENTS

23.4' 10' 46C 5' 30'

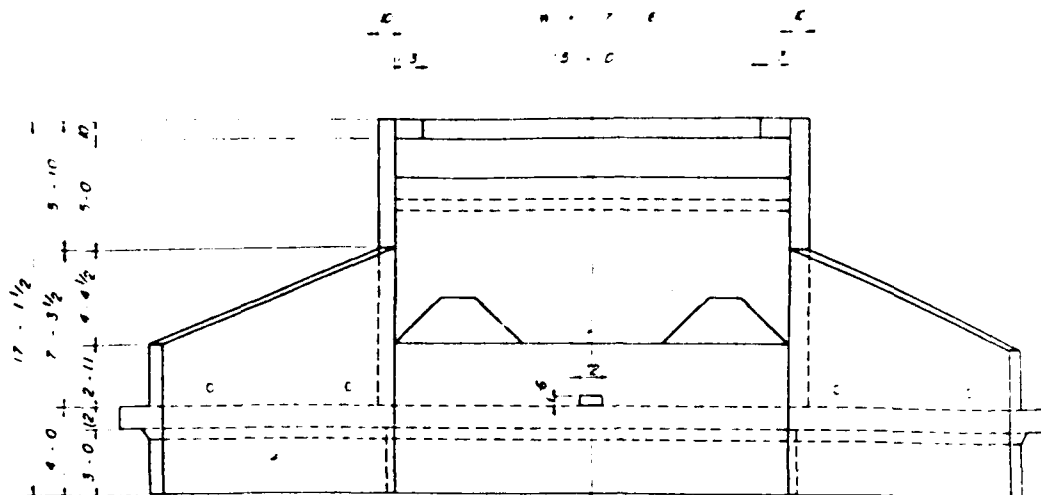
180 34.2 4712

240

CONEWANGO CREEK WATERSHED PROJECT	
SITE 9A	
FLOODWATER RETARDING DAM	
CHAUTAUQUA COUNTY, NEW YORK	
RESERVOIR DRAIN CONDUIT DETAILS	
U S DEPARTMENT OF AGRICULTURE	
SOIL CONSERVATION SERVICE	
Drawn by JULIUS D. TOENNIESEN 9-71	Checked by WILLIAM TURNER 9-71
Scale 1" = 10'	NY-2161-P

sy B-20

2



DOWNSTREAM ELEVATION

Use last section
of canal to be
as per section

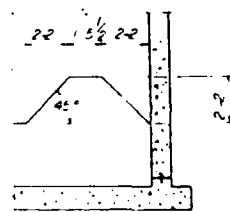
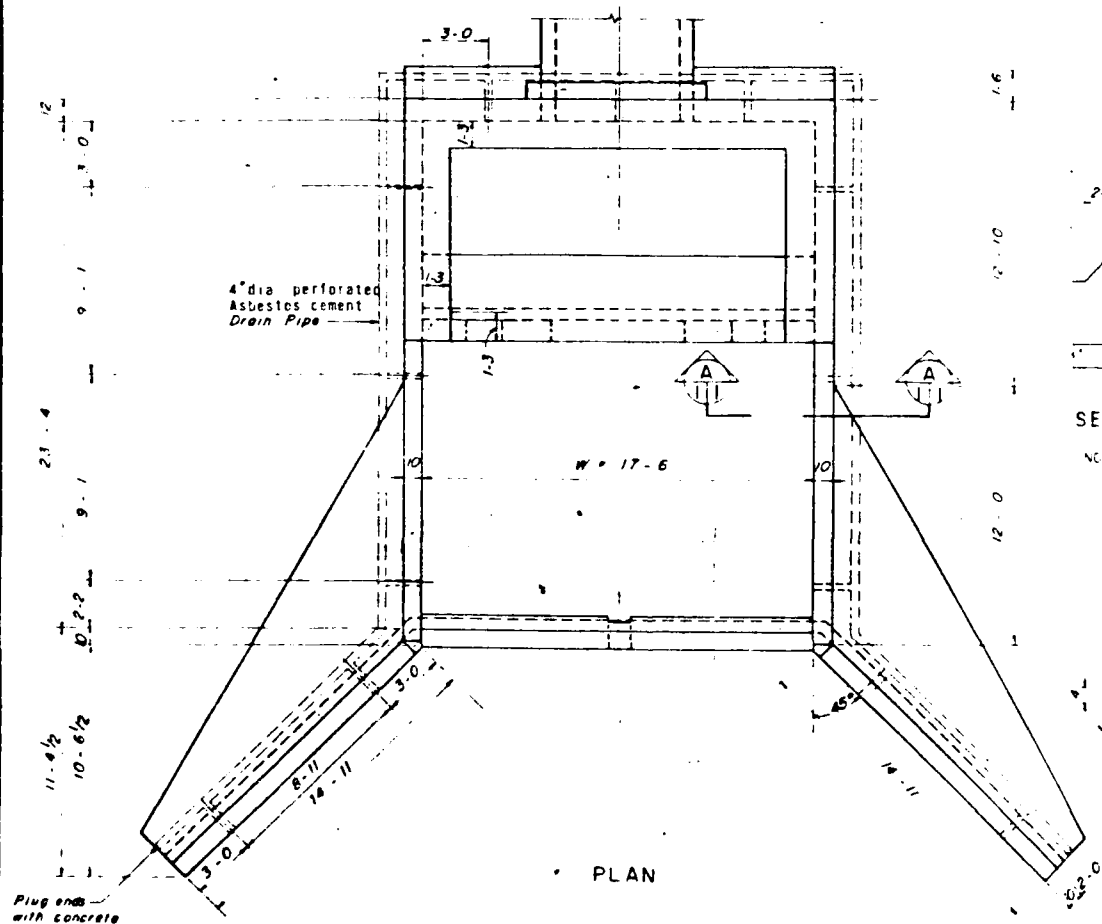
Pipe 10

Concrete
bedding

Compressible material
(Styrofoam)

1/2" Expansion joint
material

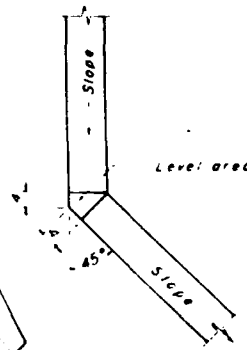
see section below



SECTION A-A

NOT TO SCALE

SECTION THRU
NOT



PLAN - JUNCTION
SIDEWALL AND
WINGWALL
NOT TO SCALE

CUTOFF WALL

STANDARD IMPACT BASIN

DESIGN CONSTANTS $f'_c = 4000 \text{ psi}$ $f'_s = 1600 \text{ psi}$
 $n = 8$ $f_s = 20,000 \text{ psi}$

STANDARD DRAWING NO ES-4175

DATE 1-70

SHEET 1 OF 5

CARL ROMDE
Consulting Engineer
654 Pidgeon Rd Lake Oswego Ore

1 0 5 10
SCALE
EXCEPT IN AS FEET
NOTED

NOTE: Last section of conduit to be as horizontal as possible

Pipe 10

Concrete bedding
Compressible material (Styrofoam)
1/2" Expansion joint material

see section below

SECTION ON CENTERLINE

Sidewall

Headwall
(Wingwall similar)

1/4" x 6" Carbon steel plate at 6" of wall Use 3" lap splices

Apron

Drain fill Detail see sheet 2

4" Drain Pipe Detail see detail, sheet 2 of 5

SECTION THROUGH DRAIN & FILTER

NOT TO SCALE

CONSTRUCTION JOINT DETAILS

NOT TO SCALE

NOTE

Perforated drain pipe shall conform to specification 545 and shall be 4" dia pressure pipe, class 200

QUANTITIES

Formwork (Contact area)	3080	Sq Ft
Reinforced Concrete (Class 4000)	77	Cu Yds
Reinforcing Steel	14,100	Lbs
Drainage		
4" Perforated drain pipe	137	Lm Ft
Animal screen detail, sheet 2 of 5	13	ea
Drain pipe tees	13	ea
Drain pipe 90° ell	2	ea
Drain pipe 45° ell	2	ea

8/21/74 AS BUILT

Joint 1/4" x 6" Carbon steel plate Structural grade 985 lbs

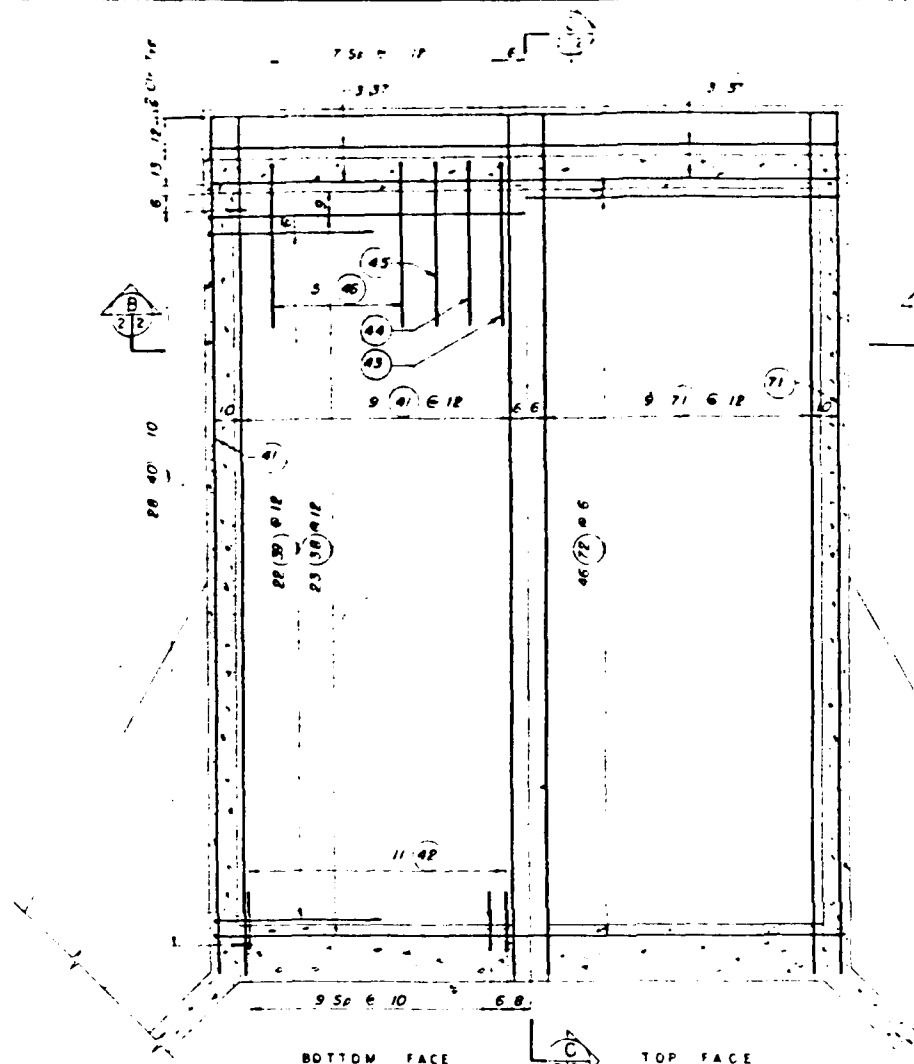
CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUE COUNTY, NEW YORK
IMPACT BASIN DETAILS

U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

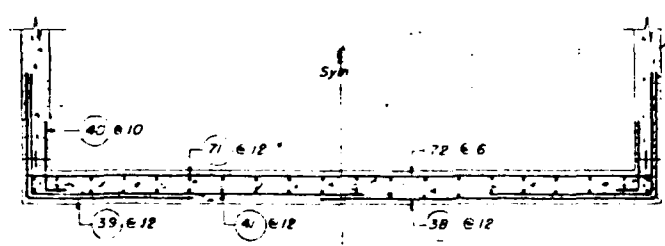
DESIGNED BY J. TOENNIESSEN	DATE 11/74	APPROVED BY
DRAWN BY	CHECKED BY	DATE
SCALE	PROJECT NO.	NY-261-P

ISOMETRIC VIEW

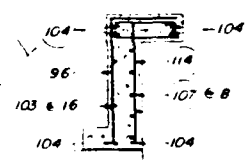
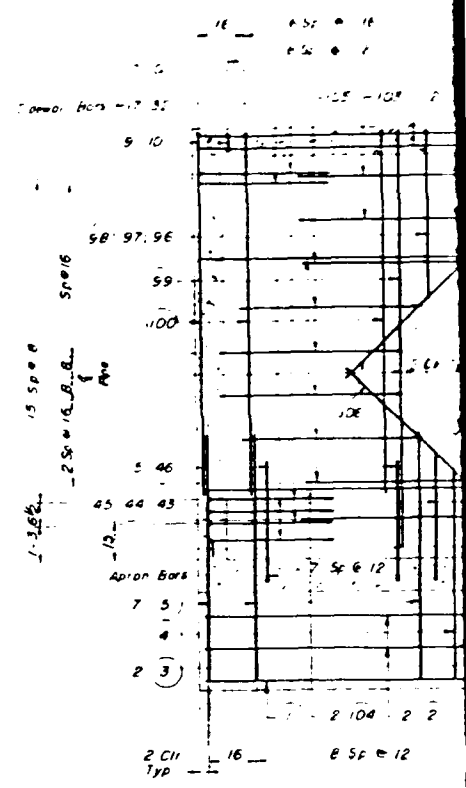
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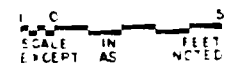
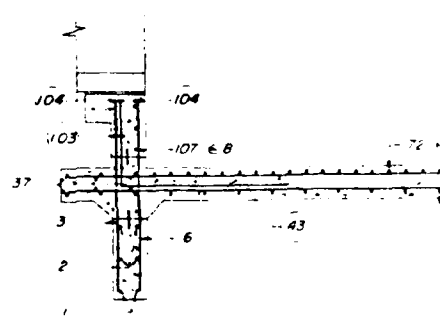
PLAN OF APRON



SECTION

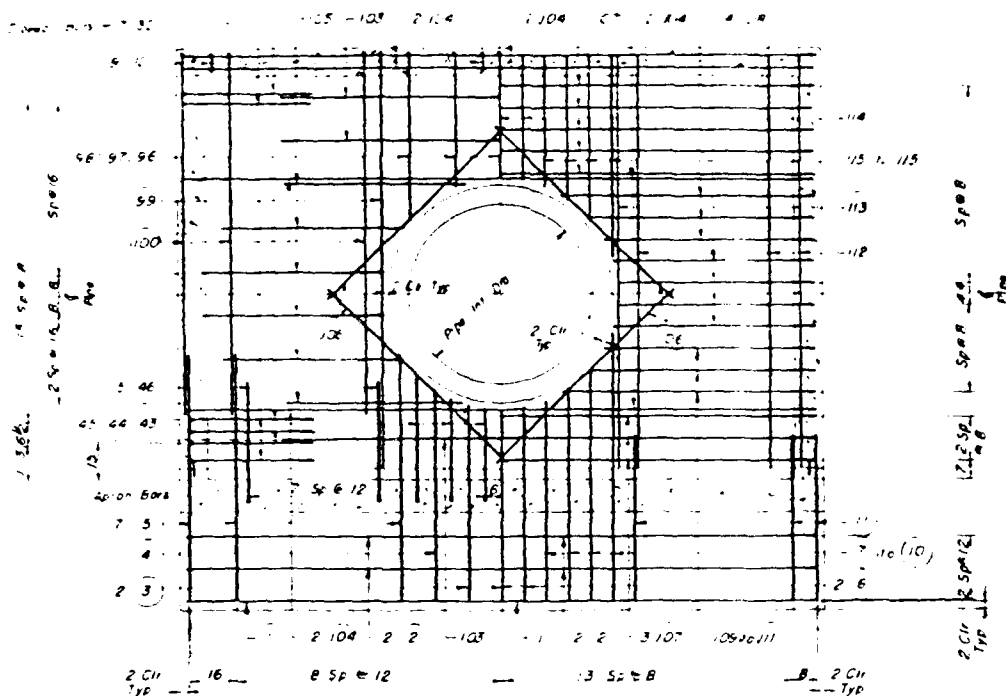


HEADW



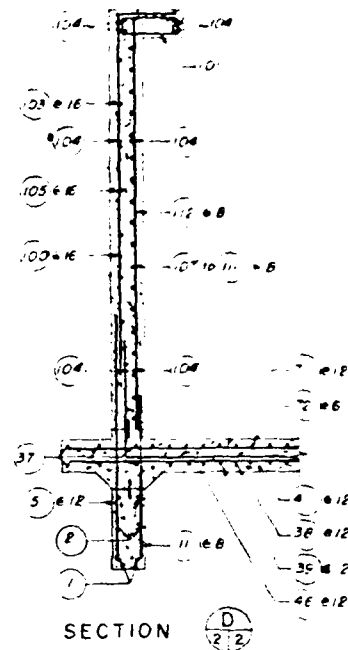
STANDARD IMPACT BASIN	
DESIGN CONSTANTS	14000 PSI 1600 PSI
	20,000 PSI
STANDARD DRAWING NO.	ES-4175
DATE	1-70
SHEET	2 OF 3

CARL RICHDE
Consulting Engineer
654 Ridgeway Rd Lake Oswego, Ore



UPSTREAM FACE DOWNSTREAM FACE

HEADWALL ELEVATION



1/4" bolt 1 1/4" long with flat washer

Clamp 1" wide 1/4" thick

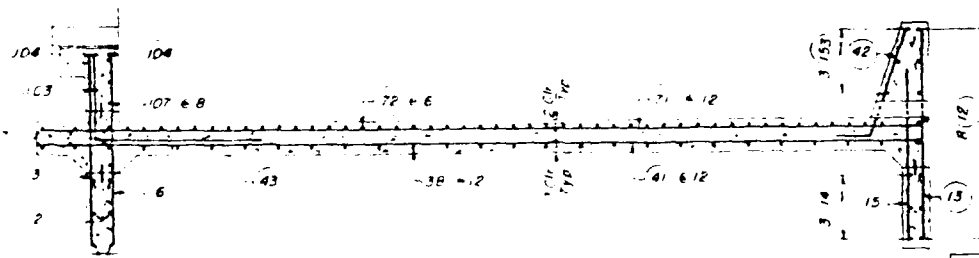
1/2" woven galv wire mesh No 12 gage clamped to pipe

3/4" premoixed asphaltic joint filler around pipe

Plug end with concrete

DETAIL OF SMALL ANIMAL GUARD SCREEN AND OUTLET OF DRAIN PIPE

SCALE IN FEET



SECTION C-C

AS BUILT

8/22/74

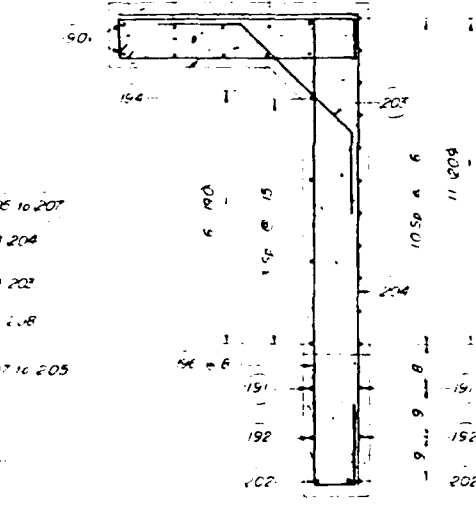
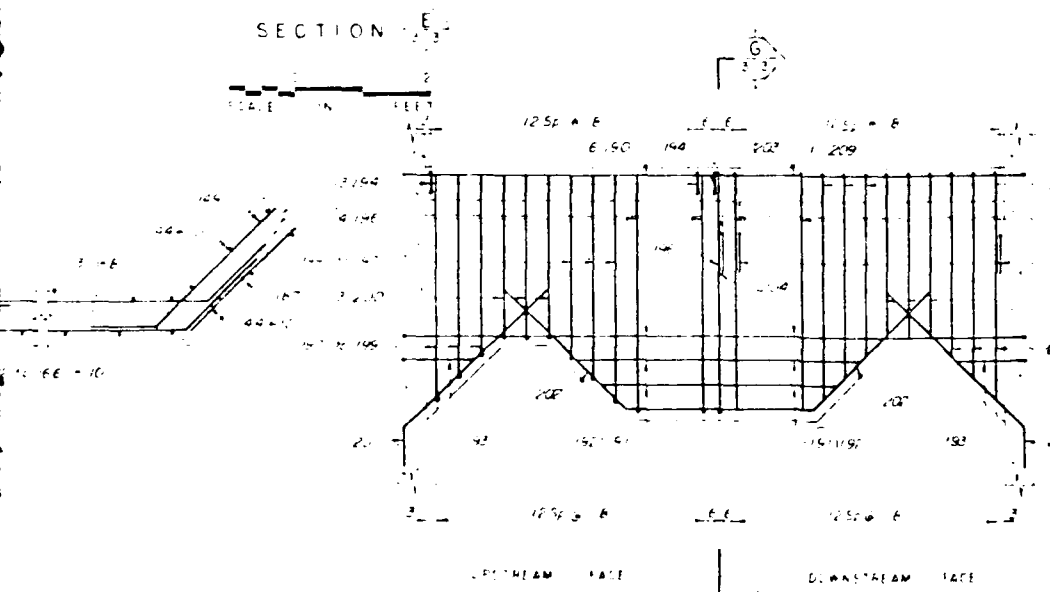
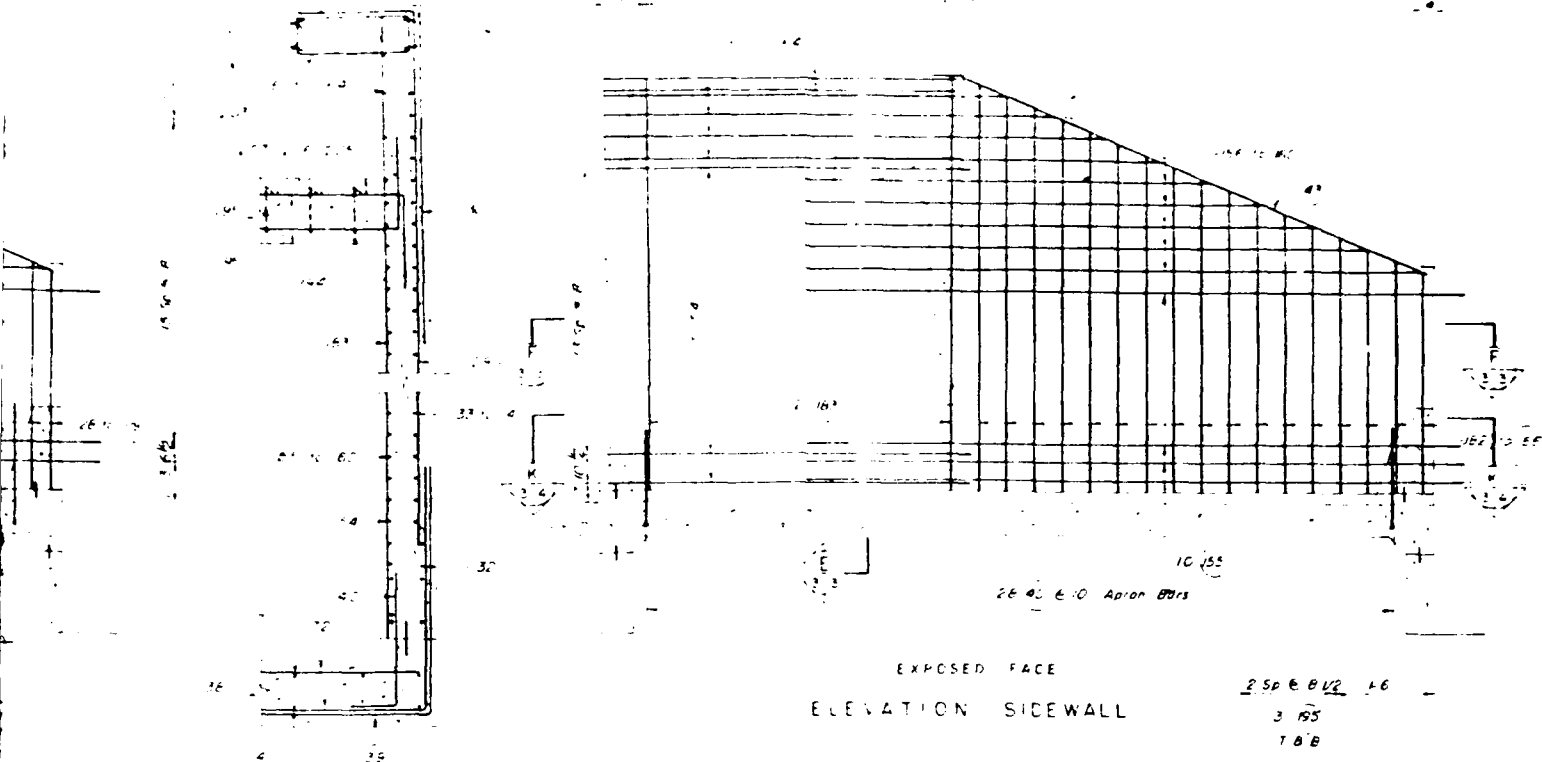
CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
IMPACT BASIN DETAILS

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

Approved: J. J. Schlessen 11/71
Checked by: [blank]
Date: [blank]
NY-2161 - P

B-22

2



BAFFLE ELEVATION

AS BUILT
 8/22/74

SECTION 6
 SCALE IN FEET

CONEWANGO CREEK WATERSHED PROJECT
 SITE 9A
 FLOODWATER RETARDING DAM
 CHAUTAUQUA COUNTY, NEW YORK
 IMPACT BASIN DETAILS

U. S. DEPARTMENT OF AGRICULTURE
 SOIL CONSERVATION SERVICE

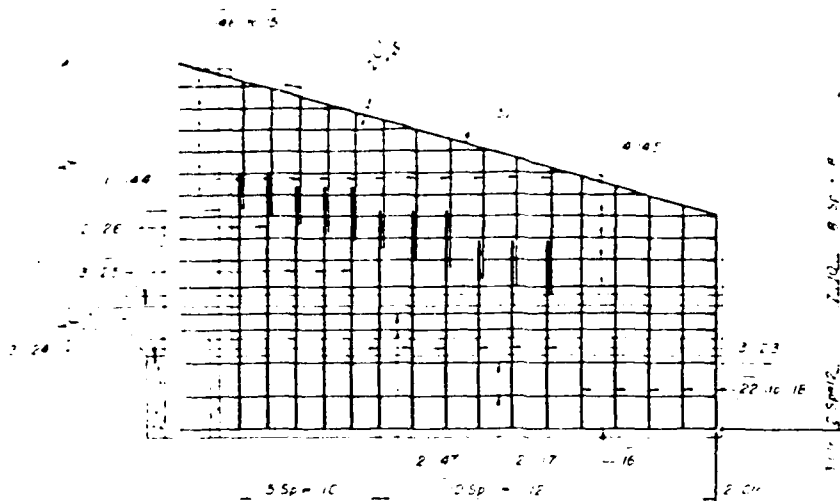
J. T. Tressler
 ASPECTED

11 71

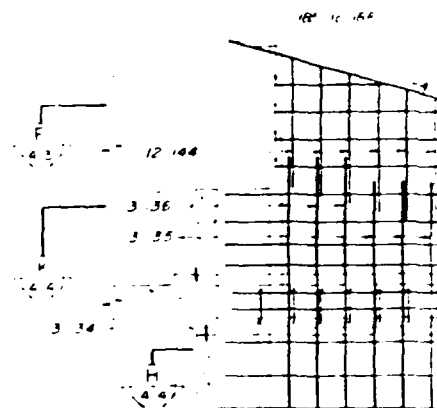
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NY-2161-P

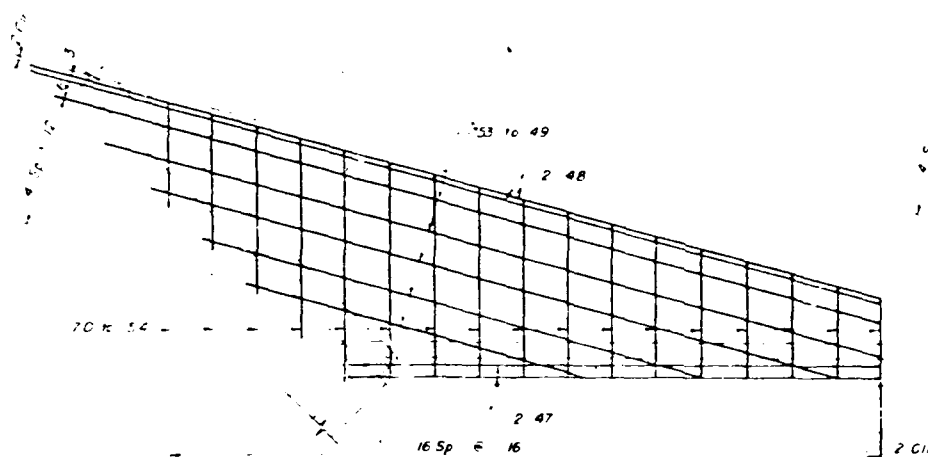
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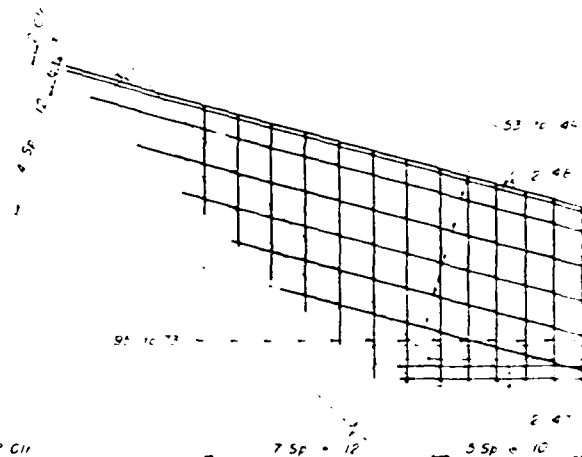
UNEXPOSED FACE
WINGWALL ELEVATION



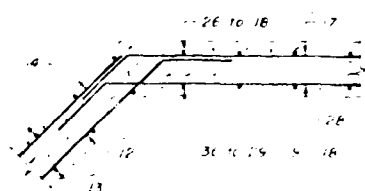
EXPOSED FACE
WINGWALL ELEVATION



PLAN WINGWALL FOOTING - BOTTOM FACE

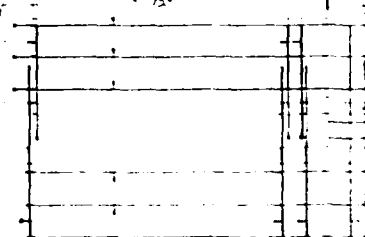


PLAN WINGWALL FOOTING - TOP FACE



SECTION H-H

1 0 2
SCALE IN FEET



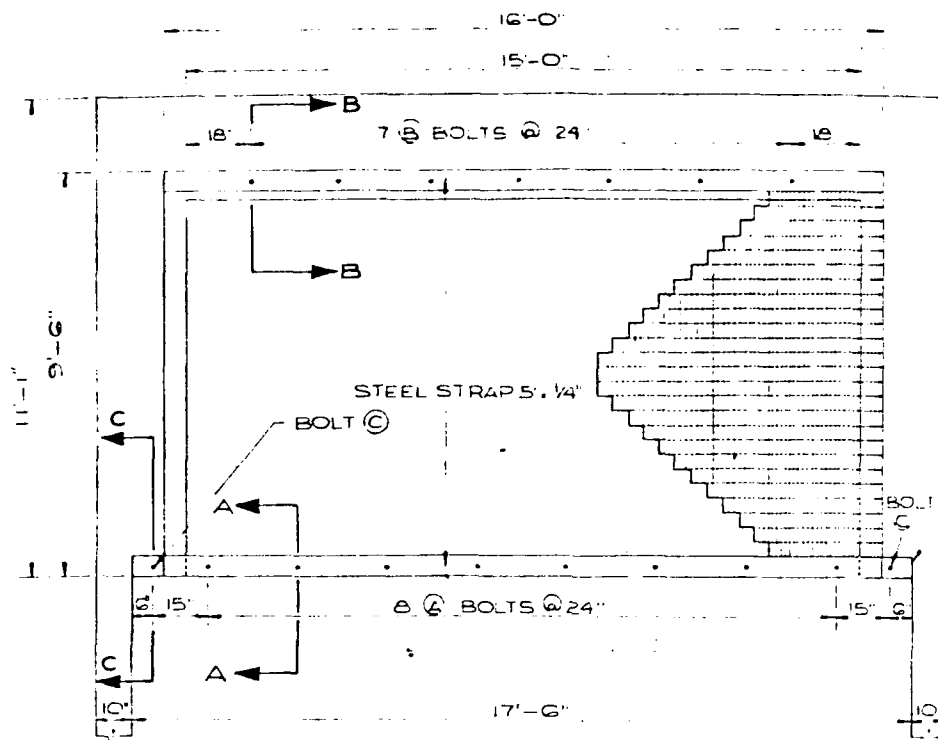
SECTION L-L

ELEVATION OF END

1 0
SCALE IN FEET
EXCEPT AS NOTED

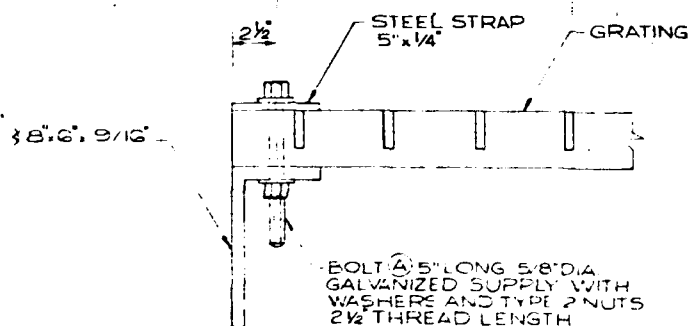
STANDARD IMPACT BASIN
NO. 1000000
ES-4.75
SHEET 4 OF 5

CARL RICHIE
Consulting Engineer
654 Prosperity Rd. Suite 100, Opa-Lake, Okla.

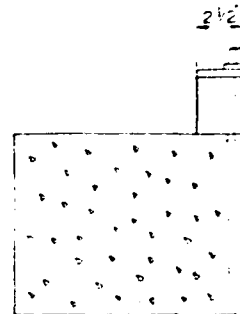


PLAN VIEW

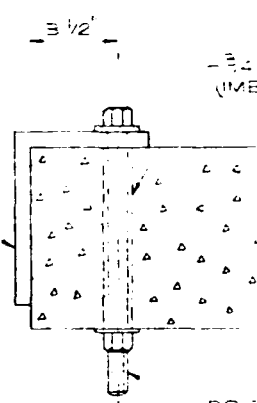
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SCALE IN FEET



SECTION A-A

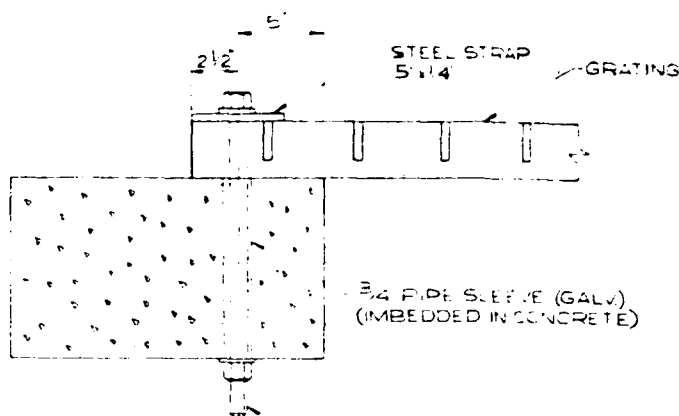


SECTION B-B



SECTION C-C

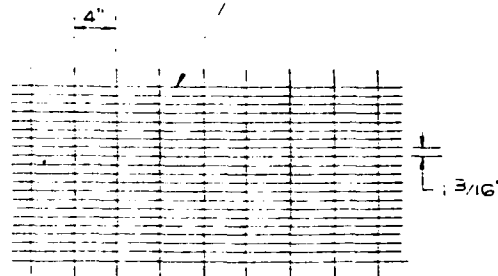
IMPACT BASIN GRATING BILL OF MATERIAL			
ITEM	SIZE	LENGTH	QUANTITY
GRATING PANEL 9'-6" x 12'-0"			
STRAP	5" x 1/4"	12'-0"	2
ANGLE IRON	6" x 6" x 1/2"	17'-6"	1
BOLT A	5/8" DIA	5"	8
BOLT B	5/8" DIA	14"	7
BOLT C	5/8" DIA	12"	2
PIPE SLEEVES	3/4" DIA	10"	8



SECTION B-B

- BOLT B 14" LONG
5/8" DIA GALVANIZED
SUPPLY WITH WASHER
AND TYPE 2 NUTS 2 1/2"
THREAD LENGTH

- BEARING BAR 2 1/4" x 3/16"



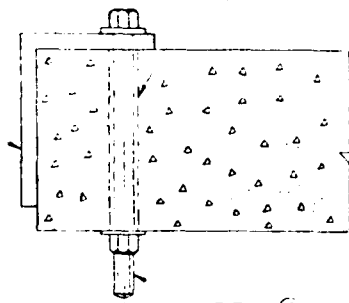
GRATING PANEL GALVANIZED (NOT TO SCALE)

CONSTRUCTION DETAILS

1. MATERIAL IN IMPACT BASIN GRATING SHALL CONFORM TO SPEC 581 FOR STRUCTURAL STEEL.
2. ENTIRE IMPACT BASIN GRATING TO BE GALVANIZED IN ACCORDANCE WITH SPEC 582.

- ANGLE IRON
6" x 6" x 1/2"

- 3/4" PIPE SLEEVE (GALV.)
(IMBEDDED IN CONCRETE)



BOLT C
12" LONG
5/8" DIA GALVANIZED
SUPPLY WITH WASHERS
AND TYPE 2 NUTS 2 1/2"
THREAD LENGTH

SECTION C-C

8/22/77
AS BUILT

CONEWANGO CREEK WATERSHED
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
IMPACT BASIN GRATING

U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

JOE TOENNIESSEN 11/71
WILLIAM TURNER 11/71

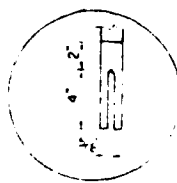
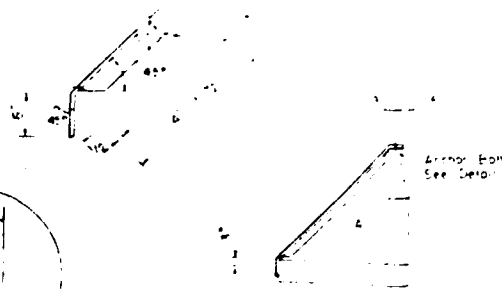
NY-2161-P

ITEM	DESCRIPTION	QUANTITY	UNIT
1	TRASH RACK	1	EA
2	ANCHOR BOLT	4	EA

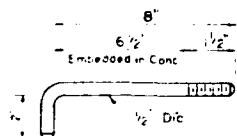
CONSTRUCTION DETAILS

Material in reservoir drain trash rack and
conform to Spec 58 for structural steel

- Trash rack to be galvanized in accordance
with Spec 582



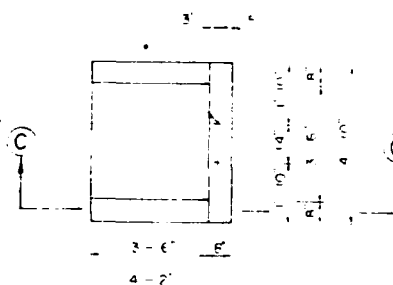
TRASH RACK



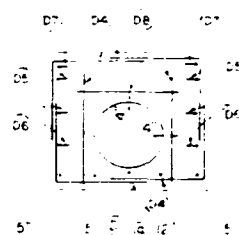
ANCHOR BOLT

Material to conform to Spec 58

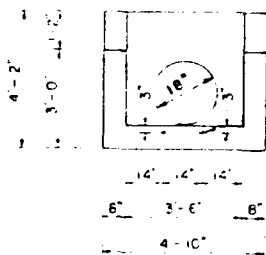
Anchor Bolt
See Detail



PLAN

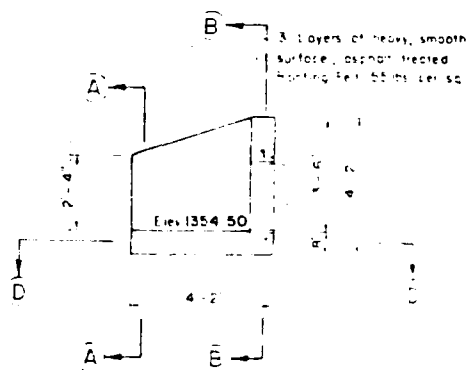


SECTION BB

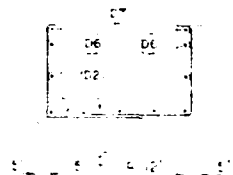


UPSTREAM ELEVATION

Anchor Bolt
See Detail



SECTION ALONG CENTERLINE



SECTION AA

REINF. CONCRETE RESERVOIR DRAIN INLET



ISOMETRIC

RESERVOIR DRAIN INLET DETAILS

NO.	QTY	SIZE	LENGTH	TYPE	WGT.	WGT.	WGT.
1	4	4"	3'-0"	1	1.5	1.5	2.0
2	4	4"	6'-0"	2	2.0	2.0	2.4
3	4	4"	5'-0"	2	2.0	2.0	2.4
4	2	4"	2'-0"	2	2.0	2.0	2.4
5	4	4"	4'-0"	2	3.0	3.0	3.6
6	2	4"	4'-0"	2	3.0	3.0	3.6
7	2	4"	3'-0"	2	3.0	3.0	3.6
8	3	4"	3'-0"	2	3.0	3.0	3.6

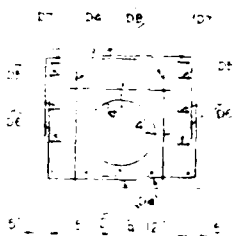
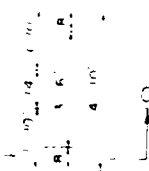
QUANTITIES (This Sheet Only)

STEEL

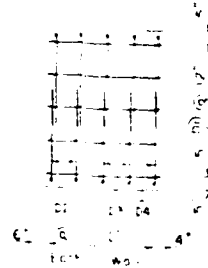
No. 4 bar 126.3 #4 1.1

CONCRETE

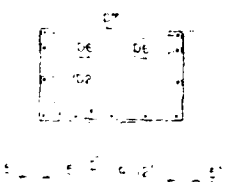
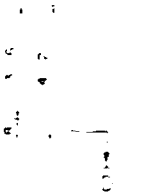
1.4 1.4 1.4 1.4 1.4 1.4 1.4 1.4



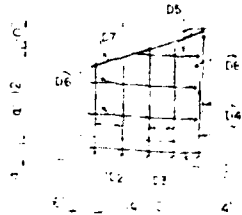
SECTION BB



SECTION DD



SECTION AA



SECTION CC

8/22/74
AS BUILT

CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK
RESERVOIR DRAIN INLET DETAILS
U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

DESIGNED BY J. E. POLULECH 3-70
CHECKED BY D. J. ANGELO 3-70
W. E. GRASSO JR.

21 NOTE - R
34

B-26

2

NATURAL DEPOSITIONS CON. MAP 9A

D
Gravel, sandy, w/little silt (55-60% gravel, 30-34% sand, 11-21% fines); max size 2", 5-8" - 4", 15-21 3-6"; gray-brown; moist, saturated in parts of flood plain; rapid permeability; non-plastic; medium-dense; alluvial and glacio-fluvial (outwash); DS 503.1 and DS 202.2 (GM-GP)

E
Gravel, sandy, w/little silt (63% gravel, 27% sand, 10% fines); max size 2", 7 1/2"-6", 18 1/2 3-6"; brown; moist; rapid permeability; non-plastic; medium-dense; alluvial; DS 205.2 (GM-GP)

F
Sand, gravelly, w/little silt (20% gravel, 69% sand, 11% fines); max size 2", 3 1/2"-3"; brown; moist; rapid permeability; non-plastic; medium; alluvial; DS 3.1: (SM-SW)

G
Sand, gravelly, w/silt and clay (30% gravel, 45% sand, 17% fines); max size 8", 3 1/2"-3"; gray-brown; moist; moderate permeability; LL-19, PI-5; hard; alluvial; DS 7.2: (SC-SM)

H
Gravel, silty w/sand (33-28% gravel, 27--26% sand, 46-60% fines); max size 15", 3 1/2"-6", 8 1/2 3-6"; color grades from brown to gray with depth; moist-wet; permeability varies from impermeable to rapid; non-plastic; dense-very dense; silty till; DS 204.1 (gray), 206.1 (brown); (GM)

I
Silt and clay, sandy w/gravel (20-20% gravel, 20-25% sand; 53-52% fines); max size 6", 2 1/2"-3" brown-yellow brown; moist; moderate permeability; non-plastic to LL-23, PI-6; hard; colluvial; DS 202.1 (ML), 7.1 (CL-ML)

J
Silt and clay, gravelly, w/sand (25% gravel, 19% sand, 56% fines); max size 3"; red-brown; moist; slight permeability; LL-32, PI-11; very stiff; lacustrine; DS 102.1 (CL-ML)

K
Silt, sandy (1% gravel, 38% sand, 61% fines); max size 3/4"; brown; wet-saturated; rapid permeability; non-plastic; medium-dense; lacustrine; DS 301.2 (ML)

L
Silt, sandy w/gravel (12-11% gravel, 15-12% sand, 76-74% fines); max size 1"; brown-yellow brown; moist; moderate permeability; non-plastic; loose-medium; colluvial; DS 205.1 and "MR" (ML)

M
Silt and clay, sandy (2% gravel, 6% sand, 92% fines); max size 3/4"; brown; moist-saturated; slight-moderate permeability; LL-36, PI-13; very stiff; lacustrine; DS 206.1 (CL-ML)

N
Silt (100% fines); max size 2 mm.; gray and brown; moist-saturated; slight-moderate permeability; non-plastic; dense; lacustrine; DS's 4.1 and 301.1 (ML)

O
Topsoil, gravelly in flood plain; some roots and organic material; brown; moist; medium to rapid permeability; loose; avg. thickness ~ 1.0'

P
Gravel, sandy w/silt (est. 55% gravel, 30% sand, 15% fines); max. size 20"; 5 1/2"-4", 15 1/2 3-6"; gray-brown; moist; rapid permeability; non-plastic; very, very dense (n>100); cemented alluvial gravel; stratified. (GM)

NATURAL DEPOSITIONS

TP #1, C/L Dan 8/26/68 DBC 1367.6

0.0	1.0	Material L (Topsoil)
1.0	3.0	" 1 (ML)
3.0	11.0	" 8 (GM-GP)
11.0	13.0	" 8 (ML)

Note: Dry pit.

TP #2, C/L Dan 8/26/68 DBC 1367.6

0.0	1.0	Material L (Topsoil)
1.0	1.8"	" 1 (ML)
1.8	3.0	" 8 (GM-GP)
3.0	10.5	" A (GM-GP)
10.5	13.0	" K (ML)

Note: Water level @ 10.0'

TP #3, C/L Dan 8/30/68 DBC 1364.8

0.0	1.0	Material L (Topsoil)
1.0	11.7	" A (GM-GP)
11.7	15.2	" K (ML)

Note: Dry pit

TP #4, C/L Dan 8/27/68 DBC 1360.4

0.0	1.0	Material L (Topsoil)
1.0	6.2	" A (GM-GP)
6.2	9.2	" AAC (GM-GP, SM-SW)
9.2	16.5	" K (ML) D.S. 4.1

Note: Water level @ 8.0'

TP #5, C/L Dan 8/27/68 DBC 1357.8

0.0	0.5	Material L (Topsoil)
0.5	4.0	" A (GM-GP)
4.0	7.5	" C (SM-SW) D.S. 5.1
7.5	12.0	" K & M interbeds (ML)

Note: Water level @ 4.0'. Materials "A" & "C" are often rhythmically bedded.

TP #6, C/L Dan 8/27/68 DBC 1353.3

0.0	3.0	Material A (GM-GP)
3.0	11.0	" B (GM)

Note: Water level @ surface (pit in stream). Break based on degree of difficulty of digging.

TP #7, C/L Dan 8/27/68 DBC 1379.3

0.0	1.0	Material L (Topsoil)
1.0	12.0	" F (CL-ML) D.S. 7.1
12.0	14.0	" D (SC-SM) D.S. 7.2

Note: Shall keep @ 11.0'. Starts to slough @ 9.7'

TP #101, Borrow Area 8/29/68 DBC 1367.7

0.0	1.0	Material L (Topsoil)
1.0	12.0	" E (GM, brown)

Note: Dry pit.

TP #102, Borrow Area 8/24/68 DBC 1372.1

0.0	1.0	Material L (Topsoil)
1.0	2.0	" 7 (ML)
2.0	5.0	" A (GM-GP)
5.0	7.0	" C (CL-ML) D.S. 102.1
7.0	12.0	" E (GM)(brown)

Note: Water level @ 7.0'

TP #103, Borrow Area 8/24/68 DBC 1372.1

0.0	1.0	Material L (Topsoil)
1.0	2.0	" 1 (ML)
2.0	6.0	" 8 (GM-GP)
6.0	14.0	" E (GM) brow

Note: Dry pit

TP #201 Emergency Spillway 8/29/68

0.0	1.5	Material L (Topsoil)
1.5	17.0	" E (GM) brow

Note: Dry pit

TP #202 Emergency Spillway 8/29/68

0.0	1.0	Material L (Topsoil)
1.0	2.5	" F (ML) D.
2.5	5.0	" 1 (ML)
5.0	8.0	" A (GM-GP)
8.0	16.0	" E (GM) brow
16.0	18.0	" E (GM) are

Note: Dry pit

TP #203 Emergency Spillway 8/24/68

0.0	1.0	Material L (Topsoil)
1.0	3.0	" 1 (ML)
3.0	7.0	" B (GM-GP)
7.0	16.0	" E (GM) brow

Note: Slight seep @ 13.0'. Interbed materials but not very distinct

TP #204 Emergency Spillway 5/24/68

0.0	1.0	Material L (Topsoil)
1.0	10.0	" E (GM) brow
10.0	14.4	" E (GM) grav
14.4	17.0	" E (GM) brow

Note: Water level at 17.0 sandier between 14.4

TP #205 Emergency Spillway 8/19/68

0.0	0.5	Material L (Topsoil)
0.5	1.8	" 1 (ML) D.
1.8	11.0	" B (GM-GP)
11.0	15.0	" E (GM) brow

Note: Dry pit. Soil scientist c (Mat'l 1) the B; horizon. Fall phase and DS 201.1 is horizon of the C & F

TP #206 Emergency Spillway 8/25/68

0.0	0.7	Material L (Topsoil)
0.7	1.8	" 1 (ML)
1.8	9.0	" B (GM-GP)
9.0	16.0	" E (GM) brow

Note: Dry pit

TP #207 Emergency Spillway 5/24/68

0.0	1.0	Material L (Topsoil)
1.0	2.0	" 1 (ML)
2.0	6.0	" E (GM-GP)
6.0	14.7	" E (GM) brow
14.7	16.0	" J (CL-ML)

Note: Slight seep @ 14.5'

TP #200 Emergency Spillway 8/29/68 DBC 1389.0

0.0 1.0 Material L (Topsoil)
1.0 2.0 " 1 (ML)
2.0 6.0 " B (GM-GP)
6.0 14.0 " E (GM) brown

Note: Dry pit

TP #201 Emergency Spillway 8/29/68 DBC 1389.0

0.0 1.0 Material L (Topsoil)
1.0 17.0 " E (GM) brown

Note: Dry pit

TP #202 Emergency Spillway 8/29/68 DBC 1414.2

0.0 1.0 Material L (Topsoil)
1.0 2.5 " F (ML) D.S. 202.1
2.5 4.0 " 1 (ML)
4.0 8.0 " A (GM-GP) D.S. 202.2
8.0 16.0 " E (GM) brown
16.0 18.0 " E (GM) gray

Note: Dry pit

TP #203 Emergency Spillway 8/29/68 DBC 1389.1

0.0 1.0 Material L (Topsoil)
1.0 3.0 " 1 (ML)
3.0 7.0 " B (GM-GP)
7.0 11.0 " E (GM) brown

Note: Slight seep @ 13.0'. Break between materials B and E is not very distinct

TP #204 Emergency Spillway 5/24/68 DBC 1401.0

0.0 1.0 Material L (Topsoil)
1.0 10.0 " E (GM) brown
10.0 14.4 " E (GM) gray D.S. 204.1
14.4 17.0 " E (GM) brown

Note: Water level at 17.0'. Material E is sandier between 14.4 and 17.0'

TP #205 Emergency Spillway 5/24/68 DBC 1357.1

0.0 1.0 Material L (Topsoil)
0.5 1.5 " 1 (ML) D.S. 205.1
1.5 11.0 " B (GM-GP) D.S. 205.2
11.0 15.0 " E (GM) brown

Note: Dry pit. Soil scientist calls DS 205.1 (Mat'l 1) the Big horizon of the Chenango Fan phase and DS 205.2 (Mat'l B) the IIC horizon of the Chenango Fan phase.

TP #206 Emergency Spillway 8/29/68 DBC 1400.2

0.0 0.5 Material L (Topsoil)
0.5 1.5 " 1 (ML)
1.5 4.0 " B (GM-GP)
4.0 16.0 " E (GM) Brown D.S. 206.1

Note: Dry pit

TP #207 Emergency Spillway 5/24/68 DBC 1381.2

0.0 1.0 Material L (Topsoil)
1.0 2.0 " 1 (ML)
2.0 6.0 " E (GM-GP)
6.0 14.7 " E (GM) brown
14.7 16.0 " J (CL-ML)

Note: Slight seep @ 14.5'

TP #208 Emergency Spillway 8/29/68 DBC 1385.8

0.0 0.5 Material L (Topsoil)
0.5 1.5 " 1 (ML)
1.5 6.0 " B (GM-GP)
6.0 12.0 " E (GM) brown
12.0 15.0 " J (CL-ML) DS 208.1

Note: Water level @ 12.0'. Material E is siltier than usual.

TP #209 Emergency Spillway 8/29/68 DBC 1385.8

0.0 0.8 Material L (Topsoil)
0.8 3.5 " B (GM-GP)
3.5 7.0 " E (GM) brown
7.0 9.8 " E (GM) brown
9.8 15.5 " J (CL-ML)

Note: Water level @ 9.3'. Material E is siltier than usual (same as TP208) from 7.0-9.8'. Some cobbles and sandy streaks in material J. Lots of flat, angular 3-4" cobbles near bottom

TP #210 Emergency Spillway 8/29/68 DBC 1392.1

0.0 1.0 Material L (Topsoil)
1.0 1.7 " 1 (ML)
1.7 4.0 " B (GM-GP)
4.0 4.7 " E (GM) brown
4.7 16.0 " E (GM) brown

Note: Dry pit. Material E is siltier from 4.0-4.7'.

TP #211 Prit. Spwy (Initial) 5/24/68 DBC 1356.4

0.0 0.5 Material L (Topsoil)
0.5 4.5 " A (GM-GP)
4.5 6.5 " C (SM-SW)
6.5 12.0 " K&N interbeds (ML) DS 301.1, 301.2

Note: Water level @ 6.5'. Materials B & N are rhythmically bedded, with DS 301.1 representing the finer fraction and DS 301.2 representing the coarser fraction.

TP #212 Prit. Spwy (Initial) 5/24/68 DBC 1356.2

0.0 1.0 Material L (Topsoil)
1.0 4.0 " A (GM-GP)
4.0 13.0 " K&N interbeds (ML)

Note: Water level @ 4.0'

TP #213 Out. Chan. (Initial) 5/24/68 DBC 1357.4

0.0 1.0 Material L (Topsoil)
1.0 7.0 " A (GM-GP)
7.0 12.0 " K&N interbeds (ML)
12.0 15.0 " A (GM-GP)

Note: Water level @ 5.4'

TP #214 Out. Chan. (Initial) 5/24/68 DBC 1351.5

0.0 1.0 Material L (Topsoil)
1.0 7.0 " A (GM-GP)
7.0 11.0 " K&N interbeds (ML)

Note: Water level @ 2.5'

TP #215 Out. Chan. (Initial) 5/24/68 DBC 1351.5

0.0 1.0 Material L (Topsoil)
1.0 1.0 " 1 (ML)
2.0 12.0 " A (GM-GP)
12.0 14.0 " E (ML)

Note: Water level @ 11.0'

TP #216 Drain Line 5/24/68 DBC 1381.4

0.0 1.0 Material L (Topsoil)
1.0 10.5 " A (GM-GP)
10.5 16.0 " E (ML)

Note: Water level @ 10.0'

TP #217 Drain Line 5/24/68 DBC 1381.4

0.0 11.0 Material A (GM-GP) D.S. 201.1
11.0 12.0 " K&N interbeds (ML)

Note: Water level @ 11.0'

TP #218 Drain Line 5/24/68 DBC 1381.4

0.0 1.0 Material L (Topsoil)
1.0 4.0 " A (GM-GP)
5.0 14.0 " M (GM)

Note: Dry pit. Hard digging in Material M. DS "M" from the above pit 504. See plan & profiles.

8/22/77
AS BUILT

CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUE COUNTY, NEW YORK
LOGS OF TEST HOLES
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

By *James Champion* 9/8/68
GEOLOGIST
By *L. Sandberg* 10/69
STATE CONS ENGINEER
NY 216-P

B-27

DRILL HOLE LOGS			DRILL HOLE LOGS			DRILL HOLE LOGS		
DM #1 C/L Den 9/13/68 DBC	Elev. 1311.0	0.0	DM #23 C/L Den 9/12/68 DBC	Elev. 1311.2	0.0	DM #34 C/L Den 9/18/68 DBC	Elev. 1311.2	0.0
Material L (Topsoil)			Material L (Topsoil)			Material L (Topsoil)		
1.5			1.5			1.5		
2.4			2.4			2.4		
2.9			2.9			2.9		
3.1			3.1			3.1		
3.2			3.2			3.2		
3.3			3.3			3.3		
3.4			3.4			3.4		
3.5			3.5			3.5		
3.6			3.6			3.6		
3.7			3.7			3.7		
3.8			3.8			3.8		
3.9			3.9			3.9		
4.0			4.0			4.0		
4.1			4.1			4.1		
4.2			4.2			4.2		
4.3			4.3			4.3		
4.4			4.4			4.4		
4.5			4.5			4.5		
4.6			4.6			4.6		
4.7			4.7			4.7		
4.8			4.8			4.8		
4.9			4.9			4.9		
5.0			5.0			5.0		
5.1			5.1			5.1		
5.2			5.2			5.2		
5.3			5.3			5.3		
5.4			5.4			5.4		
5.5			5.5			5.5		
5.6			5.6			5.6		
5.7			5.7			5.7		
5.8			5.8			5.8		
5.9			5.9			5.9		
6.0			6.0			6.0		
6.1			6.1			6.1		
6.2			6.2			6.2		
6.3			6.3			6.3		
6.4			6.4			6.4		
6.5			6.5			6.5		
6.6			6.6			6.6		
6.7			6.7			6.7		
6.8			6.8			6.8		
6.9			6.9			6.9		
7.0			7.0			7.0		
7.1			7.1			7.1		
7.2			7.2			7.2		
7.3			7.3			7.3		
7.4			7.4			7.4		
7.5			7.5			7.5		
7.6			7.6			7.6		
7.7			7.7			7.7		
7.8			7.8			7.8		
7.9			7.9			7.9		
8.0			8.0			8.0		
8.1			8.1			8.1		
8.2			8.2			8.2		
8.3			8.3			8.3		
8.4			8.4			8.4		
8.5			8.5			8.5		
8.6			8.6			8.6		
8.7			8.7					

DH #27 Elev. Spwy. 9/13/68 DBC Elev. 133.8			DH #28 Elev. Spwy. 9/13-16/68 DBC Elev. 140.7		
1	Material L (Topsoil)	0.0	11	Material L (Topsoil)	0.0
10	E (GM-GP)	3.3	12	1.5	1.5
12	3'-0" 3/15/68 5 day	4.7	13	4'-0" 4/15/68 7 day	4.7
15	5.5	5.5	14	1.5	1.5
18			15	1.5	1.5
20			16	1.5	1.5
22			17	1.5	1.5
24			18	1.5	1.5
26			19	1.5	1.5
28			20	1.5	1.5
30			21	1.5	1.5
32			22	1.5	1.5
34			23	1.5	1.5
36			24	1.5	1.5
38			25	1.5	1.5
40			26	1.5	1.5
42			27	1.5	1.5
44			28	1.5	1.5
46			29	1.5	1.5
48			30	1.5	1.5
50			31	1.5	1.5
52			32	1.5	1.5
54			33	1.5	1.5
56			34	1.5	1.5
58			35	1.5	1.5
60			36	1.5	1.5
62			37	1.5	1.5
64			38	1.5	1.5
66			39	1.5	1.5
68			40	1.5	1.5
70			41	1.5	1.5
72			42	1.5	1.5
74			43	1.5	1.5
76			44	1.5	1.5
78			45	1.5	1.5
80			46	1.5	1.5
82			47	1.5	1.5
84			48	1.5	1.5
86			49	1.5	1.5
88			50	1.5	1.5
90			51	1.5	1.5
92			52	1.5	1.5
94			53	1.5	1.5
96			54	1.5	1.5
98			55	1.5	1.5
100			56	1.5	1.5
102			57	1.5	1.5
104			58	1.5	1.5
106			59	1.5	1.5
108			60	1.5	1.5
110			61	1.5	1.5
112			62	1.5	1.5
114			63	1.5	1.5
116			64	1.5	1.5
118			65	1.5	1.5
120			66	1.5	1.5
122			67	1.5	1.5
124			68	1.5	1.5
126			69	1.5	1.5
128			70	1.5	1.5
130			71	1.5	1.5
132			72	1.5	1.5
134			73	1.5	1.5
136			74	1.5	1.5
138			75	1.5	1.5
140			76	1.5	1.5
142			77	1.5	1.5
144			78	1.5	1.5
146			79	1.5	1.5
148			80	1.5	1.5
150			81	1.5	1.5
152			82	1.5	1.5
154			83	1.5	1.5
156			84	1.5	1.5
158			85	1.5	1.5
160			86	1.5	1.5
162			87	1.5	1.5
164			88	1.5	1.5
166			89	1.5	1.5
168			90	1.5	1.5
170			91	1.5	1.5
172			92	1.5	1.5
174			93	1.5	1.5
176			94	1.5	1.5
178			95	1.5	1.5
180			96	1.5	1.5
182			97	1.5	1.5
184			98	1.5	1.5
186			99	1.5	1.5
188			100	1.5	1.5
190			101	1.5	1.5
192			102	1.5	1.5
194			103	1.5	1.5
196			104	1.5	1.5
198			105	1.5	1.5
200			106	1.5	1.5
202			107	1.5	1.5
204			108	1.5	1.5
206			109	1.5	1.5
208			110	1.5	1.5
210			111	1.5	1.5
212			112	1.5	1.5
214			113	1.5	1.5
216			114	1.5	1.5
218			115	1.5	1.5
220			116	1.5	1.5
222			117	1.5	1.5
224			118	1.5	1.5
226			119	1.5	1.5
228			120	1.5	1.5
230			121	1.5	1.5
232			122	1.5	1.5
234			123	1.5	1.5
236			124	1.5	1.5
238			125	1.5	1.5
240			126	1.5	1.5
242			127	1.5	1.5
244			128	1.5	1.5
246			129	1.5	1.5
248			130	1.5	1.5
250			131	1.5	1.5
252			132	1.5	1.5
254			133	1.5	1.5
256			134	1.5	1.5
258			135	1.5	1.5
260			136	1.5	1.5
262			137	1.5	1.5
264			138	1.5	1.5
266			139	1.5	1.5
268			140	1.5	1.5
270			141	1.5	1.5
272			142	1.5	1.5
274			143	1.5	1.5
276			144	1.5	1.5
278			145	1.5	1.5
280			146	1.5	1.5
282			147	1.5	1.5
284			148	1.5	1.5
286			149	1.5	1.5
288			150	1.5	1.5
290			151	1.5	1.5
292			152	1.5	1.5
294			153	1.5	1.5
296			154	1.5	1.5
298			155	1.5	1.5
300			156	1.5	1.5
302			157	1.5	1.5
304			158	1.5	1.5
306			159	1.5	1.5
308			160	1.5	1.5
310			161	1.5	1.5
312			162	1.5	1.5
314			163	1.5	1.5
316			164	1.5	1.5
318			165	1.5	1.5
320			166	1.5	1.5
322			167	1.5	1.5
324			168	1.5	1.5
326			169	1.5	1.5
328			170	1.5	1.5
330			171	1.5	1.5
332			172	1.5	1.5
334			173	1.5	1.5
336			174	1.5	1.5
338			175	1.5	1.5
340			176	1.5	1.5
342			177	1.5	1.5
344			178	1.5	1.5
346			179	1.5	1.5
348			180	1.5	1.5
350			181	1.5	1.5
352			182	1.5	1.5
354			183	1.5	1.5
356			184	1.5	1.5
358			185	1.5	1.5
360			186	1.5	1.5
362			187	1.5	1.5
364			188	1.5	1.5
366			189	1.5	1.5
368			190	1.5	1.5
370			191	1.5	1.5
372			192	1.5	1.5
374			193	1.5	1.5
376			194	1.5	1.5
378			195	1.5	1.5
380			196	1.5	1.5
382			197	1.5	1.5
384			198	1.5	1.5
386			199	1.5	1.5
388			200	1.5	1.5
390			201	1.5	1.5
392			202	1.5	1.5
394			203	1.5	1.5
396			204	1.5	1.5
398			205	1.5	1.5
400			206	1.5	1.5
402			207	1.5	1.5
404			208	1.5	1.5
406			209	1.5	1.5
408			210	1.5	1.5
410			211	1.5	1.5
412			212	1.5	1.5
414			213	1.5	1.5
416			214	1.5	1.5
418			215	1.5	1.5
420			216	1.5	1.5
422			217	1.5	1.5
424			218	1.5	1.5
426			219	1.5	1.5
428			220	1.5	1.5
430			221	1.5	1.5
432			222	1.5	1.5
434			223	1.5	1.5
436			224	1.5	1.5
438			225	1.5	1.5
440			226	1.5	1.5
442			227	1.5	1.5
444			228	1.5	1.5
446			229	1.5	1.5
448			230	1.5	1.5
450			231	1.5	1.5
452			232	1.5	1.5
454			233	1.5	1.5
456			234	1.5	1.5
458			235	1.5	1.5
460			236	1.5	1.5
462			237	1.5	1.5
464			238	1.5	1.5
466			239	1.5	1.5
468			240	1.5	1.5
470			241	1.5	1.5
472			242	1.5	1.5
474			243	1.5	1.5
476			244	1.5	1.5
478			245	1.5	1.5
480			246	1.5	1.5
482			247	1.5	1.5
484			248	1.5	1.5
486			249	1.5	1.5
488			250	1.5	1.5
490			251	1.5	1.5
492			252	1.5	1.5
494			253	1.5	1.5
496			254	1.5	1.5
498			255	1.5	1.5
500			256	1.5	1.5
502			257	1.5	1.5
504			258	1.5	1.5
506			259	1.5	1.5
508			260	1.5	1.5
510			261	1.5	1.5
512			262	1.5	1.5
514			263	1.5	1.5
516			264	1.5	1.5
518			265	1.5	1.5
520			266	1.5	1.5
522			267	1.5	1.5
524			268	1.5	1.5
526			269	1.5	1.5
528			270	1.5	1.5
530			271	1.5	1.5
532			272	1.5	1.5
534			273	1.5	1.5
536			274	1.5	1.5
538			275	1.5	1.5
540			276	1.5	1.5
542			277	1.5	1.5
544					

Note: Water level = 3.9', 2 day.

D. #31.1 Prie. Soun. (Indicated) 9/11/65 - DHC 11.1	
23	3.52 fpd
19	
23	
18	
11	
3'	
3'	11.4 fpd
27	
23	
12	
11	0.00 fpd
13	
8	
23	0.79 fpd
10	
4	
12	0.00 fpd
9	
17	
13	
27	12.2 fpd
12	
13	
12	0.00 fpd

Note: Water level @ 2.9', 9/13/65, 1 day.
Co rd @ 3.0', 9/13/65, 1 day.

D. #31.1 Prie. Soun. (Indicated) 9/13/65 - DHC 11.1	
18	1.01 9/18/65 1 day
18	Material A (Q1-QP)
16	
19	8.42 fpd
22	
12	
48	
48	2.15 fpd
58	
117	
150/2	
Aug.	
243	8.56 fpd
Aug.	
199/2	15.9 fpd
Aug.	

Note: Water level accurate.

D. #31.1 Prie. Soun. (Indicated) 5/14/65 Ind.	
23	
19	
23	
18	4.64 fpd
11	
3'	
3'	15.4 fpd
27	
23	
74	
138	2.33 fpd
382	
Aug.	
356	2.75 fpd
Aug.	
414	1.25 fpd
Aug.	
250/2	2.50 fpd
Aug.	
321/2	5.39 fpd

Note: Water level accurate.

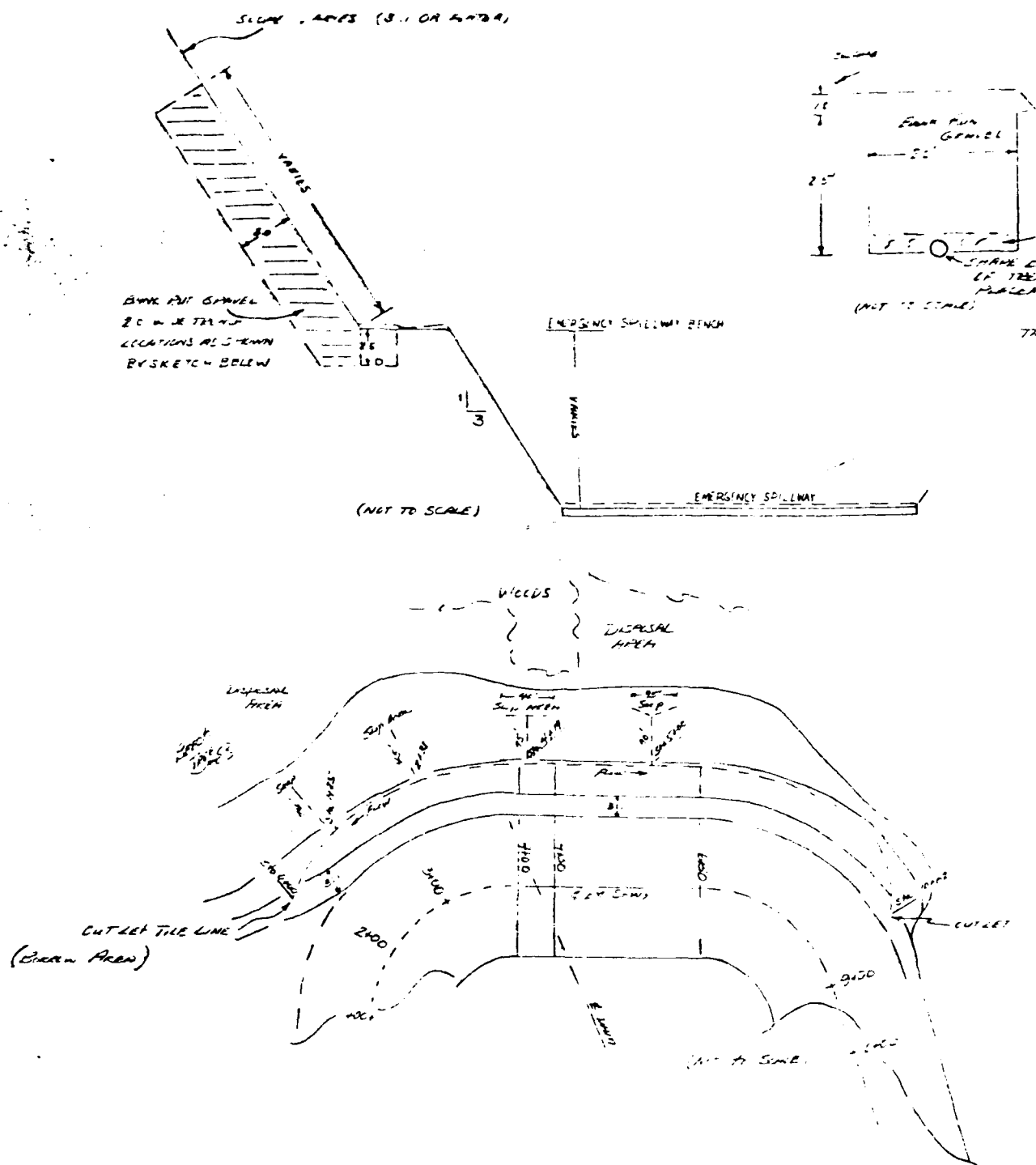
CONEWANGO CREEK WATERSHED PROJECT
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUE COUNTY, NEW YORK
LOGS OF TEST HOLES

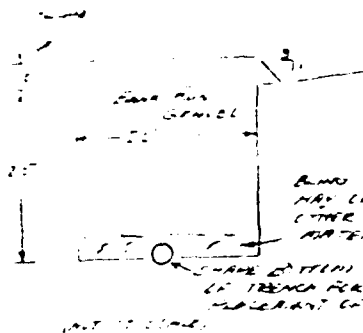
U. S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

By *Bruce Hampton* Date *9.18.65*
TITL GEOLOGIST
By *J. Lindley* Date *10.20.65*
By *L.H. Conley* Date *10.20.65*
STATE CONS. ENGINEER
NY 2161-P

8/22/74
ASTUJ

B-29





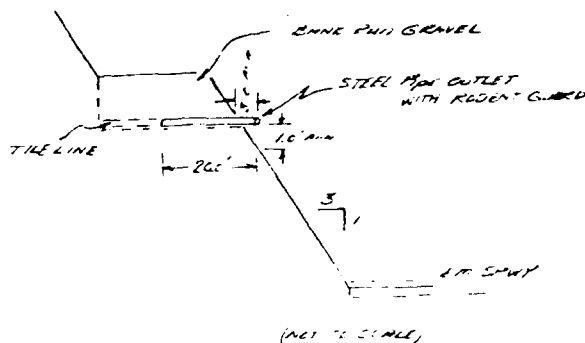
REFER TO CONSTRUCTION PLAN

ROUND TILE WITH
HAY OR STRAW OR
OTHER SUITABLE
MATERIAL - MIN OF 6" OVER TILE

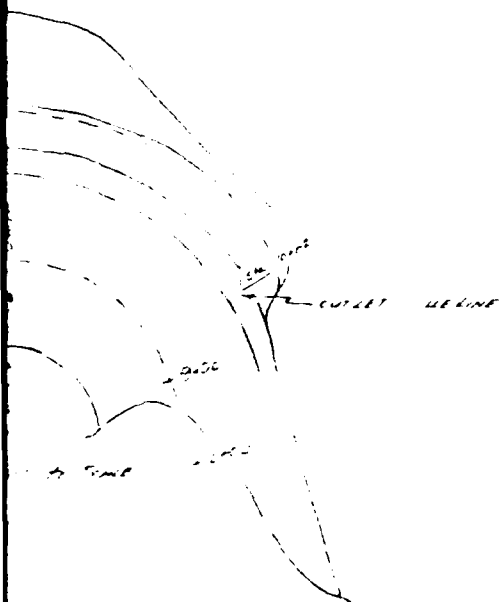
USE 1/4" HOLE 2" DIA
FOR DRAINING TO TILE TRENCH

THE LIVE STAKE MUST BE IN PLACE
FOLLOWING THE 1/4" DIA. WITHIN 24 HRS
AFTER CONSTRUCTION BE 24"

OUTLET DETAIL



EMERGENCY SPILLWAY



LIST OF MATERIALS

4" TILE LINE MATERIAL 100 LBS
CHUNKY PATTI GRAVEL 100 LBS
2 CURTAINS 2 RE' EA
4" STEEL OUTLET PIPE 40 LBS
POLLUT GUARDS 2 NO.
BLANKING PLATE 1 NO.

THIS CONSTRUCTION PLAN IS FOR THE
USE OF THE PROJECT ONLY

CONWAY AND GREEN WATERSHED PROJECT
SITE 9A
FLOODWATER BY ARUNDAM
CHARMINGUA COUNTY NEW YORK
TILE DRAINAGE - EMERGENCY SPILLWAY
U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

8/22/77
AS BUILT

AD-A105 730

ERDMAN ANTHONY ASSOCIATES ROCHESTER NY

F/G 13/13

NATIONAL DAM SAFETY PROGRAM, CONEWANGO CREEK WATERSHED DAM NUMB--ETC(U)

AUG 81 R J FARRELL

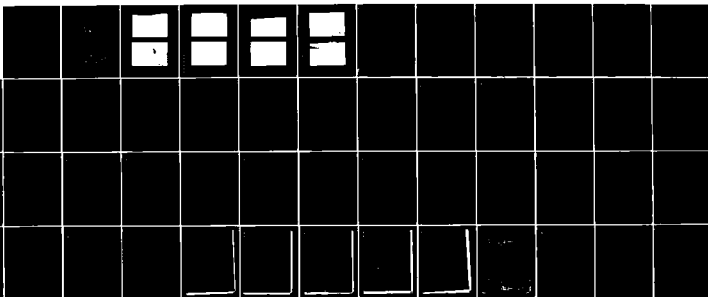
DACW51-81-C-0017

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2 2

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END

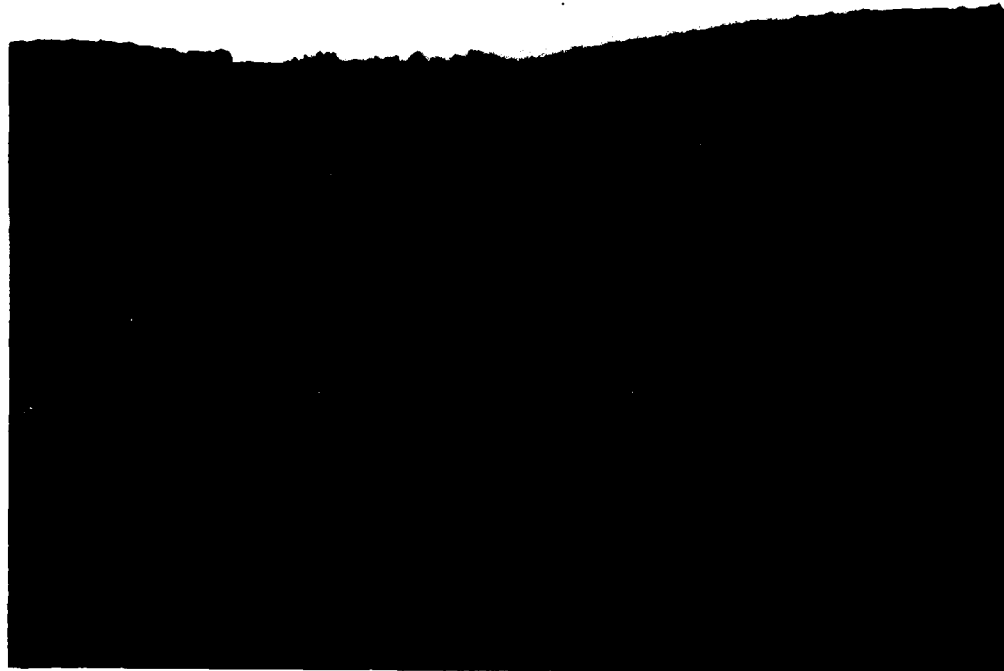
DATE

FILMED

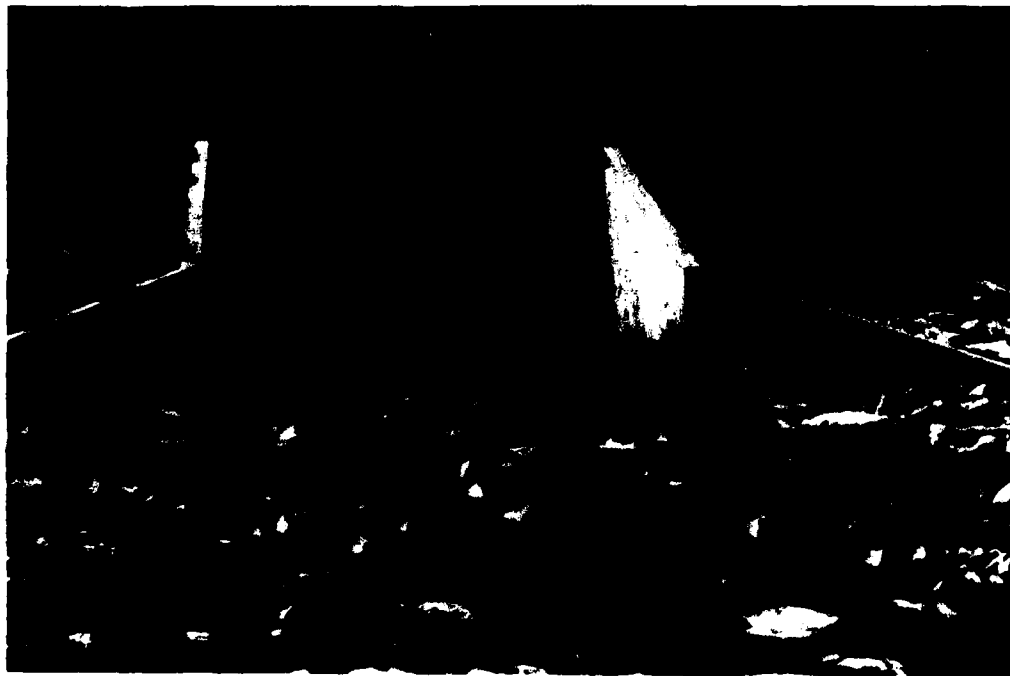
11-81

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APPENDIX C
PHOTOGRAPHS



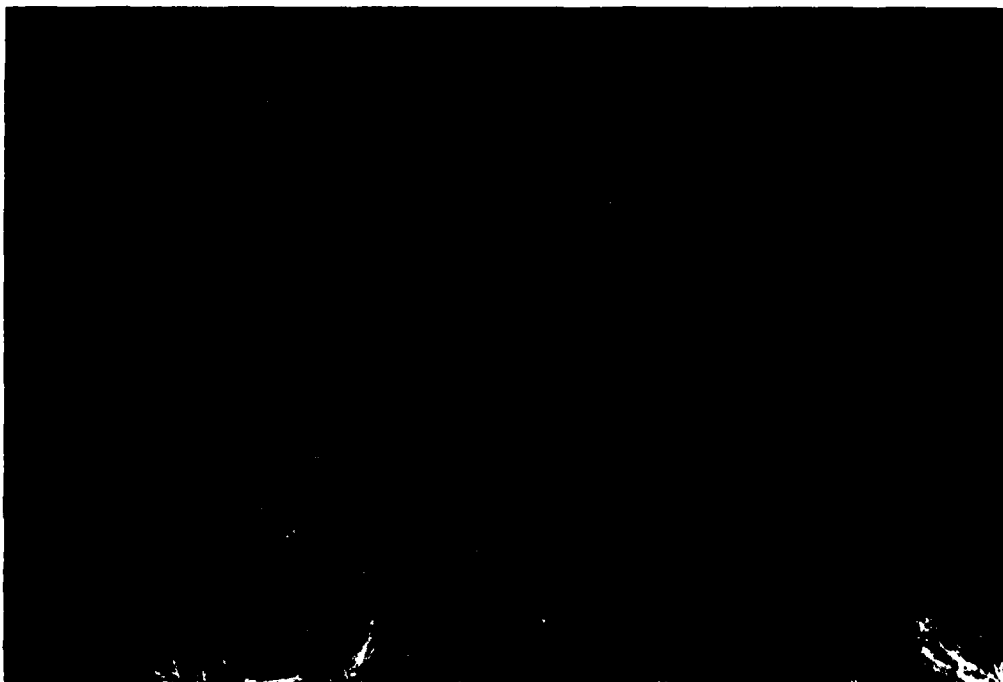
1. Principal spillway inlet structure. Note slide gate stem and lack of access to the top of structure.



2. Principal spillway impact basin



3. Principal spillway inlet structure, showing low stage inlet and trash rack.



4. Upstream slope of dam. Note rutting due to vehicular traffic.



5. Upstream slope of dam. Note debris at recent high water level.



6. Spring in north slope of emergency spillway



7. Upstream slope of dam. Note wave erosion.



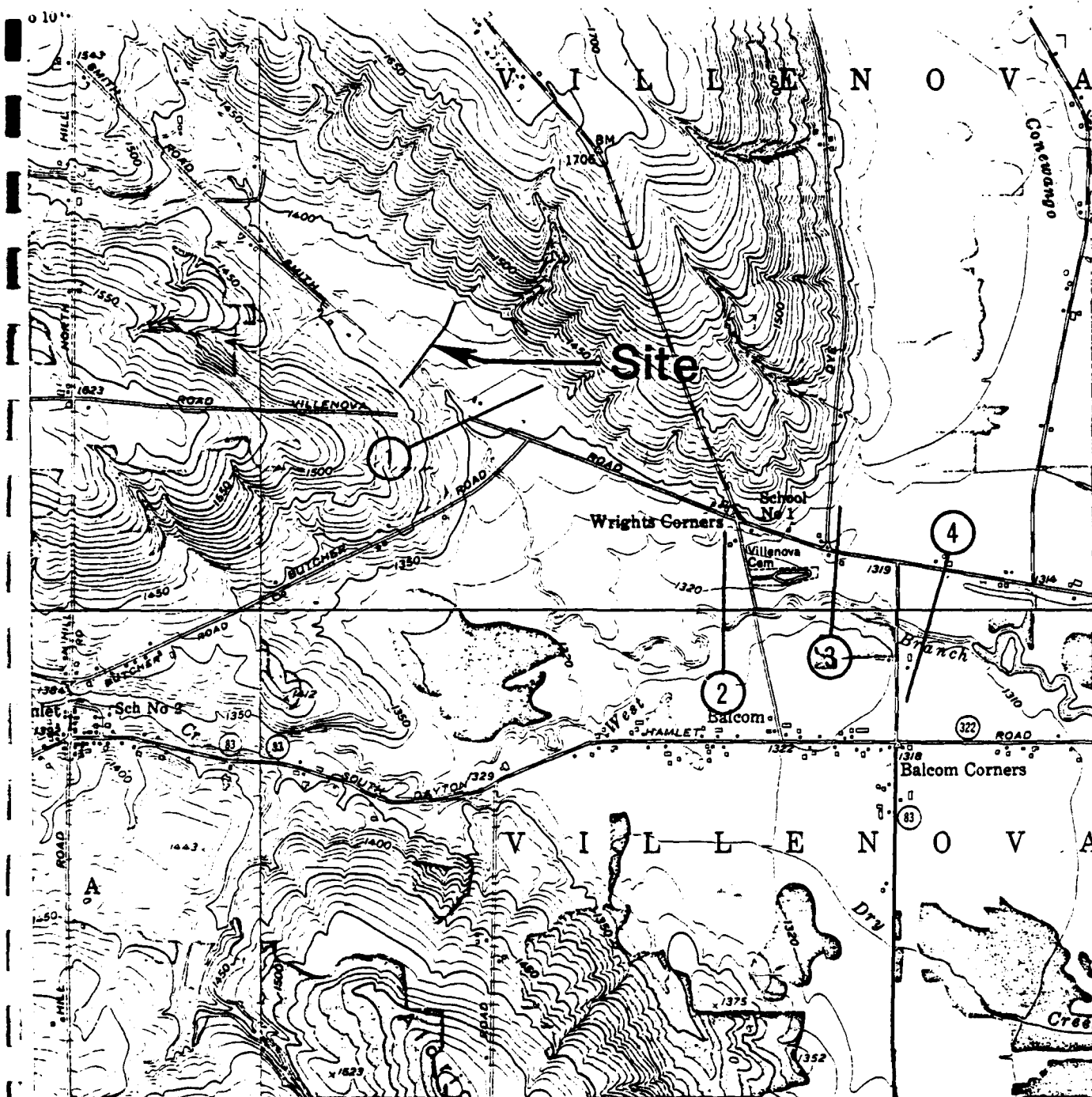
8. Downstream channel. Note minor erosion on right bank of channel.

APPENDIX D

HYDRAULIC AND HYDROLOGIC COMPUTATIONS

APPENDIX D

	<u>PAGE</u>
Cross Section Location Plan	D-2
HEC-1 Dam Safety Version Computer Program-Input	D-3
HEC-1 Dam Safety Version Computer Program-Output	D-5
Supporting Calculations	
o Hydrology	D-14
o Spillway Hydraulics	D-18
o Downstream Channel Routing	D-28
Checklist for Hydrologic and Hydraulic Engineering Data	D-30



Conewango Creek Watershed (Site 9A)

CROSS SECTION LOCATION PLAN

Scale: 1"=2000' D-2

ANALYSIS OF DAM OVERTOPPING USING RATIOS OF PMF
 HYDROLOGIC-HYDRAULIC ANALYSIS OF SAFETY OF CONEWAGO CREEK-SITE 9A
 RATIOS OF PMF ROUTED THROUGH THE RESERVOIR AND DOWNSTREAM

DAM NY 596

0 0 -1

100 0 15

01 5

J 1 6 1

J1 0.2 0.4 0.5 0.6 0.8 1.0 1

K 0 INFLOW

K1 CALCULATION OF INFLOW HYDROGRAPH

M 1 6.0 12.17 0

P 0 22.6 114 124 138 148 1.0 0.1

T 4.08 0.63

U 2.0 -1.0 2.0

X 1 OUTFLOW

K1 COMPUTE OUTFLOW HYDROGRAPH FROM DAM NY596

Y 1

Y1 1381 1382 1383 1384 1385 1387 1388 1389 1390 1391

Y4 1391.8 1392 356 467 473 640 1522 2844 4489 6453

Y5 110 205

Y5 8200 8550

Y5 40.6 611.9 746.2 964.2

Y5 1366.6 1381 1386.6 1388.7 1391.8

Y5 1386.6

Y5 1391.8 2.7 1.5 1590

K 1

K1 CHANNEL ROUTING -MOD PULS REACH 0-1

Y 1

Y1 1

Y6 0.045 0.04 0.45 1346 1360 670 0.0116

Y7 0 1360 700 1355 1370 1352 1395

Y7 1430 1352 1700 1360 1701 1360

K 0 INFLOW

K1 COMPUTE RUNOFF FROM ADJACENT WATERSHED

M 1 6.17 12.17 0

P 0 22.6 114 124 138 148 1.0 0.1

T 3.96 0.63

U -0.1 2.

X 2 COMBINE HYDROGRAPHS

K1 2

K 1

K1 CHANNEL ROUTING -MOD PULS REACH 1-2

Y 1

Y1 1

Y6 0.045 0.04 0.045 1308 1330 7600 0.0005

Y7 0 1330 700 1320 1300 1314 1340

Y7 1400 1314 2200 1320 2201 1320

K 1

K1 CHANNEL ROUTING -MOD PULS REACH 2-3

Y 1

Y1 1

Y6 0.045 0.04 0.045 1304 1322 1800 0.0022

Y7 0 1320 700 1322 880 1320

Y7 1370 1304 1360 1314 2200 1322

K 1

K1 CHANNEL ROUTING -MOD PULS REACH 3-4

V 1

V1 1

V6 0.045

V7 0

V7 1900

K 99

A

0.04

1315

1315

0.045

1200

2900

1310

1302

1312

1500

1302

1318

0.0013

1295

1302

1320

1312

OK. SFG #HEC108

OK. SEG #HEC108
ENTER PROJECT NUMBER
80166-08.09
INPUT FILE ? NYS96
1.....
FLOOD HYDROGRAPH PACKAGE (HEC-1)
DAM SAFETY VERSION JULY 1978
LAST MODIFICATION 26 FEB 79
.....

PREVIEW OF SEQUENCE OF STREAM NETWORK CALCULATIONS
1
RUNOFF HYDROGRAPH AT INFLOW
ROUTE HYDROGRAPH TO UTIFLOW
ROUTE HYDROGRAPH TO 1
RUNOFF HYDROGRAPH AT INFLOW
COMBINE 2 HYDROGRAPHS AT DMBINE 2
ROUTE HYDROGRAPH TO 3
ROUTE HYDROGRAPH TO 4
END OF NETWORK.

1.....
FLOOD HYDROGRAPH PACKAGE (HEC-1)
DAM SAFETY VERSION JULY 1978
LAST MODIFICATION 26 FEB 79
.....

RUN DATE: 6/10/
TIME: 8:55 AM

ANALYSIS OF DAM OVERTOPPING USING RATIOS OF PMF DAM NY 596
HYDROLOGIC-HYDRAULIC ANALYSIS OF SAFETY OF CONEWAGO CREEK-SITE 9A
RATIOS OF PMF ROUTED THROUGH THE RESERVOIR AND DOWNSTREAM

JOB SPECIFICATION									
NO	NHR	NMIN	1DAY	IHR	IMIN	METRC	IPLT	IFRT	NSTAN
100	0	15	0	0	0	0	-1	4	0
	JOPER		5	NWT	LROPT	TRACE			
				0	0	0			

MULTI-PLAN ANALYSES TO BE PERFORMED
RTIOS= 0.20 0.40 0.50 0.60 0.80 1.00
NPLAN= 1 NRTIO= 6 LRTIO= 1

SUR-AREA RUNOFF COMPUTATION

CALCULATION OF INFLOW HYDROGRAPH									
INFLW	ISTAG	ICOMP	IECON	ITAPE	JPLT	JPRT	INAME	ISTAGE	IAUTO
0	0	0	0	0	0	0	1	0	0

HYDROGRAPH DATA

INYOG	IUNG	TAREA	SNAP	TRSDA	TRSPC	RATIO	ISNOW	ISAME	LOCAL

OK, SEE #MEC10R

PAGE 0002

1 1 6.00 0.00 12.17 0.00 0.00 0 1 0

PRECIP DATA
R6 R12 R24 R48 R72 R96
0.00 22.60 114.00 124.00 130.00 148.00 0.00 0.00 0.00

TRAPC COMPUTED BY THE PROGRAM IS 0.007

LOSS DATA
LROPT STRKR OLTKR RTIOL ERRAIN STRKS RTIOK STRTL CNSTL ALSMX RTIMP
0 0.00 0.00 1.00 0.00 0.00 1.00 1.00 0.10 0.00 0.00

UNIT HYDROGRAPH DATA
TP= 4.00 CP=0.63 NTA= 0

RECESSION DATA
STRTO= 2.00 QRC5N= -0.10 RTIOR= 2.00

UNIT HYDROGRAPH 89 END-OF-PERIOD ORDINATES, LAG= 4.09 HOURS, CP= 0.64 VCL= 1.00

9.	35.	73.	117.	166.	218.	273.	330.	388.	445.
496.	537.	571.	596.	613.	621.	619.	603.	571.	534.
499.	467.	436.	408.	381.	356.	333.	312.	291.	272.
255.	238.	222.	208.	194.	182.	170.	159.	149.	139.
130.	121.	113.	106.	99.	93.	87.	81.	76.	71.
66.	62.	58.	54.	51.	47.	44.	41.	39.	36.
34.	32.	30.	28.	26.	24.	23.	21.	20.	18.
17.	16.	15.	14.	13.	12.	11.	10.	9.	9.
9.	8.	8.	7.	7.	6.	6.	5.	5.	4.

MO.DA HR.MN PERIOD RAIN EXCS LOSS END-OF-PERIOD FLOW NO.DA HR.MN PERIOD RAIN EXCS LOSS CCHF 0
SUM 26.99 23.23 3.76 290432.
(685.)(596.)(95.)(8224.11)

HYDROGRAPH ROUTING

COMPUTE OUTFLOW HYDROGRAPH FROM DAM NY596

ISTAQ ICOMP IRECON ITAPE JPLI JPR1 INAPE ISTAGE IAU0
0 0 0 0 0 0 0 0 0 0
ROUTING DATA
IRES ISAME IOPT IPMP LSTR
1 1 0 0 0
LAG AMSKK X TSK STORA ISPRAT
0 0.000 0.000 0.000 -1367. -1

STAGE	1381.00	1382.00	1383.00	1384.00	1385.00	1387.00	1388.00	1389.00	1390.00	1391.00
FLOW	8200.00	205.00	356.00	467.00	473.00	640.00	1522.00	2844.00	4489.00	6451.00
CAPACITY=	41.	416.	612.	746.	964.					

CNEL	SPWID	COGV	EXPV	ELEV	COOL	CAREA	EXFL
1386.6	0.0	0.0	0.0	0.0	0.0	0.0	0.0

PEAK OUTFLOW IS	1442. AT TIME	46.00 HOURS
PEAK OUTFLOW IS	4010. AT TIME	44.25 HOURS
PEAK OUTFLOW IS	5116. AT TIME	44.00 HOURS
PEAK OUTFLOW IS	6167. AT TIME	44.00 HOURS
PEAK OUTFLOW IS	8259. AT TIME	43.75 HOURS
PEAK OUTFLOW IS	10423. AT TIME	43.75 HOURS

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TESTING	STAG	ICOMP	IECON	ITAPE	JPLY	JPRT	INAVE	ISTAGE	IAUTO
1	1	1	0	0	0	0	1	0	0

QLOSS	CLOSS	AVG	ROUTING DATA	
6.6	6.000	0.000	IRIS	ISAME
			1	1
	NSTPS	NSTOL	LAG	APSKK
	1	0	0	0.000

NORMAL DEPTH CHANNEL ROUTING

QN(1)	QN(2)	QN(3)	ELNVT	ELMAX	RLNTH	SEL
0.0450	0.0400	0.0450	1346.0	1360.0	670.	0.01160

CROSS SECTION COORDINATES--STA.ELEV,STA.ELEV--ETC

CROSS SECTION COORDINATES--STA,ELEV,STA,ELEV--ETC	0+00	1369.00	700.00	1355.00	1370.00	1352.00	1395.00	1346.00	1420.00	1346.00
	1430.00	1352.00	1780.00	1360.00	1701.00	1360.00				

	1979	1980	1981	1982	1983	1984	1985	1986	1987	1988	1989	1990	1991	1992	1993	1994	1995	1996	1997	1998	1999	2000	2001	2002	2003	2004	2005	2006	2007	2008	2009	2010	2011	2012	2013	2014	2015	2016	2017	2018	2019	2020	2021	2022	2023	2024	2025	2026	2027	2028	2029	2030	2031	2032	2033	2034	2035	2036	2037	2038	2039	2040	2041	2042	2043	2044	2045	2046	2047	2048	2049	2050	2051	2052	2053	2054	2055	2056	2057	2058	2059	2060	2061	2062	2063	2064	2065	2066	2067	2068	2069	2070	2071	2072	2073	2074	2075	2076	2077	2078	2079	2080	2081	2082	2083	2084	2085	2086	2087	2088	2089	2090	2091	2092	2093	2094	2095	2096	2097	2098	2099	2100	2101	2102	2103	2104	2105	2106	2107	2108	2109	2110	2111	2112	2113	2114	2115	2116	2117	2118	2119	2120	2121	2122	2123	2124	2125	2126	2127	2128	2129	2130	2131	2132	2133	2134	2135	2136	2137	2138	2139	2140	2141	2142	2143	2144	2145	2146	2147	2148	2149	2150	2151	2152	2153	2154	2155	2156	2157	2158	2159	2160	2161	2162	2163	2164	2165	2166	2167	2168	2169	2170	2171	2172	2173	2174	2175	2176	2177	2178	2179	2180	2181	2182	2183	2184	2185	2186	2187	2188	2189	2190	2191	2192	2193	2194	2195	2196	2197	2198	2199	2200	2201	2202	2203	2204	2205	2206	2207	2208	2209	2210	2211	2212	2213	2214	2215	2216	2217	2218	2219	2220	2221	2222	2223	2224	2225	2226	2227	2228	2229	2230	2231	2232	2233	2234	2235	2236	2237	2238	2239	2240	2241	2242	2243	2244	2245	2246	2247	2248	2249	2250	2251	2252	2253	2254	2255	2256	2257	2258	2259	2260	2261	2262	2263	2264	2265	2266	2267	2268	2269	2270	2271	2272	2273	2274	2275	2276	2277	2278	2279	2280	2281	2282	2283	2284	2285	2286	2287	2288	2289	2290	2291	2292	2293	2294	2295	2296	2297	2298	2299	2300	2301	2302	2303	2304	2305	2306	2307	2308	2309	2310	2311	2312	2313	2314	2315	2316	2317	2318	2319	2320	2321	2322	2323	2324	2325	2326	2327	2328	2329	2330	2331	2332	2333	2334	2335	2336	2337	2338	2339	2340	2341	2342	2343	2344	2345	2346	2347	2348	2349	2350	2351	2352	2353	2354	2355	2356	2357	2358	2359	2360	2361	2362	2363	2364	2365	2366	2367	2368	2369	2370	2371	2372	2373	2374	2375	2376	2377	2378	2379	2380	2381	2382	2383	2384	2385	2386	2387	2388	2389	2390	2391	2392	2393	2394	2395	2396	2397	2398	2399	2400	2401	2402	2403	2404	2405	2406	2407	2408	2409	2410	2411	2412	2413	2414	2415	2416	2417	2418	2419	2420	2421	2422	2423	2424	2425	2426	2427	2428	2429	2430	2431	2
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OK, SEE #MEC108

PAGE 0004

STAGE	1346.00	1346.74	1347.47	1348.21	1348.95	1349.68	1350.42	1351.16	1351.89	1352.63
	1353.37	1354.10	1354.84	1355.58	1356.32	1357.05	1357.79	1358.53	1359.26	1360.00
FLOW	0.00	61.02	202.91	411.60	688.91	1036.16	1456.09	1951.85	2526.78	3375.65
	4031.06	7216.05	10819.22	16083.62	22936.79	31422.70	41652.64	53738.30	67798.06	83916.67

MAXIMUM STAGE IS 1350.4
 MAXIMUM STAGE IS 1353.0
 MAXIMUM STAGE IS 1353.5
 MAXIMUM STAGE IS 1353.8
 MAXIMUM STAGE IS 1354.3
 MAXIMUM STAGE IS 1354.8

SUB-AREA RUNOFF COMPUTATION

COMPUTE RUNOFF FROM ADJACENT WATERSHED
 ISTAQ ICOMP IRECON ITAPE JPLY JPRT INAPE ISTAGE IAUOTO
 INFLOW 0 0 0 0 0 0 0 0 0 0

HYDROGRAPH DATA

INHYD	IUNG	TAREA	SNAP	TRSDA	TRSPC	RATIO	ISNOW	ISAME	LOCAL
1	1	6.17	0.00	12.17	0.00	0.000	0	0	0

PRECIP DATA

SPEE	PMS	R6	R12	R24	R48	R72	R96
0.00	22.60	114.00	124.00	138.00	148.00	0.00	0.00

TRSPC COMPUTED BY THE PROGRAM IS 0.807

LOSS DATA

LAOPT	STAKR	DLTKR	RTIOL	ERAIN	STKRS	RTIOK	STRTL	CNSTL	ALSMX	RTIMP
0	0.00	0.00	1.00	0.00	0.00	1.00	1.00	0.10	0.00	0.00

UNIT HYDROGRAPH DATA

TPE= 3.96 CP=0.63 NTA= 0

RECESSION DATA

STRIO= 2.00 GRCSNE= -0.10 RTIOR= 2.00

UNIT HYDROGRAPH 86 END-OF-PERIOD ORDINATES, LAG= 3.95 HOURS, CP= 0.63 VOL= 1.00

10.	39.	79.	127.	181.	238.	297.	359.	423.	483.
535.	578.	611.	636.	651.	655.	648.	623.	585.	546.
509.	475.	443.	414.	386.	360.	336.	314.	293.	275.
255.	238.	222.	207.	193.	180.	168.	157.	146.	137.
128.	119.	111.	104.	97.	90.	84.	79.	73.	68.
64.	60.	56.	52.	48.	45.	42.	39.	37.	34.
32.	30.	28.	26.	24.	23.	21.	20.	18.	17.
16.	15.	14.	13.	12.	11.	11.	10.	9.	9.
8.	7.	7.	7.	6.	6.	6.	6.	6.	6.

OK. SEE SHEET 08

PAGE 0005

0
MO.DA HR.MN PERIOD RAIN EXCS LOSS COMP 0 MO.DA HR.MN PERIOD RAIN EXCS LOSS COMP 0
SUM 26.99 23.23 3.76 202347.
(6P5.3(596.3(95.3(2561.51)

COMBINE HYDROGRAPHS

COMBINE HYDROGRAPHS
ISTAO ICOMP 2 IECON ITAPE JPLT JPRI INAPE ISTAGE IAUTO
OMBINE 0 0 0 0 0 0 0 0 0

HYDROGRAPH ROUTING

CHANNEL ROUTING -MOD PULS REACH 1-2
ISTAO ICOMP 1 IECON ITAPE JPLT JPRI INAPE ISTAGE IAUTO
2 0 0 0 0 0 0 0 0
ROUTING DATA
QLOSS CLOSS AVG IRES ISAME IOPT IPMP LSTR
0.0 0.000 0.00 1 1 0 0 0 0
NSTPS NSTOL LAG ANSKK X TSK STORA ISPRAT
1 0 0 0.000 0.000 0.000 0.000 0.000 0.000 0.000 0.000

NORMAL DEPTH CHANNEL ROUTING

QN(1) QN(2) QN(3) ELNVT ELMAX RLNTH SEL
0.0450 0.0400 0.0450 1308.0 1330.0 7600. 0.00050

CROSS SECTION COORDINATES--STA.FLEV,STA.FLEV--ETC
0.00 1338.00 700.00 1320.00 1300.00 1314.00 1340.00 1308.00 1370.00 1302.00
1400.00 1314.00 2200.00 1320.00 2201.00 1320.00

STORAGE	0.00	7.42	17.58	30.46	46.06	64.40	102.78	194.86	341.51	547.71
	798.49	1101.25	1423.02	1761.14	2115.64	2486.51	2872.75	3277.35	3697.33	4137.67
OUTFLOW	0.00	34.81	122.06	264.55	468.78	741.57	1195.01	2036.15	3474.30	5687.63
	8433.60	13411.18	19284.59	26214.89	34194.46	43224.27	53316.59	64463.27	76694.53	90016.39
STAGE	1308.00	1309.16	1310.32	1311.47	1312.63	1313.79	1314.95	1316.10	1317.26	1318.42
	1319.58	1320.73	1321.89	1323.05	1324.21	1325.37	1326.52	1327.68	1328.84	1330.00
FLOW	0.00	34.81	122.06	264.55	468.78	741.57	1195.01	2036.15	3474.30	5687.63
	8433.60	13411.18	19284.59	26214.89	34194.46	43224.27	53316.59	64463.27	76694.53	90016.39

MAXIMUM STAGE IS 1316.7
 MAXIMUM STAGE IS 1319.1
 MAXIMUM STAGE IS 1319.8
 MAXIMUM STAGE IS 1320.3
 MAXIMUM STAGE IS 1321.3
 MAXIMUM STAGE IS 1322.1

HYDROGRAPH ROUTING

CHANNEL ROUTING -MOD PULS REACH 2-3

ISTAQ	ICOMP	IECON	ITAPE	JPLT	JPRT	INAVE	ISTAGE	IAUTO
3	1	0	0	0	0	1	0	0
ROUTING DATA								
GROSS	CLOSS	AVG	IRES	ISAME	IOPT	IPMP	LSTR	
0.0	0.000	0.00	1	1	0	0		
NSTPS NSTOL LAG ANSKK X TSK STORA ISPRAT								
1	0	0	0.000	0.000	0.000	0.0		0

NORMAL DEPTH CHANNEL ROUTING

ON(1)	ON(2)	ON(3)	ELNVT	ELMAX	RLNTH	SEL
0.0450	0.0400	0.0450	1304.0	1322.0	1000.	0.00220

CROSS SECTION COORDINATES--STA,ELEV,STA,ELEV--ETC

STA	ELEV	STA	ELEV
0.00	1320.00	700.00	1322.00
0.00	1320.00	800.00	1320.00
1370.00	1304.00	1314.00	2200.00

STORAGE	0.00	1.60	3.28	5.03	6.86	8.76	10.73	12.70	14.90	17.09
	19.37	22.34	30.84	45.86	67.40	95.46	130.03	171.21	227.11	301.13
OUTFLOW	0.00	64.04	204.00	402.51	652.86	951.26	1295.30	1683.33	2114.23	2587.25
	3101.86	2742.33	2750.56	3683.55	5422.09	8049.00	11681.41	16538.40	23626.22	32014.54
STAGE	1304.00	1304.95	1305.89	1306.84	1307.79	1308.74	1309.68	1310.63	1311.58	1312.53
	1313.47	1314.42	1315.37	1316.31	1317.26	1318.21	1319.16	1320.10	1321.05	1322.00
FLOW	0.00	64.04	204.00	402.51	652.86	951.26	1295.30	1683.33	2114.23	2587.25
	3101.86	2742.33	2750.56	3683.55	5422.09	8049.00	11681.41	16538.40	23626.22	32014.54

MAXIMUM STAGE IS 1312.9

MAXIMUM STAGE IS 1318.0

[illegible]

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MAXIMUM STAGE IS 1316.6

PEAK FLOW AND STORAGE (END OF PERIOD) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
AREA IN SQUARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	AREA (PLAN	RATIO 1	RATIOS APPLIED TO FLOWS				
					RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6
HYDROGRAPH AT INFLOW	1	6.00 (15.54)	1	2090.	4179.	5224.	6269.	8359.	10442.
				(59.17)	(118.35)	(147.93)	(177.52)	(236.69)	(295.87)
ROUTED TO	1	6.00 (15.54)	1	1442.	4010.	5116.	6167.	8259.	10423.
				(40.82)	(113.55)	(146.86)	(174.62)	(233.86)	(295.13)
ROUTED TO	1	6.00 (15.54)	1	1447.	4013.	5116.	6167.	8261.	10430.
				(40.97)	(113.63)	(146.86)	(174.63)	(233.93)	(295.34)
HYDROGRAPH AT INFLOW	1	6.17 (15.98)	1	2187.	4373.	5467.	6560.	8747.	10932.
				(61.92)	(123.84)	(154.80)	(185.76)	(247.68)	(309.55)
2 COMBINED	1	12.17 (31.52)	1	3025.	8231.	10490.	12645.	16922.	21337.
				(85.66)	(233.08)	(297.05)	(358.07)	(479.18)	(604.12)
ROUTED TO	2	12.17 (31.52)	1	2788.	7451.	9678.	11866.	16222.	20599.
				(78.96)	(210.99)	(274.06)	(336.02)	(459.36)	(583.30)
ROUTED TO	3	12.17 (31.52)	1	2787.	7449.	9676.	11854.	16219.	20605.
				(78.92)	(210.94)	(274.01)	(335.68)	(459.26)	(583.46)
ROUTED TO	4	12.17 (31.52)	1	2785.	7435.	9654.	11856.	16215.	20577.
				(78.87)	(210.54)	(273.38)	(335.72)	(459.15)	(582.67)

SUMMARY OF DAM SAFETY ANALYSIS

[illegible]

0.40	1389.71	0.00	817.	4010.	0.00	44.25	0.00
0.50	1390.32	0.00	860.	5116.	0.00	44.00	0.00
0.60	1398.85	0.00	898.	6167.	0.00	44.00	0.00
0.80	1391.82	0.02	966.	8259.	0.50	43.75	0.00
1.00	1392.24	0.44	995.	10423.	3.50	43.75	0.00

PLAN 1		STATION 1	
RATIO	MAXIMUM FLOW, CFS	MAXIMUM STAGE, FT	TIME HOURS
0.20	1447.	1350.4	46.00
0.40	4013.	1353.0	44.25
0.50	5116.	1353.5	44.00
0.60	6167.	1353.8	44.00
0.80	8261.	1354.3	44.00
1.00	10430.	1354.8	43.75

PLAN 1		STATION 2	
RATIO	MAXIMUM FLOW, CFS	MAXIMUM STAGE, FT	TIME HOURS
0.20	2788.	1316.7	46.25
0.40	7451.	1319.1	45.00
0.50	9678.	1319.8	44.75
0.60	11866.	1320.3	44.50
0.80	16222.	1321.3	44.25
1.00	20599.	1322.1	44.25

PLAN 1		STATION 3	
RATIO	MAXIMUM FLOW, CFS	MAXIMUM STAGE, FT	TIME HOURS
0.20	2787.	1312.9	46.25
0.40	7449.	1318.0	45.00
0.50	9676.	1318.6	44.75
0.60	11854.	1319.2	44.50
0.80	16219.	1320.0	44.50
1.00	20605.	1320.6	44.25

PLAN 1		STATION 4	
RATIO	MAXIMUM FLOW, CFS	MAXIMUM STAGE, FT	TIME HOURS
0.20	2785.	1310.6	46.50
0.40	7435.	1314.8	45.25
0.50	9654.	1315.2	45.00
0.60	11856.	1315.6	44.75
0.80	16215.	1316.1	44.50
1.00	20577.	1316.6	44.25

 FLOOD HYDROGRAPH PACKAGE (HEC-1)
 DAM SAFETY VERSION JULY 1978
 LAST MODIFICATION 26 FEB 79

WATERSHED UPSTREAM OF DAM

$$T_p = c_t (L L_{ca})^{0.3} \checkmark$$

$$T_r = \frac{T_p}{5.5} \checkmark$$

$$c_t = 2.00$$

$$c_p = 0.63$$

$$T_{PR} = T_p + 0.25 (T_R - T_r)$$

$$L = 25000' = \frac{25000}{5280} = 4.73 \text{ MI} \checkmark$$

$$L_{ca} = 11300' = \frac{11300}{5280} = 2.14 \text{ MI} \checkmark$$

$$T_p = 2 (4.73 \times 2.14)^{0.3} = 4.01 \text{ hr.} \checkmark$$

$$T_r = \frac{4.01}{5.5} = 0.73 \text{ hr} \checkmark \Rightarrow T_R = 1 \text{ hr} \checkmark$$

$$T_{PR} = 4.01 + 0.25 (1 - 0.73) = 4.08 \text{ hr.} \checkmark$$

D.P. DATE 3-27-81 ERDMAN, ANTHONY, ASSOCIATES SHEET 2 OF 16
 DKO B.R. DATE 4/27/81 SUBJECT DAM SITE HYDROLOGY SUB-SHEET NO. 2
 OWNER PROJECT NAME HE-1 DAM INSPECTION 80166-00.09

WATERSHED UPSTREAM OF DAM

DAM 096 JONEWALLS CREEK SITE 9A

REF. QUAD. PERRYSBURG, N.Y.
FORESTVILLE, N.Y.

DISTANCE L & LCA MEAS. WITH MAP MEAS. WHEEL (1" = 2000')

COMPUTATION FOR L DISTANCE

RUN	MEAS. DIST	AVG. DIST	COEF.	L DISTANCE
A	1 = 12.50			
	2 = 12.50			
	$25.00 \div 2 = 12.50$			$\times 2000' = \underline{25,000. FT.}^*$

RUN	MEAS. DIST	AVG. DIST	COEF.	LCA DISTANCE
B	1 = 3.6			
	2 = 3.7			
	$7.3 \div 2 = 3.65$			$\times 2000' = \underline{17,300 FT}$

COMPUTATION FOR LCA DISTANCE

RUN	MEAS. DIST	AVG. DIST	COEF.	LCA DISTANCE
A	1 = 5.6			
	2 = 5.7			
	$11.3 \div 2 = 5.65$			$\times 2000' = \underline{11,300. FT.}^*$

SUMMARY

* USE RUN A FOR L DISTANCE = 25,000. FT.

* USE RUN A FOR LCA DISTANCE = 11,300. FT.

ADJACENT WATERSHED

$$L = 27000 \text{ ft} \checkmark = \frac{27000}{5280} = 5.11 \text{ MI} \checkmark$$

$$L_a = 9500 \text{ ft} \checkmark = \frac{9500}{5280} = 1.80 \text{ MI} \checkmark$$

$$T_p = C_r (L \times L_a)^{0.3}$$

$$C_r = 2.00$$

$$T_p = 2 (5.11 \times 1.80)^{0.3}$$

$$C_p = 0.63$$

$$T_p = 3.89 \text{ hr.} \checkmark$$

$$T_r = \frac{T_p}{5.5}$$

$$T_r = \frac{3.89}{5.5} = 0.71 \implies T_R = 1 \text{ hr} \checkmark$$

$$T_{PR} = T_p + 0.25 (T_R - T_r)$$

$$T_{PR} = 3.89 + 0.25 (1 - 0.71) = 3.96 \text{ hr.} \checkmark$$

DATE 4/28/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 4 OF 16
 D 6.R. DATE 4/28/81 SUBJECT LAM 596 HYDROLOGY SUB-SHEET NO. 4
 OWNER PROJECT NAME HEC-1 DB DAM INSPECTION 80136-00.09

ADJACENT WATERSHED
 LAM 596 CONEWANGS CREEK SITE 9A

REF. QUAD HAMLET, NY
 CHERRY CR., NY
 FORESTVILLE, NY
 PEREYSBURG, NY.

Drainage Distance

DISTANCE L & LCA MEAS. WITH MAP MEAS. WHEEL (1"=2000')

COMPUTATIONS FOR L DISTANCE

Run	MEAS. DIST.	AVG. DIST.	COEF.	L DIST.
A 1	13.5			
2	13.5			
	27.0	$\div 2 = 13.5$	$\times 2000'$	$= 27,000 \text{ ft.}$

Run	MEAS. DIST.	AVG. DIST.	COEF.	L DIST.
B 1	12.6			
2	12.7			
	25.2	$\div 2 = 12.65$	$\times 2000$	$= 25,300 \text{ ft}$

* L = 27,000 ft. USED RUN A

COMPUTATION FOR LCA DISTANCE

Run	MEAS. DIST.	AVG. DIST.	COEF.	LCA DIST.
A 1	4.8			
2	4.7			
	9.5	$\div 2 = 4.75$	$\times 2000'$	$= 9,500 \text{ ft.}$

* Lca = 9,500 ft.

BY B.R. DATE 4/24/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 5 OF 16
 D DATE 1/1/71 SUBJECT Dam 596 HYDRAULICS SUB-SHEET NO. 1
 OWNER PROJECT NAME Dam Inspection 80166-00.09

Dam 596 HYDRAULICS

SERVICE SPILLWAY

18" ϕ RCP \checkmark w/ 4' x 12' Riser \checkmark

From design report:

$$Q_s = 481 \text{ cfs} \quad \text{Elev. } 1386.6 \checkmark$$

$$Q_s = 467 \text{ cfs} \quad \text{Elev. } 1384 \checkmark$$

①
$$Q_s = C_o A_o \sqrt{2gh_o} + 467 \text{ cfs}, \quad h_o \text{ is Elev. above Elev. } 1384$$

$$A_o = \left[\left(\frac{48}{12} \right)^2 / 4 \right] \pi = 12.57 \text{ ft}^2 \checkmark$$

Determine C_o from $\begin{cases} Q = 481 - 467 \text{ cfs} \\ Q = 14 \text{ cfs} \end{cases} \quad \begin{cases} h_o = 1386.6 - 1384 \\ h_o = 2.6 \end{cases}$

From eq. ①

$$C_o = \frac{14}{12.57 \sqrt{2 \times 32.2 \times 2.6}} = 0.09$$

NOTE: Equation ① is only for elevations above elevation 1384.

For elevations below 1384 flow ^{D-18} are given by design report

$$Q_s = 0.09 \times 12.57 \sqrt{2 \times 32.2 \times h} + 467 = 9.08 h_o^{0.5} + 467 \text{ cfs}$$

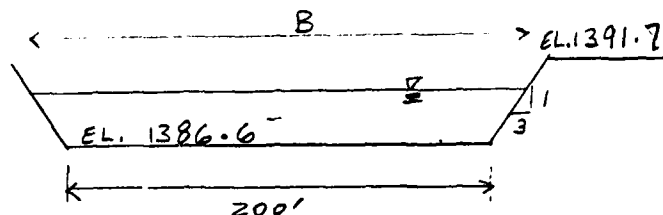
The above formula is used only for elevations above 1394.

SERVICE SPILLWAY		
ELEV.	h_o	Q_s
1381		118 ✓
1382		205 ✓
1383		356 ✓
1383.5		446 ✓
1384	0	467 ✓
1386.6	2.6	481 ✓
1387	3	483 ✓
1388	4	485 ✓
1389	5	487 ✓
1390	6	489 ✓
1391	7	491 ✓
* 1391.8	7.8	492 ✓
1392	8	493 ✓
1393	9	494 ✓
1394	10	

FROM
DESIGN
REPORT

* Top of dam

EMERGENCY SPILLWAY



EMERGENCY SPILLWAY SECTION

$$S_0 = 0.03$$

$$Q_c = \sqrt{\frac{g A^3}{B}}$$

$$\text{for } y = 1'$$

$$B = (2 \times 3) + 200 = 206'$$

$$A = \frac{1}{2}(206 + 200) \times 1 = 203 \text{ ft}^2$$

$$Q_c = \sqrt{\frac{32.2 \times 203^3}{206}} = 1143.5 \text{ cfs}$$

$$K = \frac{1.49}{n} A R^{2/3} = \frac{1.49}{0.035} 203 \left[\frac{203}{200 + 2(1+9)^{0.5}} \right]^{2/3}$$

$$K = 8549$$

$$S_c = \left(\frac{1143.5}{8549} \right)^2 = 0.018$$

spillway slope > critical slope ($0.03 > 0.018$)

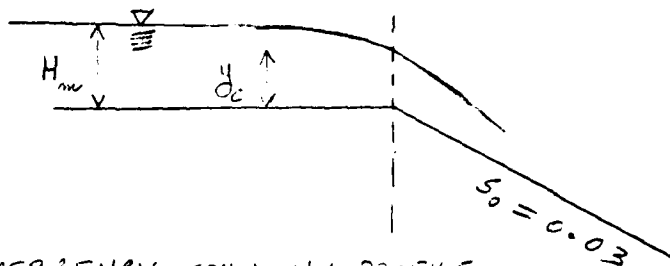
∴ Flow goes through critical depth for $y = 1'$ and also for $y > 1'$

use Table 4-7 from "King and Brister"

$$Z = 3/1 = 3$$

$$b = 200'$$

$$Q_E = C_2 b H_m^{1.5}$$



EMERGENCY SPILLWAY PROFILE

EMERGENCY SPILLWAY DISCHARGE - ELEVATION RELATIONSHIP				
H_m	$\frac{H_m Z}{b}$	C_2	Q_E	ELEV.
0	0	3.09	0	1386.6
0.4	0.01	3.11	157 ✓	1387
1.4	0.02	3.13	1037 ✓	1388
2.4	0.04	3.17	2357 ✓	1389
3.4	0.05	3.19	4000 ✓	1390
4.4	0.07	3.23	5962 ✓	1391
* 5.2	0.08	3.25	7708 ✓	1391.3
5.4	0.08	3.25	8157 ✓	1392
6.4	0.10	3.29	10654 ✓	1393
7.4	0.11	3.32	13366 ✓	1394

* actual top of dam.

LONGWANG CREEK DAM 596 CITE 9A

C.L. AREA RESEVIOIR SURFACE AREA

LEFF. U.S. DEPT. OF A.S.C.S. AS BUILT PLANS DWG. NY-2161-P
 SCALE 1" = 200' PLAN & 1/2" REDUCTION = 1" = 400

$$\text{Eq. } \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = \text{AC}$$

ELEV. 1370

$$4.6 \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = 16.90 \text{ AC. } \checkmark$$

ELEV. 1375

$$8.28 \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = 30.41 \text{ AC. } \checkmark$$

ELEV. 1380

$$12.10 \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = 44.44 \text{ AC. } \checkmark$$

ELEV. 1385

$$16.67 \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = 51.23 \text{ AC. } \checkmark$$

ELEV. 1390

$$19.66 \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = 72.21 \text{ AC. } \checkmark$$

ELEV. 1395

$$24.0 \frac{\text{in}^2 \times 400^2 \text{ ft}^2}{\text{in}^2} \times \frac{1 \text{ AC}}{43,560 \text{ ft}^2} = 88.15 \text{ AC. } \checkmark$$

TOTAL AC = 303.34

* Used storage values from ^{main} D-22 report

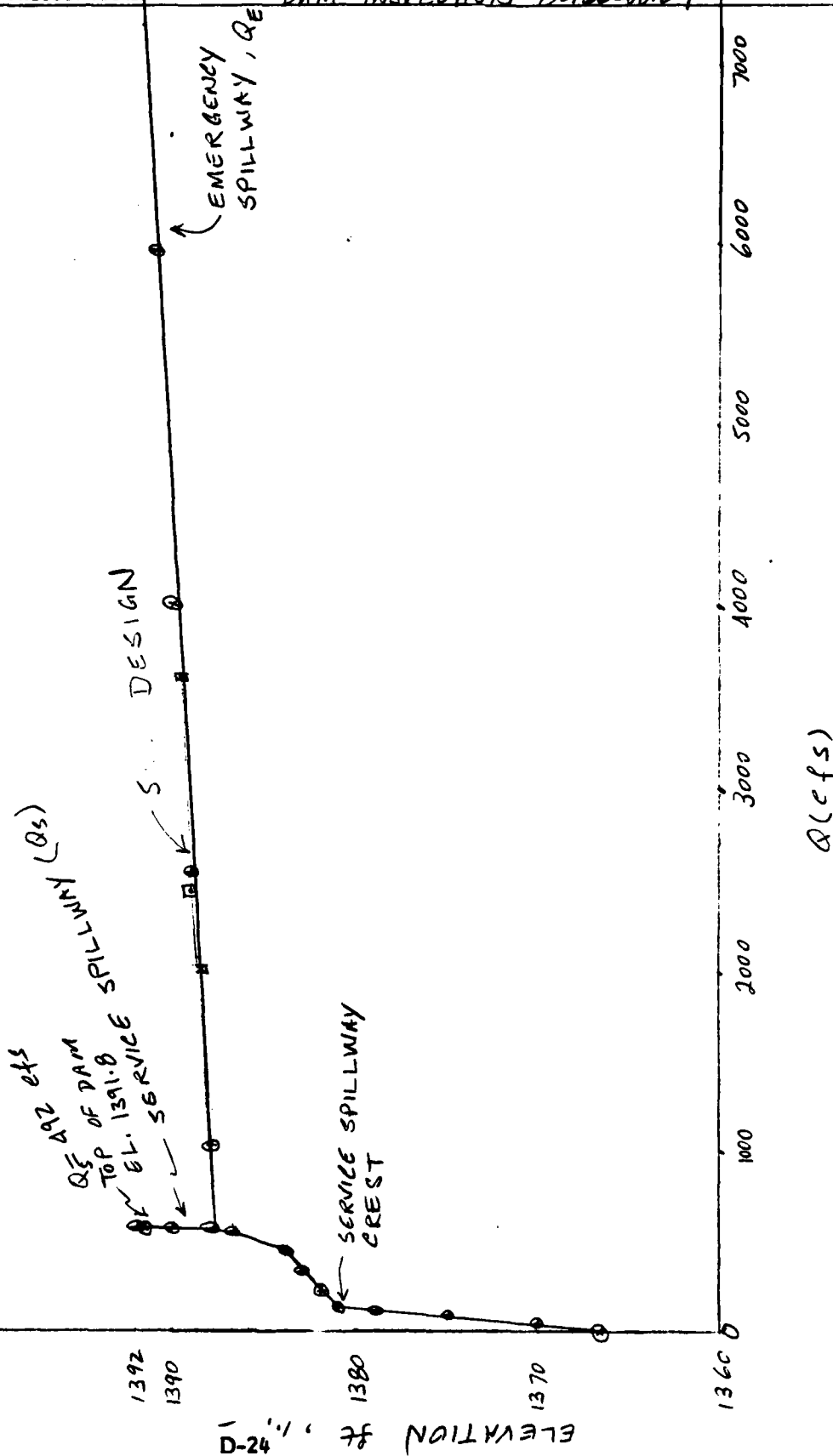
BY B.R. DATE 4/29/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 10 OF 16
 CD 1 DATE 1 SUBJECT DAM 596 HYDRAULICS SUB-SHEET NO. 6
 OWNER PROJECT NAME DAM INSPECTION 60166-0009

$Q_S + Q_E$ TOTAL SPILLWAYS DISCHARGE		
ELEV. ft	$Q_S + Q_E$ (cfs)	RESERVOIR SURFACE AREA
1366.6	0	8.8
1367	2.5	
1367.5	8.5	
1368	16.4	
1368.77	32	
1370	49	16.90 AC.
1375	87	30.41 AC.
1379	113	
1380	118	44 AC
1381	116	
1382	205	
1383	356	
1383.5	446	
1384	467	51.23 AC
1385	473	59.5 AC.
1386.6	481	
1387	640	
1388	1522	65.5
1389	2844	
1390	4489	72.21 AC
1391	6453	
1391.8	8200	74.5 AC
1392	8650	
1393	11148	
1394		
1395		88.15 AC

* TOP OF DAM

BY B.R. DATE 4/27/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 11 OF 16
 DATE 7/11 SUBJECT DAM 596 HYDRAULICS SUB-SHEET NO. 7
 OWNER PROJECT NAME DAM INSPECTION B0166-00.09

SPILLWAY RATING CURVE - DAM 596



B.R. DATE 4/27/81 ERDMAN, ANTHONY, ASSOCIATES SHEET 12 OF 16
 KD RRA DATE 5/29/81 SUBJECT DAM 596 - HYDRAULICS SUB-SHEET NO. 8
 OWNER PROJECT NAME DAM INSPECTION 80166-00.09

VALUES ON \$D CARD OF HEC-1

FIELD	VARIABLE	VALUE
0	ID	\$D
1	TOPEL	1391.8 ✓
2	CQCD	2.7 ✓
3	EXPD	1.5 ✓
4	DAMWID	1590 ✓

AREA OF THE ADJACENT WATERSHED

$$A = 43.0 \text{ in}^2 \text{ (scale : } 1'' = 2000') \text{)}$$

$$A = 43 \text{ in}^2 \times \frac{2000^2 \cancel{\text{ft}^2}}{\text{in}^2} \times \frac{\text{ac}}{43560 \cancel{\text{ft}^2}} \times \frac{\text{MILE}^2}{640 \text{ ac.}} = 6.17 \text{ Mile}^2 \checkmark$$

Emergency Spillway Capacities

<u>Flood</u>	<u>Q_T</u>	<u>Elev.</u>	<u>Q_{es}</u>	<u>A</u>	<u>V</u>	<u>Comments</u>
H.F.	16,423	1392.21'	8756	1075	8.15	> 8.0 : erosion
M.F.	5116	1390.32	4328	575	8.08	> 8.0 : erosion

PMF

$$y = 8157 + \frac{(20)(13354 - 8157)}{13354 - 8157} = 8756 \text{ as } \checkmark$$

$$\text{Assume } \frac{y}{b} < 0.02 \Rightarrow \frac{y}{b} = 0.749 \left(\frac{Q n}{b S_b^{1/2}} \right)^{0.6}$$

$$y/b = 0.749 \left(\frac{8756 (0.06)}{200 (0.03)^{1/2}} \right)^{0.6} = 4.03', \frac{y}{b} = \frac{4.03}{200} = 0.02 \neq 0.02 \text{ N.G.}$$

Since $\frac{y}{b}$ is not less than 0.02, then $\frac{y}{b}$ is found from Table 10.1 of Fundamentals of Open Channel Hydraulics byacey.

$$\frac{Q n}{(b)^{3/2} (S_b)^{1/2}} = \frac{8756 (0.06)}{(200)^{3/2} (0.03)^{1/2}} = 0.00222 \checkmark$$

0.00150	0.02	$\frac{y}{b} = 0.02 + \frac{0.1(0.00222)}{0.00147} = 0.025 \checkmark$
0.00222	$\frac{y}{b}$	
0.00298	0.03	

$$y_n = 0.025(200) = 50' \checkmark$$

$$A = (50)(200) + \frac{1}{2} \left(\frac{1}{2} (50)(3)(200) \right) = 1075 \text{ ft}^2 \checkmark$$

$$V = \frac{Q}{A} = \frac{8756 \text{ ft}^3/\text{s}}{1075 \text{ ft}^2} = 8.15 \text{ ft/s} \checkmark$$

DATE 6/1/71 ERDMAN, ANTHONY, ASSOCIATES SHEET 14 OF 16
 NO BR DATE 6/1/71 SUBJECT DAM 596 - Hydraulics SUB-SHEET NO. 10
 OWNER PROJECT NAME DAM 596 (80166-33, 39)

1/2 DMF

1982 4000
 1981 32 Y
 1981 1982

$$y = 4000 + 0.32(5962 - 4000) = 4628 \checkmark$$

$$\text{Assume } y/b < 0.02 \Rightarrow y_n = 0.754 \left(\frac{Q n}{b \sqrt{g}} \right)^{0.6}$$

$$y_n = 0.754 \left(\frac{4628 (0.02)}{200 (0.02)^{1/2}} \right)^{0.6} = 2.75', \quad y/b = \frac{2.75'}{200} = 0.014 < 0.02 \quad \text{OK}$$

$$A = 2.75(200') + \frac{1}{2} \left(\frac{1}{3} (2.75')(3(2.75')) \right) = 573 \text{ ft}^2 \checkmark$$

$$V = \frac{Q}{A} = \frac{4628}{573} = 8.08 \text{ ft/sec} \checkmark$$

BY S.R. DATE 6/1/81 **ERDMAN, ANTHONY, ASSOCIATES** SHEET 15 OF 16
 CD PKP DATE 6/1/81 SUBJECT DHM 596 - Channel Raising SUB-SHEET NO. 1
 OWNER _____ PROJECT NAME DHM INSPECTION 80166-CC-09

CONEWANGO CREEK SITE 9A

REF. US. DEP. OF ARCS DESIGN REPORT SHEETS 4 RATING CURVE
SHEET A AREA SHEET

DHM TOP ELEV. 1391.8
DAM INV. ELEV. 1353.78

REACH 1 LENGTH = 670'

CROSS SECTION: $\frac{1360}{0}$, $\frac{1355}{700}$, $\frac{1352}{1370}$, $\frac{1346}{1395}$, $\frac{1346}{1420}$, $\frac{1352}{1430}$, $\frac{1360}{1700}$, $\frac{1360}{1701}$

SLOPE = (DAM INV. - RE. 1 INV.) \div REACH LENGTH

$$1353.8 - 1346 = 7.8 \div 670 = 0.0116$$

REACH 2 LENGTH = 7600'

CROSS SECTION: $\frac{1330}{0}$, $\frac{1320}{700}$, $\frac{1314}{1300}$, $\frac{1308}{1340}$, $\frac{1308}{1370}$, $\frac{1314}{1400}$, $\frac{1320}{2200}$, $\frac{1320}{2201}$

SLOPE = (1346 - 1308) \div 8200 = 0.0046
7600 = 0.005

REACH 3 LENGTH = 1800' ✓

CROSS SECTION ✓: $\frac{1320}{0}$, $\frac{1322}{700}$, $\frac{1320}{880}$, $\frac{1314}{1320}$, $\frac{1304}{1330}$, $\frac{1304}{1370}$, $\frac{1314}{1380}$, $\frac{1322}{2200}$

SLOPE = (1308 - 1304) \div 1800 = 0.0022

REACH 4 LENGTH = 1500'

CROSS SECTION: $\frac{1315}{0}$, $\frac{1312}{1200}$, $\frac{1302}{1255}$, $\frac{1302}{1295}$, $\frac{1312}{1320}$, $\frac{1315}{1400}$, $\frac{1318}{2900}$, $\frac{1318}{3000}$

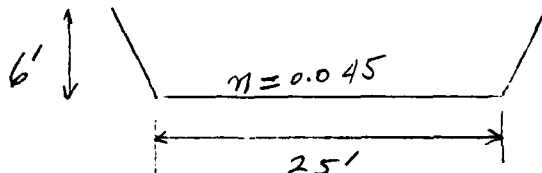
SLOPE = (1304 - 1302) \div 1500 = 0.0013

S.R. DATE 5-22-81 ERDMAN, ANTHONY, ASSOCIATES SHEET 16 OF 16
 RD 112H DATE 5/29/81 SUBJECT Dam 596 - Channel Section SUB-SHEET NO. 2
 OWNER PROJECT NAME Dam Inspection - B0166-00.09

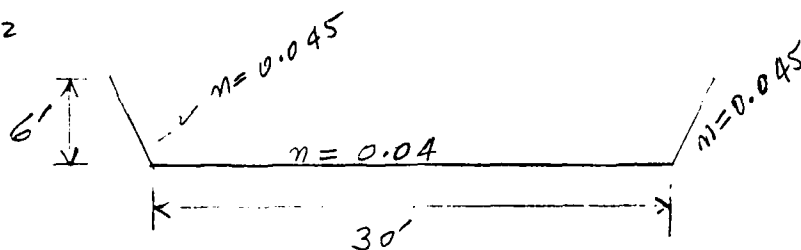
DOWNSTREAM CHANNEL SECTIONS

SECTION 1

2

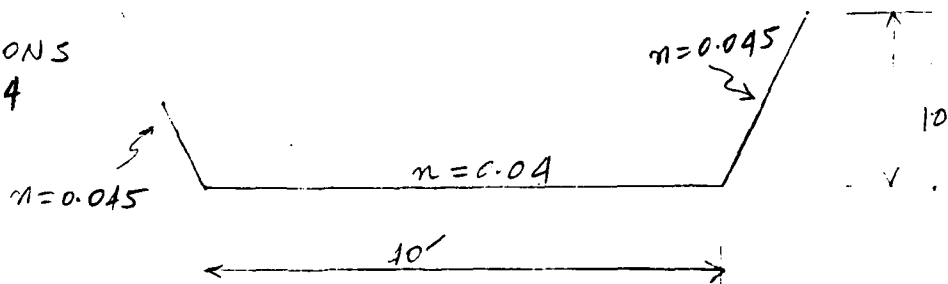


SECTION 2



SECTIONS

3 & 4



CHECK LIST FOR DAMS
HYDROLOGIC AND HYDRAULIC
ENGINEERING DATA

(DAM NY 596)

1

AREA-CAPACITY DATA:

	<u>Elevation</u> (ft.)	<u>Surface Area</u> (acres)	<u>Storage Capacity</u> (acre-ft.)
1) Top of Dam	<u>1391.8</u>	<u>74.6</u>	<u>964</u>
2) Design High Water (Max. Design Pool)	<u>1386.6</u>	<u>59.5</u>	<u>612</u>
3) Auxiliary Spillway Crest	<u>1386.6</u>	<u>59.5</u>	<u>612</u>
4) Pool Level with Flashboards	<u>N/A</u>	<u>-</u>	<u>-</u>
5) Service Spillway Crest	<u>1381.0</u>	<u>8.8</u>	<u>41</u>

DISCHARGES

	<u>Volume</u> (cfs)
1) Average Daily	<u>unknown</u>
2) Spillway @ Maximum High Water	<u>492</u>
3) Spillway @ Design High Water	<u>481</u>
4) Spillway @ Auxiliary Spillway Crest Elevation	<u>481</u>
5) Low Level Outlet (gated reservoir drain)	<u>0</u>
6) Total (of all facilities) @ Maximum High Water	<u>8200</u>
7) Maximum Known Flood	<u>unknown</u>
8) At Time of Inspection	<u>31</u>

CREST:

ELEVATION: 1391.8Type: broad-crested ; grassed earth embankmentWidth: 16 ft. Length 1590 ft.

Spillover _____

Location South end of dam

SPILLWAY:

SERVICE

AUXILIARY

1381.0Elevation 1386.6conc. pipe w/ riserType excavated channel48" dia.Width 200' Bottom width w/ 1V:3H sideslopesType of Control

✓

Uncontrolled

✓

Controlled:

Type

(Flashboards; gate)

Number

Size/Length

Invert Material

Anticipated Length
of operating service

Chute Length

Height Between Spillway Crest
& Approach Channel Invert
(Weir Flow)

HYDROMETEROLOGICAL GAGES:

Type : None

Location: -

Records:

Date - -

Max. Reading - -

FLOOD WATER CONTROL SYSTEM:

Warning System: None

Method of Controlled Releases (mechanisms):

None

DRAINAGE AREA: 6.0 sq. mi.

DRAINAGE BASIN RUNOFF CHARACTERISTICS:

Land Use - Type: Woodland, pastures, farmlands, very minor development

Terrain - Relief: Rolling

Surface - Soil: Glacial till over shallow bedrock

Runoff Potential (existing or planned extensive alterations to existing
(surface or subsurface conditions))

None

Potential Sedimentation problem areas (natural or man-made; present or future)

None at present. The dam was designed for
a 50 yr. sediment accumulation.

Potential Backwater problem areas for levels at maximum storage capacity
including surcharge storage:

flooding of agricultural lands.

Dikes - Floodwalls (overflow & non-overflow) - Low reaches along the
Reservoir perimeter:

Location: None

Elevation: -

Reservoir:

Length @ Maximum Pool ±0.6 (Miles)

Length of Shoreline (@ Spillway Crest) ±0.4 (Miles)

APPENDIX E

REFERENCES

APPENDIX E

REFERENCES

- 1) U.S. Department of Commerce, Technical Paper No. 40, Rainfall Frequency Atlas of the United States, May, 1961.
- 2) F.M. Henderson, Open Channel Flow, Macmillian Publishing Co., Inc., 1966.
- 3) H.W. King and E.F. Brater, Handbook of Hydraulics, 5th Edition, McGraw-Hill, 1963.
- 4) T. W. Lambe and R.V. Whitman, Soil Mechanics, John Wiley and Sons, 1969.
- 5) W.D. Thornbury, Principles of Geomorphology, John Wiley and Sons, 1969.
- 6) University of the State of New York, Geology of New York, Education Leaflet 20, Reprinted 1973.
- 7) Cornell University Agriculture Experiment Station (compiled by M.G. Cline and R.L. Marshall), General Soil Map of New York State and Soils of New York Landscapes, Information Bulletin 119, 1977.
- 8) U.S. Department of Commerce, Hydrometeorological Report No. 33, Seasonal Variation of the Probable Maximum Precipitation East of the 105th Meridian for Areas From 10 to 1000 Square Miles and Durations of 6, 12, 24, and 48 hours, April 1956.
- 9) U.S. Department of the Army, Engineering Manual 1110-2-1411, Standard Project Flood Determinations, March 1952.
- 10) U.S. Army Corps of Engineers, The Hydrologic Engineering Center, Flood Hydrograph Package (HEC-1) Users Manual for Dam Safety Investigations, September, 1978.

APPENDIX F

PREVIOUS INSPECTION REPORTS/
AVAILABLE DOCUMENTS

DAM INSPECTION REPORT
(By Visual Inspection)

Dam Number	River Basin	Town	County	Hazard Class	Date & Inspector
7B-3979	Allegheny	Villanova	Chataqua	B+	10/18/77 K.W.H.

Stream =

Owner =

County

Type of Construction

- ☐ Earth w/Concrete Spillway
☒ Earth w/Drop Inlet Pipe *conc.*
☐ Earth w/Stone or Riprap Spillway
☐ Concrete
☐ Stone
☐ Timber
☐ Other _____

Use

- ☐ Water Supply
☐ Power
☐ Recreation - ☐ High Density
☐ Fish and Wildlife
☐ Farm Pond
☐ No Apparent Use-Abandoned
☒ Flood Control
☐ Other _____

~~Estimated~~ Impoundment Size 65 Acres ~~###~~ *Estimated* Height of Dam above Streambed 42 Ft.

Condition of Spillway

- ☒ Service satisfactory ☒ Auxiliary satisfactory
☐ In need of repair or maintenance ☐ In need of repair or maintenance

Explain: _____

Condition of Non-Overflow Section

- ☒ Satisfactory ☐ In need of repair or maintenance

Explain: _____

Condition of Mechanical Equipment

- ☒ Satisfactory ☐ In need of repair or maintenance

Explain: _____

Siltation

- ☐ High ☒ Low

Explain: _____

Remarks: _____

Evaluation (From Visual Inspection)

- ☐ Repairs req'd. beyond normal maint. ☒ No defects observed beyond normal maint.

DATE February 14, 1972

MEMORANDUM
DEPARTMENT OF TRANSPORTATION

SUBJECT CONEWANGO CREEK WATERSHED PROJECT
FLOODWATER RETARDING DAM, SITE 9A
CHAUTAUQUA COUNTY

FROM Wm. P. Hofmann, Soil Mechanics Bureau, Rm. 102, Bldg. 7 *BEB*
By: Bernard E. Butler

TO A. W. Moon, Bridge Planning and Railroads Bur., 6th Flr., Bldg. 5 ✓

This Bureau has completed a review of the soils and foundation aspects of the subject dam. Our review was based on plans and specifications prepared by the U.S.D.A. Soil Conservation Service and received in this office on January 19, 1972.

Our review indicates the design, in general, properly accounts for the anticipated soils and foundation conditions. However, we offer the following comment:

1. On sheet No. 7, Drawing No. NY-2161-P under Earth Fill Requirements Note No. 2, "hand tamping or" should be deleted.

BEB:PJW:MVM

DESIGN REPORT

CONEWAGO CREEK WATERSHED
SITE 9A
FLOODWATER RETARDING DAM
CHAUTAUQUA COUNTY, NEW YORK

U.S. DEPARTMENT OF AGRICULTURE
SOIL CONSERVATION SERVICE

DESIGN SECTION, SYRACUSE, N.Y.

Sheet 1 of 6

MAY 1951

U. S. DEPARTMENT OF AGRICULTURE — SOIL CONSERVATION SERVICE

This single purpose flood control structure is located on an unnamed tributary to the West branch of Conewango Creek approximately 4 miles NNE of South Dayton in the Town of Villenova. Sheet 5 of this report, together with the Perrysburg 7.5' quadrangle published by the U.S. Geological Survey, may be used to locate this site.

A summary of pertinent design information is given on Sheet 3 of this report.

Criteria and procedures used in this design are given in Soil Conservation Service publications.

This structure is one of 20 proposed floodwater retarding dams in the Conewango Creek Watershed designed to reduce floodwater damage.

Site 9A is designed to retard a 50-yr. frequency storm without discharge occurring in the emergency spillway.

The results of hydrologic and hydraulic computations are given on Sheet 4 of this report.

The structure consists of a zoned, compacted earth fill primarily of gravelly glacial till (GM), and alluvial gravel (GM-GP).

In the floodplain of the foundation, sandy gravel (GM-GP) alluvium overlies lacustrine CL silt and sandy silt deposits. Alluvial gravels and sands underlie the lacustrine materials and glacial till underlies the alluvial materials.

A dense cemented alluvial GM gravel underlies the glacial till of the left abutment and the alluvium and colluvium in the right abutment.

A drainage system is located under the downstream portion of the earth fill to control the phreatic surface and to provide a safe outlet for foundation seepage. A cutoff trench is located on the dam centerline to reduce seepage.

The principal spillway is a drop inlet structure composed of a 2-stage reinforced concrete riser, 48" diameter concrete water pipe, impact basin, and excavated outlet channel.

A vegetated earth emergency spillway with a bottom width of 200' is provided in the left abutment.

U.S. DEPARTMENT OF AGRICULTURE - SOIL CONSERVATION SERVICE

Element of Structure	Determining Factor	Elev.	Surface Area Acres	Storage		Inflow		Peak Outflow C.F.S.
				AC.FT.	Inches #	Volume In. #	Rate C.F.S.	
Invert of Orifice	50 Yr. Submerged Sediment	1366.6	8.8	40.6	0.13	-	-	-
Crest of Riser	1.00" Storage plus 100 Yr. Total Sediment	1381.0	44.0	415.6 ^{1/}	1.30	-	-	114
Crest of Emergency Spillway	50 Yr. Frequency Storm, AMC II	1386.6	59.5	611.2 ^{2/}	1.91	-	-	312
Design High Water	ES-1020 Sh. 2 of 5. AMC II **	1398.7	65.5	746.2 ^{2/}	2.33	3.56	3178	1709
Top of Dam	ES-1020 Sh. 3 of 5. AMC II **	1391.8	74.5	964.2 ^{2/}	3.01	8.80	7938	6941

1/ Includes 14.7 Ac. Ft. of Aer. Sediment Storage.

2/ Excludes 95.8 Ac. Ft. total sediment storage.

* Volume expressed in inches of runoff from controlled watershed of 3840 acres.

** Refer to hydrologic criteria in National Engineering Memo SCS-27 (Rev.).

DESIGN SECTION, SYRACUSE, N.Y.

42° 25' 00"

79° 07' 30"

79° 05' 00"

CONEWANGO CR. SITE 9A
N 42° 23' 05"
E 79° 06' 58"

65



108

42° 22' 30"

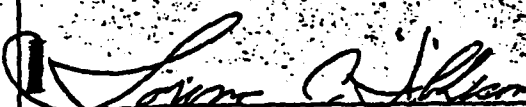
REF. USGS QUAD. 7 1/2' PERRYSBURG NY

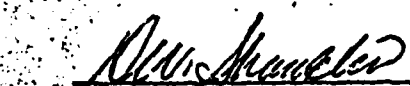
DESIGN SECTION, SYRACUSE, N.Y.

Sheet 5 of 6

U. S. DEPARTMENT OF AGRICULTURE — SOIL CONSERVATION SERVICE

Information pertaining to the criteria and procedures referred to in this report may be obtained from Mr. Albert C. Addison, State Conservationist, U. S. Department of Agriculture, Soil Conservation Service, Syracuse, New York.


Design Engineer


for State Conservation Engineer

DESIGN SECTION, SYRACUSE, N. Y.

Sheet 1 of 1

March 1, 1972

Mr. Eldred Rich, Chief
Bureau of Water Management
Department of Environmental Conservation
Division of Resource Management Services
50 Wolf Road
Albany, New York 12205

Dear Sir:

Dam at Site 9A
Conewango Creek Watershed Project

The plans, specifications and other data submitted by the Bureau of Water Management, to the Structures Subdivision of the Department of Transportation for the construction by the owner, Conewango Creek Watershed Commission, Court House, Mayville, New York, of a flood water retarding dam located in the Town of Villenova, County of Chautauqua and situated on an unknown tributary of Conewango Creek, have been reviewed.

The design and details pertaining to the soils, foundation and structural features of the dam are satisfactory to us insofar as the safety and stability of the structure are concerned.

The structure has been listed upon our records under the designation of Dam No. 7B-3979 of the Allegheny River Watershed.

Two sets of formally approved plans and specifications are enclosed. Also enclosed are two copies of the Bureau of Soil Mechanics' memorandum to this office stating the Bureau's comments concerning the anticipated soils and foundation conditions at the dam site with a recommendation to be followed during the construction of the structure. The recommendation is shown marked in red on the plans.

Very truly yours,

Original signed by
A. W. MOON
A. W. MOON
Assistant Deputy Chief Engineer
AMM:RCS:ME
Attachments
cc: Mr. F. Hofmann

New York State Department of Environmental Conservation

MEMORANDUM

7B 3979
NY 576

TO: Eldred Rich
FROM: Charles W. Kolak
SUBJECT: Conewango Creek Site 9-A Watershed Project, March 17, 1972
DATE: May 10, 1972

~~In response to the request by the Stream Protection Section of the Bureau of Water Regulation, We~~ have made a hydrologic and hydraulic investigation of the proposed watershed project at Conewango Creek - Site 9A, Hamlet, New York.

The following information was used to evaluate the proposed dam:

1. Application for permit submitted by SCS, Syracuse, New York
2. Contract drawings and specifications submitted by SCS

The design of the auxiliary spillway and the service spillway were reviewed and the following results were obtained:

AUXILIARY SPILLWAY

Hydrology:

Downstream hazard classification is Class "B".

Drainage Area -- 6.00 square miles

Design Flood -- Emergency Spillway Hydrograph for Class "B" Structures
(ES 1020 sheet 2 of 5)

Reference -- "Guidelines for Small Earth Dam Designs" - New York State
Rainfall = 6.2"

CN=77

Runoff 3.7"

Reference -- SCS National Engineering Handbook, Section 4 - Hydrology
Chapter 21

Flood Routing:

The design hydrograph indicates a maximum inflow of 2890 cfs. At 3.00 hours, water will begin spilling over the crest of the auxiliary spillway. The peak discharge occurs at t=5.04 hours with 2335 cfs discharging over the auxiliary spillway and 340 cfs discharging through the service spillway. The reservoir water surface reached an elevation of 1388.95 which will provide more than the required 2 feet of freeboard.

Memo to: Eldred Rich

- 2 -

May 10, 1972

SERVICE SPILLWAY

Hydrology:

Downstream hazard classification is Class "B".

Drainage Area -- 6.00 square miles.

Design Flood -- New York State requirement 25-year, 6-hour storm

Reference -- "Guidelines for Small Earth Dam Designs" - New York State
and Technical Paper #40, Pg. 42

Rainfall = 3.5"

CN=77

Runoff -- 1.45"

Maximum Q = 1290 cfs

Reference -- SCS National Engineering Handbook, Section 4 - Hydrology
Chapter 21

Flood Routing:

The reservoir will have sufficient capacity to store all the runoff from the design flood without discharging in the auxiliary spillway. It was therefore not necessary to go through the flood routing calculations.

CONCLUSION

Auxiliary Spillway:

The auxiliary spillway has sufficient capacity to discharge the design storm and also have ~~1 foot~~ ^{2 feet} of freeboard below the top of the dam.

Service Spillway:

The service spillway has sufficient capacity to retard the design storm without discharge occurring in the auxiliary spillway.

Drawdown:

The reservoir drain inlet is sufficient to drain the reservoir within the drawdown times.

General Comments:

1. A copy of the hydrologic and hydraulic comments that were sent to ~~the Bureau of Water Regulation~~ are attached.
Frank Dwyer of Water Management
- 2.. Soil stability analysis and structural comments will be furnished by the Department of Transportation.

CWK:CK/ea

New York State Department of Environmental Conservation

MEMORANDUM

TO: Eldred Rich
FROM: Charles W. Kolak *CK*
SUBJECT: Review of Conewango Creek Watershed Project - Site 9A
DATE: March 8, 1972

The hydraulics and hydrology were reviewed for the proposed dam and were found to be satisfactory.

CWK/ea

DATE
FILMED
— 8